chapter

# Network Theorems

A network is a combination of components, such as resistances and voltage sources, interconnected to achieve a particular end result. However, networks generally need more than the rules of series and parallel circuits for analysis. Kirchhoff's laws can always be applied for any circuit connections. The network theorems, though, usually provide shorter methods for solving a circuit.

Some theorems enable us to convert a network into a simpler circuit, equivalent to the original. Then the equivalent circuit can be solved by the rules of series and parallel circuits. Other theorems enable us to convert a given circuit into a form that permits easier solutions.

Only the applications are given here, although all network theorems can be derived from Kirchhoff's laws. Note that resistance networks with batteries are shown as examples, but the theorems can also be applied to ac networks.

## **Chapter Outline**

- **10–1** Superposition Theorem
- 10-2 Thevenin's Theorem
- **10–3** Thevenizing a Circuit with Two Voltage Sources
- **10–4** Thevenizing a Bridge Circuit
- 10–5 Norton's Theorem
- **10–6** Thevenin-Norton Conversions
- **10–7** Conversion of Voltage and Current Sources
- 10-8 Millman's Theorem
- **10–9** T or Y and  $\pi$  or  $\Delta$  Connections

# **Chapter Objectives**

After studying this chapter you should be able to

- Apply the superposition theorem to find the voltage across two points in a circuit containing more than one voltage source.
- *State* the requirements for applying the superposition theorem.
- Determine the Thevenin and Norton equivalent circuits with respect to any pair of terminals in a complex network.
- Apply Thevenin's and Norton's theorems in solving for an unknown voltage or current.
- Convert a Thevenin equivalent circuit to a Norton equivalent circuit and vice versa.
- Apply Millman's theorem to find the common voltage across any number of parallel branches.
- Simplify the analysis of a bridge circuit by using delta to wye conversion formulas.

# **Important Terms**

active components bilateral components current source linear component Millman's theorem Norton's theorem passive components superposition theorem Thevenin's theorem voltage source

# **Online Learning Center**

Additional study aids for this chapter are available at the Online Learning Center: www.mhhe.com/grob11e.

# 10–1 Superposition Theorem

The superposition theorem is very useful because it extends the use of Ohm's law to circuits that have more than one source. In brief, we can calculate the effect of one source at a time and then superimpose the results of all sources. As a definition, the superposition theorem states: *In a network with two or more sources, the current or voltage for any component is the algebraic sum of the effects produced by each source acting separately.* 

To use one source at a time, all other sources are "killed" temporarily. This means disabling the source so that it cannot generate voltage or current without changing the resistance of the circuit. A voltage source such as a battery is killed by assuming a short circuit across its potential difference. The internal resistance remains.

#### Voltage Divider with Two Sources

The problem in Fig. 10–1 is to find the voltage at P to chassis ground for the circuit in Fig. 10–1*a*. The method is to calculate the voltage at P contributed by each source separately, as in Fig. 10–1*b* and *c*, and then superimpose these voltages.

To find the effect of  $V_1$  first, short-circuit  $V_2$  as shown in Fig. 10–1*b*. Note that the bottom of  $R_1$  then becomes connected to chassis ground because of the short circuit across  $V_2$ . As a result,  $R_2$  and  $R_1$  form a series voltage divider for the  $V_1$  source.

Furthermore, the voltage across  $R_1$  becomes the same as the voltage from P to ground. To find this  $V_{R_1}$  across  $R_1$  as the contribution of the  $V_1$  source, we use the voltage divider formula:

$$V_{R_1} = \frac{R_1}{R_1 + R_2} \times V_1 = \frac{60 \text{ k}\Omega}{60 \text{ k}\Omega + 30 \text{ k}\Omega} \times 24 \text{ V}$$
$$= \frac{60}{90} \times 24 \text{ V}$$
$$V_{R_2} = 16 \text{ V}$$

Next find the effect of  $V_2$  alone, with  $V_1$  short-circuited, as shown in Fig. 10–1*c*. Then point A at the top of  $R_2$  becomes grounded.  $R_1$  and  $R_2$  form a series voltage divider again, but here the  $R_2$  voltage is the voltage at P to ground.

With one side of  $R_2$  grounded and the other side to point P,  $V_{R_2}$  is the voltage to calculate. Again we have a series divider, but this time for the negative voltage  $V_2$ . Using

MultiSim Figure 10–1 Superposition theorem applied to a voltage divider with two sources  $V_1$  and  $V_2$ . (a) Actual circuit with +13 V from point P to chassis ground. (b)  $V_1$  alone producing +16 V at P. (c)  $V_2$  alone producing -3 V at P.



the voltage divider formula for  $V_{R_2}$  as the contribution of  $V_2$  to the voltage at P,

$$V_{R_2} = \frac{R_2}{R_1 + R_2} \times V_2 = \frac{30 \text{ k}\Omega}{30 \text{ k}\Omega + 60 \text{ k}\Omega} \times -9 \text{ V}$$
$$= \frac{30}{90} \times -9 \text{ V}$$
$$V_{R_2} = -3 \text{ V}$$

This voltage is negative at P because  $V_2$  is negative. Finally, the total voltage at P is

$$V_P = V_{R_1} + V_{R_2} = 16 - 3$$
  
 $V_p = 13$  V

This algebraic sum is positive for the net  $V_{\rm P}$  because the positive  $V_1$  is larger than the negative  $V_2$ .

By superposition, therefore, this problem was reduced to two series voltage dividers. The same procedure can be used with more than two sources. Also, each voltage divider can have any number of series resistances. Note that in this case we were dealing with ideal voltage sources, that is, sources with zero internal resistance. If the source did have internal resistance, it would have been added in series with  $R_1$  and  $R_2$ .

#### **Requirements for Superposition**

All components must be linear and bilateral to superimpose currents and voltages. *Linear* means that the current is proportional to the applied voltage. Then the currents calculated for different source voltages can be superimposed.

*Bilateral* means that the current is the same amount for opposite polarities of the source voltage. Then the values for opposite directions of current can be combined algebraically. Networks with resistors, capacitors, and air-core inductors are generally linear and bilateral. These are also *passive components*, that is, components that do not amplify or rectify. *Active components*, such as transistors, semiconductor diodes, and electron tubes, are never bilateral and often are not linear.

#### 10–1 Self-Review

Answers at end of chapter.

- a. In Fig. 10–1b, which R is shown grounded at one end?
- b. In Fig. 10–1*c*, which *R* is shown grounded at one end?

# 10-2 Thevenin's Theorem

Named after M. L. Thevenin, a French engineer, Thevenin's theorem is very useful in simplifying the process of solving for the unknown values of voltage and current in a network. By Thevenin's theorem, many sources and components, no matter how they are interconnected, can be represented by an equivalent series circuit with respect to any pair of terminals in the network. In Fig. 10–2, imagine that the block at the left contains a network connected to terminals A and B. Thevenin's theorem states that the *entire* network connected to A and B can be replaced by a single voltage source  $V_{\rm TH}$  in series with a single resistance  $R_{\rm TH}$ , connected to the same two terminals.

Voltage  $V_{\text{TH}}$  is the open-circuit voltage across terminals A and B. This means finding the voltage that the network produces across the two terminals with an open circuit between A and B. The polarity of  $V_{\text{TH}}$  is such that it will produce current from A to B in the same direction as in the original network.

Resistance  $R_{\text{TH}}$  is the open-circuit resistance across terminals A and B, but with all sources killed. This means finding the resistance looking back into the network from terminals A and B. Although the terminals are open, an ohmmeter across AB

## GOOD TO KNOW

When applying the superposition theorem to a dc network, it is important to realize that the power dissipated by a resistor in the network is not equal to the sum of the power dissipation values produced by each source acting separately. The reason is that power is not linearly related to either voltage or current. Recall that  $P = \frac{V^2}{R}$  and  $P = l^2 R$ .

## **GOOD TO KNOW**

Of all the different theorems covered in this chapter, Thevenin's theorem is by far the most widely used. **Figure 10–2** Any network in the block at the left can be reduced to the Thevenin equivalent series circuit at the right.



would read the value of  $R_{\rm TH}$  as the resistance of the remaining paths in the network without any sources operating.

## **Thevenizing a Circuit**

As an example, refer to Fig. 10–3*a*, where we want to find the voltage  $V_{\rm L}$  across the 2- $\Omega R_{\rm L}$  and its current  $I_{\rm L}$ . To use Thevenin's theorem, mentally disconnect  $R_{\rm L}$ . The two open ends then become terminals A and B. Now we find the Thevenin equivalent of the remainder of the circuit that is still connected to A and B. In general, open the part of the circuit to be analyzed and "thevenize" the remainder of the circuit connected to the two open terminals.

Our only problem now is to find the value of the open-circuit voltage  $V_{\text{TH}}$  across AB and the equivalent resistance  $R_{\text{TH}}$ . The Thevenin equivalent always consists of a single voltage source in series with a single resistance, as in Fig. 10–3*d*.

The effect of opening  $R_{\rm L}$  is shown in Fig. 10–3*b*. As a result, the 3- $\Omega R_{\rm 1}$  and 6- $\Omega R_{\rm 2}$  form a series voltage divider without  $R_{\rm L}$ .

Furthermore, the voltage across  $R_2$  now is the same as the open-circuit voltage across terminals A and B. Therefore  $V_{R_2}$  with  $R_L$  open is  $V_{AB}$ . This is the  $V_{TH}$  we need for the Thevenin equivalent circuit. Using the voltage divider formula,

$$V_{R_2} = \frac{6}{9} \times 36 \text{ V} = 24 \text{ V}$$
  
 $V_{R_2} = V_{AB} = V_{TH} = 24 \text{ V}$ 

This voltage is positive at terminal A.

MultiSim Figure 10–3 Application of Thevenin's theorem. (a) Actual circuit with terminals A and B across  $R_{\rm L}$ . (b) Disconnect  $R_{\rm L}$  to find that  $V_{\rm AB}$  is 24 V. (c) Short-circuit V to find that  $R_{\rm AB}$  is 2  $\Omega$ . (d) Thevenin equivalent circuit. (e) Reconnect  $R_{\rm L}$  at terminals A and B to find that  $V_{\rm L}$  is 12 V.



To find  $R_{\text{TH}}$ , the 2- $\Omega R_{\text{L}}$  is still disconnected. However, now the source V is shortcircuited. So the circuit looks like Fig. 10–3c. The 3- $\Omega R_1$  is now in parallel with the 6- $\Omega R_2$  because both are connected across the same two points. This combined resistance is the product over the sum of  $R_1$  and  $R_2$ .

$$R_{\rm TH}=\frac{18}{9}=2\ \Omega$$

Again, we assume an ideal voltage source whose internal resistance is zero.

As shown in Fig. 10–3*d*, the Thevenin circuit to the left of terminals A and B then consists of the equivalent voltage  $V_{\text{TH}}$ , equal to 24 V, in series with the equivalent series resistance  $R_{\text{TH}}$ , equal to 2  $\Omega$ . This Thevenin equivalent applies for any value of  $R_{\text{L}}$  because  $R_{\text{L}}$  was disconnected. We are actually thevenizing the circuit that feeds the open AB terminals.

To find  $V_{\rm L}$  and  $I_{\rm L}$ , we can finally reconnect  $R_{\rm L}$  to terminals A and B of the Thevenin equivalent circuit, as shown in Fig. 10–3*e*. Then  $R_{\rm L}$  is in series with  $R_{\rm TH}$  and  $V_{\rm TH}$ . Using the voltage divider formula for the 2- $\Omega R_{\rm TH}$  and 2- $\Omega R_{\rm L}$ ,  $V_{\rm L} = 1/2 \times 24 \text{ V} = 12 \text{ V}$ . To find  $I_{\rm L}$  as  $V_{\rm L}/R_{\rm L}$ , the value is  $12 \text{ V}/2 \Omega$ , which equals 6 A.

These answers of 6 A for  $I_{\rm L}$  and 12 V for  $V_{\rm L}$  apply to  $R_{\rm L}$  in both the original circuit in Fig. 10–3*a* and the equivalent circuit in Fig. 10–3*e*. Note that the 6-A  $I_{\rm L}$  also flows through  $R_{\rm TH}$ .

The same answers could be obtained by solving the series-parallel circuit in Fig. 10–3*a*, using Ohm's law. However, the advantage of the enizing the circuit is that the effect of different values of  $R_{\rm L}$  can be calculated easily. Suppose that  $R_{\rm L}$  is changed to 4  $\Omega$ . In the Thevenin circuit, the new value of  $V_{\rm L}$  would be  $4/6 \times 24 \text{ V} = 16 \text{ V}$ . The new  $I_{\rm L}$  would be  $16 \text{ V}/4 \Omega$ , which equals 4 A. If we used Ohm's law in the original circuit, a complete, new solution would be required each time  $R_{\rm L}$  was changed.

#### Looking Back from Terminals A and B

The way we look at the resistance of a series-parallel circuit depends on where the source is connected. In general, we calculate the total resistance from the outside terminals of the circuit in toward the source as the reference.

When the source is short-circuited for the venizing a circuit, terminals A and B become the reference. Looking back from A and B to calculate  $R_{TH}$ , the situation becomes reversed from the way the circuit was viewed to determine  $V_{TH}$ .

For  $R_{TH}$ , imagine that a source could be connected across AB, and calculate the total resistance working from the outside in toward terminals A and B. Actually, an ohmmeter placed across terminals A and B would read this resistance.

This idea of reversing the reference is illustrated in Fig. 10–4. The circuit in Fig. 10–4*a* has terminals A and B open, ready to be thevenized. This circuit is similar to that in Fig. 10–3 but with the 4- $\Omega R_3$  inserted between  $R_2$  and terminal A. The interesting point is that  $R_3$  does not change the value of  $V_{AB}$  produced by the source V, but  $R_3$  does increase the value of  $R_{TH}$ . When we look back from





#### **GOOD TO KNOW**

The Thevenin equivalent circuit driving terminals A and B does not change even though the value of  $R_1$  may change.

terminals A and B, the 4  $\Omega$  of  $R_3$  is in series with 2  $\Omega$  to make  $R_{\text{TH}} 6 \Omega$ , as shown for  $R_{\text{AB}}$  in Fig. 10–4*b* and  $R_{\text{TH}}$  in Fig. 10–4*c*.

Let us consider why  $V_{AB}$  is the same 24 V with or without  $R_3$ . Since  $R_3$  is connected to the open terminal A, the source V cannot produce current in  $R_3$ . Therefore,  $R_3$  has no *IR* drop. A voltmeter would read the same 24 V across  $R_2$  and from A to B. Since  $V_{AB}$  equals 24 V, this is the value of  $V_{TH}$ .

Now consider why  $R_3$  does change the value of  $R_{\text{TH}}$ . Remember that we must work from the outside in to calculate the total resistance. Then, A and B are like source terminals. As a result, the 3- $\Omega R_1$  and 6- $\Omega R_2$  are in parallel, for a combined resistance of 2  $\Omega$ . Furthermore, this 2  $\Omega$  is in series with the 4- $\Omega R_3$ because  $R_3$  is in the main line from terminals A and B. Then  $R_{\text{TH}}$  is 2 + 4 = 6  $\Omega$ . As shown in Fig. 10–4*c*, the Thevenin equivalent circuit consists of  $V_{\text{TH}} = 24$  V and  $R_{\text{TH}} = 6 \Omega$ .

10–2 Self-Review

Answers at end of chapter.

- a. For a Thevenin equivalent circuit, terminals A and B are open to find both  $V_{\text{TH}}$  and  $R_{\text{TH}}$ . (True/False)
- b. For a Thevenin equivalent circuit, the source voltage is shortcircuited only to find  $R_{\text{TH}}$ . (True/False)

# 10–3 Thevenizing a Circuit with Two Voltage Sources

The circuit in Fig. 10–5 has already been solved by Kirchhoff's laws, but we can use Thevenin's theorem to find the current  $I_3$  through the middle resistance  $R_3$ . As shown in Fig. 10–5*a*, first mark the terminals A and B across  $R_3$ . In Fig. 10–5*b*,  $R_3$  is disconnected. To calculate  $V_{\text{TH}}$ , find  $V_{\text{AB}}$  across the open terminals.

**Figure 10–5** Thevenizing a circuit with two voltage sources  $V_1$  and  $V_2$ . (*a*) Original circuit with terminals A and B across the middle resistor  $R_3$ . (*b*) Disconnect  $R_3$  to find that  $V_{AB}$  is -33.6 V. (*c*) Short-circuit  $V_1$  and  $V_2$  to find that  $R_{AB}$  is 2.4  $\Omega$ . (*d*) Thevenin equivalent with  $R_L$  reconnected to terminals A and B.



#### **Superposition Method**

With two sources, we can use superposition to calculate  $V_{AB}$ . First short-circuit  $V_2$ . Then the 84 V of  $V_1$  is divided between  $R_1$  and  $R_2$ . The voltage across  $R_2$  is between terminals A and B. To calculate this divided voltage across  $R_2$ ,

$$V_{R_2} = \frac{R_2}{R_{1-2}} \times V_1 = \frac{3}{15} \times (-84)$$
  
 $V_{R_2} = -16.8 \text{ V}$ 

This is the only contribution of  $V_1$  to  $V_{AB}$ . The polarity is negative at terminal A.

To find the voltage that  $V_2$  produces between A and B, short-circuit  $V_1$ . Then the voltage across  $R_1$  is connected from A to B. To calculate this divided voltage across  $R_1$ ,

$$V_{R_1} = \frac{R_1}{R_{1-2}} \times V_2 = \frac{12}{15} \times (-21)$$
  
 $V_R = -16.8 \text{ V}$ 

Both  $V_1$  and  $V_2$  produce -16.8 V across the AB terminals with the same polarity. Therefore, they are added.

The resultant value of  $V_{AB} = -33.6$  V, shown in Fig. 10–5*b*, is the value of  $V_{TH}$ . The negative polarity means that terminal A is negative with respect to B.

To calculate  $R_{\text{TH}}$ , short-circuit the sources  $V_1$  and  $V_2$ , as shown in Fig. 10–5*c*. Then the 12- $\Omega R_1$  and 3- $\Omega R_2$  are in parallel across terminals A and B. Their combined resistance is 36/15, or 2.4  $\Omega$ , which is the value of  $R_{\text{TH}}$ .

The final result is the Thevenin equivalent in Fig. 10–5*d* with an  $R_{\text{TH}}$  of 2.4  $\Omega$  and a  $V_{\text{TH}}$  of 33.6 V, negative toward terminal A.

To find the current through  $R_3$ , it is reconnected as a load resistance across terminals A and B. Then  $V_{\text{TH}}$  produces current through the total resistance of 2.4  $\Omega$  for  $R_{\text{TH}}$  and 6  $\Omega$  for  $R_3$ :

$$I_3 = \frac{V_{\text{TH}}}{R_{\text{TH}} + R_3} = \frac{33.6}{2.4 + 6} = \frac{33.6}{8.4} = 4 \text{ A}$$

This answer of 4 A for  $I_3$  is the same value calculated before, using Kirchhoff's laws, in Fig. 9–5.

It should be noted that this circuit can be solved by superposition alone, without using Thevenin's theorem, if  $R_3$  is not disconnected. However, opening terminals A and B for the Thevenin equivalent simplifies the superposition, as the circuit then has only series voltage dividers without any parallel current paths. In general, a circuit can often be simplified by disconnecting a component to open terminals A and B for Thevenin's theorem.

10–3 Self-Review

Answers at end of chapter.

In the Thevenin equivalent circuit in Fig. 10–5d,

- a. How much is  $R_{\rm T}$ ?
- **b.** How much is  $V_{R_1}$ ?

# 10-4 Thevenizing a Bridge Circuit

As another example of Thevenin's theorem, we can find the current through the 2- $\Omega R_L$  at the center of the bridge circuit in Fig. 10–6*a*. When  $R_L$  is disconnected to open terminals A and B, the result is as shown in Fig. 10–6*b*. Notice how the circuit has become simpler because of the open. Instead of the unbalanced bridge

#### **GOOD TO KNOW**

The polarity of  $V_{\text{TH}}$  is extremely critical because it allows us to determine the actual direction of  $I_3$  through  $R_3$ .

**Figure 10–6** The venizing a bridge circuit. (a) Original circuit with terminals A and B across middle resistor  $R_L$ . (b) Disconnect  $R_L$  to find  $V_{AB}$  of -8 V. (c) With source V short-circuited,  $R_{AB}$  is  $2 + 2.4 = 4.4 \Omega$ . (d) The venine equivalent with  $R_L$  reconnected to terminals A and B.



in Fig. 10–6*a* which would require Kirchhoff's laws for a solution, the Thevenin equivalent in Fig. 10–6*b* consists of just two voltage dividers. Both the  $R_3$ – $R_4$  divider and the  $R_1$ – $R_2$  divider are across the same 30-V source.

Since the open terminal A is at the junction of  $R_3$  and  $R_4$ , this divider can be used to find the potential at point A. Similarly, the potential at terminal B can be found from the  $R_1$ – $R_2$  divider. Then  $V_{AB}$  is the difference between the potentials at terminals A and B.

Note the voltages for the two dividers. In the divider with the 3- $\Omega R_3$  and 6- $\Omega R_4$ , the bottom voltage  $V_{R_4}$  is  $\% \times 30 = 20$  V. Then  $V_{R_3}$  at the top is 10 V because both must add up to equal the 30-V source. The polarities are marked negative at the top, the same as the source voltage V.

Similarly, in the divider with the 6- $\Omega R_1$  and 4- $\Omega R_2$ , the bottom voltage  $V_{R_2}$  is  $\frac{4}{10} \times 30 = 12$  V. Then  $V_{R_1}$  at the top is 18 V because the two must add up to equal the 30-V source. The polarities are also negative at the top, the same as V.

Now we can determine the potentials at terminals A and B with respect to a common reference to find  $V_{AB}$ . Imagine that the positive side of the source V is connected to a chassis ground. Then we would use the bottom line in the diagram as our reference for voltages. Note that  $V_{R_4}$  at the bottom of the  $R_3-R_4$  divider is the same as the potential of terminal A with respect to ground. This value is -20 V, with terminal A negative.

Similarly,  $V_{R_2}$  in the  $R_1 - R_2$  divider is the potential at B with respect to ground. This value is -12 V with terminal B negative. As a result,  $V_{AB}$  is the difference between the -20 V at A and the -12 V at B, both with respect to the common ground reference.

The potential difference  $V_{AB}$  then equals

 $V_{\rm AB} = -20 - (-12) = -20 + 12 = -8 \text{ V}$ 

Terminal A is 8 V more negative than B. Therefore,  $V_{\text{TH}}$  is 8 V, with the negative side toward terminal A, as shown in the Thevenin equivalent in Fig. 10–6*d*.

The potential difference  $V_{AB}$  can also be found as the difference between  $V_{R_3}$  and  $V_{R_1}$  in Fig. 10–6b. In this case,  $V_{R_3}$  is 10 V and  $V_{R_1}$  is 18 V, both positive with

respect to the top line connected to the negative side of the source V. The potential difference between terminals A and B then is 10 - 18, which also equals -8 V. Note that  $V_{AB}$  must have the same value no matter which path is used to determine the voltage.

To find  $R_{\rm TH}$ , the 30-V source is short-circuited while terminals A and B are still open. Then the circuit looks like Fig. 10–6*c*. Looking back from terminals A and B, the 3- $\Omega R_3$  and 6- $\Omega R_4$  are in parallel, for a combined resistance  $R_{\rm T_A}$  of <sup>18</sup>/<sub>9</sub> or 2  $\Omega$ . The reason is that  $R_3$  and  $R_4$  are joined at terminal A, while their opposite ends are connected by the short circuit across the source *V*. Similarly, the 6- $\Omega R_1$  and 4- $\Omega R_2$ are in parallel for a combined resistance  $R_{\rm T_B}$  of <sup>24</sup>/<sub>10</sub> = 2.4  $\Omega$ . Furthermore, the short circuit across the source now provides a path that connects  $R_{\rm T_A}$  and  $R_{\rm T_B}$  in series. The entire resistance is 2 + 2.4 = 4.4  $\Omega$  for  $R_{\rm AB}$  or  $R_{\rm TH}$ .

The Thevenin equivalent in Fig. 10–6*d* represents the bridge circuit feeding the open terminals A and B with 8 V for  $V_{\text{TH}}$  and 4.4  $\Omega$  for  $R_{\text{TH}}$ . Now connect the 2- $\Omega R_{\text{L}}$  to terminals A and B to calculate  $I_{\text{L}}$ . The current is

$$I_{\rm L} = \frac{V_{\rm TH}}{R_{\rm TH} + R_{\rm L}} = \frac{8}{4.4 + 2} = \frac{8}{6.4}$$
$$I_{\rm L} = 1.25 \text{ A}$$

This 1.25 A is the current through the 2- $\Omega R_L$  at the center of the unbalanced bridge in Fig. 10–6*a*. Furthermore, the amount of  $I_L$  for any value of  $R_L$  in Fig. 10–6*a* can be calculated from the equivalent circuit in Fig. 10–6*d*.

10–4 Self-Review

Answers at end of chapter.

In the Thevenin equivalent circuit in Fig. 10-6d,

- a. How much is  $R_{\rm T}$ ?
- b. How much is  $V_{R_1}$ ?

# 10–5 Norton's Theorem

Named after E. L. Norton, a scientist with Bell Telephone Laboratories, Norton's theorem is used to simplify a network in terms of currents instead of voltages. In many cases, analyzing the division of currents may be easier than voltage analysis. For current analysis, therefore, Norton's theorem can be used to reduce a network to a simple parallel circuit with a current source. The idea of a *current source* is that it supplies a total line current to be divided among parallel branches, corresponding to a *voltage source* applying a total voltage to be divided among series components. This comparison is illustrated in Fig. 10–7.

# **Example of a Current Source**

A source of electric energy supplying voltage is often shown with a series resistance that represents the internal resistance of the source, as in Fig. 10-7a. This method corresponds to showing an actual voltage source, such as a battery for dc circuits. However, the source may also be represented as a current source with a parallel resistance, as in Fig. 10-7b. Just as a voltage source is rated at, say, 10 V, a current source may be rated at 2 A. For the purpose of analyzing parallel branches, the concept of a current source.

If the current *I* in Fig. 10–7*b* is a 2-A source, it supplies 2 A no matter what is connected across the output terminals A and B. Without anything connected across A and B, all 2 A flows through the shunt *R*. When a load resistance  $R_L$  is connected across A and B, then the 2-A *I* divides according to the current division rules for parallel branches.

**Figure 10–7** General forms for a voltage source or current source connected to a load *R*<sub>L</sub> across terminals A and B. (*a*) Voltage source *V* with series *R*. (*b*) Current source *I* with parallel *R*. (*c*) Current source *I* with parallel conductance *G*.



## **GOOD TO KNOW**

A current source symbol that uses a solid arrow indicates the direction of conventional current flow. A dashed or broken arrow indicates the direction of electron flow. **Figure 10–8** Any network in the block at the left can be reduced to the Norton equivalent parallel circuit at the right.



Remember that parallel currents divide inversely to branch resistances but directly with conductances. For this reason it may be preferable to consider the current source shunted by the conductance G, as shown in Fig. 10–7c. We can always convert between resistance and conductance because 1/R in ohms is equal to G in siemens.

The symbol for a current source is a circle with an arrow inside, as shown in Fig. 10-7b and *c*, to show the direction of current. This direction must be the same as the current produced by the polarity of the corresponding voltage source. Remember that a source produces electron flow out from the negative terminal.

An important difference between voltage and current sources is that a current source is killed by making it open, compared with short-circuiting a voltage source. Opening a current source kills its ability to supply current without affecting any parallel branches. A voltage source is short-circuited to kill its ability to supply voltage without affecting any series components.

#### **The Norton Equivalent Circuit**

As illustrated in Fig. 10–8, Norton's theorem states that the entire network connected to terminals A and B can be replaced by a single current source  $I_N$  in parallel with a single resistance  $R_N$ . The value of  $I_N$  is equal to the short-circuit current through the AB terminals. This means finding the current that the network would produce through A and B with a short circuit across these two terminals.

The value of  $R_{\rm N}$  is the resistance looking back from open terminals A and B. These terminals are not short-circuited for  $R_{\rm N}$  but are open, as in calculating  $R_{\rm TH}$  for Thevenin's theorem. Actually, the single resistor is the same for both the Norton and Thevenin equivalent circuits. In the Norton case, this value of  $R_{\rm AB}$  is  $R_{\rm N}$  in parallel with the current source; in the Thevenin case, it is  $R_{\rm TH}$  in series with the voltage source.

## Nortonizing a Circuit

As an example, let us recalculate the current  $I_{\rm L}$  in Fig. 10–9*a*, which was solved before by Thevenin's theorem. The first step in applying Norton's theorem is to imagine a short circuit across terminals A and B, as shown in Fig. 10–9*b*. How much current is flowing in the short circuit? Note that a short circuit across AB shortcircuits  $R_{\rm L}$  and the parallel  $R_2$ . Then the only resistance in the circuit is the 3- $\Omega R_1$ in series with the 36-V source, as shown in Fig. 10–9*c*. The short-circuit current, therefore, is

$$I_{\rm N} = \frac{36}{3} \frac{\rm V}{\Omega} = 12 \rm A$$

This 12-A  $I_{\rm N}$  is the total current available from the current source in the Norton equivalent in Fig. 10–9*e*.

To find  $R_N$ , remove the short circuit across A and B and consider the terminals open without  $R_L$ . Now the source V is considered short-circuited. As shown in Fig. 10–9d, the resistance seen looking back from terminals A and B is 6  $\Omega$  in parallel with 3  $\Omega$ , which equals 2  $\Omega$  for the value of  $R_N$ .

MultiSim Figure 10–9 Same circuit as in Fig. 10–3, but solved by Norton's theorem. (a) Original circuit. (b) Short circuit across terminals A and B. (c) The short-circuit current  $I_{\rm N}$  is  ${}^{36}/_{3} = 12$  A. (d) Open terminals A and B but short-circuit V to find  $R_{\rm AB}$  is 2  $\Omega$ , the same as  $R_{\rm TH}$ . (e) Norton equivalent circuit. (f)  $R_{\rm I}$  reconnected to terminals A and B to find that  $I_{\rm I}$  is 6 A.



The resultant Norton equivalent is shown in Fig. 10–9*e*. It consists of a 12-A current source  $I_N$  shunted by the 2- $\Omega R_N$ . The arrow on the current source shows the direction of electron flow from terminal B to terminal A, as in the original circuit.

Finally, to calculate  $I_{\rm L}$ , replace the 2- $\Omega R_{\rm L}$  between terminals A and B, as shown in Fig. 10–9*f*. The current source still delivers 12 A, but now that current divides between the two branches of  $R_{\rm N}$  and  $R_{\rm L}$ . Since these two resistances are equal, the 12-A  $I_{\rm N}$  divides into 6 A for each branch, and  $I_{\rm L}$  is equal to 6 A. This value is the same current we calculated in Fig. 10–3, by Thevenin's theorem. Also,  $V_{\rm L}$  can be calculated as  $I_{\rm L}R_{\rm L}$ , or 6 A  $\times$  2  $\Omega$ , which equals 12 V.

#### Looking at the Short-Circuit Current

In some cases, there may be a question of which current is  $I_N$  when terminals A and B are short-circuited. Imagine that a wire jumper is connected between A and B to short-circuit these terminals. Then  $I_N$  must be the current that flows in this wire between terminals A and B.

Remember that any components directly across these two terminals are also short-circuited by the wire jumper. Then these parallel paths have no effect. However, any components in series with terminal A or terminal B are in series with the wire jumper. Therefore, the short-circuit current  $I_N$  also flows through the series components.

An example of a resistor in series with the short circuit across terminals A and B is shown in Fig. 10–10. The idea here is that the short-circuit  $I_N$  is a branch current, not the main-line current. Refer to Fig. 10–10*a*. Here the short circuit connects  $R_3$  across  $R_2$ . Also, the short-circuit current  $I_N$  is now the same as the current  $I_3$  through  $R_3$ . Note that  $I_3$  is only a branch current.

To calculate  $I_3$ , the circuit is solved by Ohm's law. The parallel combination of  $R_2$  with  $R_3$  equals <sup>72</sup>/<sub>18</sub> or 4  $\Omega$ . The  $R_T$  is 4 + 4 = 8  $\Omega$ . As a result, the  $I_T$  from the source is 48 V/8  $\Omega$  = 6 A.

This  $I_{\rm T}$  of 6 A in the main line divides into 4 A for  $R_2$  and 2 A for  $R_3$ . The 2-A  $I_3$  for  $R_3$  flows through short-circuited terminals A and B. Therefore, this current of 2 A is the value of  $I_{\rm N}$ .

**Figure 10–10** Nortonizing a circuit where the short-circuit current  $I_N$  is a branch current. (a)  $I_N$  is 2 A through short-circuited terminals A and B and  $R_3$ . (b)  $R_N = R_{AB} = 14.4 \Omega$ . (c) Norton equivalent circuit.



To find  $R_{\rm N}$  in Fig. 10–10*b*, the short circuit is removed from terminals A and B. Now the source *V* is short-circuited. Looking back from open terminals A and B, the 4- $\Omega R_1$  is in parallel with the 6- $\Omega R_2$ . This combination is  ${}^{24}\!_{10} = 2.4 \Omega$ . The 2.4  $\Omega$  is in series with the 12- $\Omega R_3$  to make  $R_{\rm AB} = 2.4 + 12 = 14.4 \Omega$ .

The final Norton equivalent is shown in Fig. 10–10*c*. Current  $I_N$  is 2 A because this branch current in the original circuit is the current that flows through  $R_3$  and short-circuited terminals A and B. Resistance  $R_N$  is 14.4  $\Omega$  looking back from open terminals A and B with the source V short-circuited the same way as for  $R_{TH}$ .

10–5 Self-Review

Answers at end of chapter.

- a. For a Norton equivalent circuit, terminals A and B are short-circuited to find  $I_{N}$ . (True/False)
- b. For a Norton equivalent circuit, terminals A and B are open to find  $R_{\rm N}$ . (True/False)

# 10-6 Thevenin-Norton Conversions

Thevenin's theorem says that any network can be represented by a voltage source and series resistance, and Norton's theorem says that the same network can be represented by a current source and shunt resistance. It must be possible, therefore, to convert directly from a Thevenin form to a Norton form and vice versa. Such conversions are often useful.

#### Norton from Thevenin

Consider the Thevenin equivalent circuit in Fig. 10–11*a*. What is its Norton equivalent? Just apply Norton's theorem, the same as for any other circuit. The short-circuit current through terminals A and B is

$$I_{\rm N} = \frac{V_{\rm TH}}{R_{\rm TH}} = \frac{15 \text{ V}}{3 \Omega} = 5 \text{ A}$$

Figure 10–11 Thevenin equivalent circuit in (a) corresponds to the Norton equivalent in (b).



# **GOOD TO KNOW**

An ideal current source is assumed to have an internal resistance of infinite ohms. Therefore, when calculating the Thevenin resistance,  $R_{TH}$ , it is only practical to consider a current source as an open circuit. The resistance, looking back from open terminals A and B with the source  $V_{\text{TH}}$  short-circuited, is equal to the 3  $\Omega$  of  $R_{\text{TH}}$ . Therefore, the Norton equivalent consists of a current source that supplies the short-circuit current of 5 A, shunted by the same 3- $\Omega$  resistance that is in series in the Thevenin circuit. The results are shown in Fig. 10–11*b*.

#### **Thevenin from Norton**

For the opposite conversion, we can start with the Norton circuit of Fig. 10–11*b* and get back to the original Thevenin circuit. To do this, apply Thevenin's theorem, the same as for any other circuit. First, we find the Thevenin resistance by looking back from open terminals A and B. An important principle here, though, is that, although a voltage source is short-circuited to find  $R_{\rm TH}$ , a current source is an open circuit. In general, a current source is killed by opening the path between its terminals. Therefore, we have just the 3- $\Omega R_N$ , in parallel with the infinite resistance of the open current source. The combined resistance then is 3  $\Omega$ .

In general, the resistance  $R_{\rm N}$  always has the same value as  $R_{\rm TH}$ . The only difference is that  $R_{\rm N}$  is connected in parallel with  $I_{\rm N}$ , but  $R_{\rm TH}$  is in series with  $V_{\rm TH}$ .

Now all that is required is to calculate the open-circuit voltage in Fig. 10–11*b* to find the equivalent  $V_{\text{TH}}$ . Note that with terminals A and B open, all current from the current source flows through the 3- $\Omega R_{\text{N}}$ . Then the open-circuit voltage across the terminals A and B is

 $I_{\rm N}R_{\rm N} = 5 \text{ A} \times 3 \Omega = 15 \text{ V} = V_{\rm TH}$ 

As a result, we have the original Thevenin circuit, which consists of the 15-V source  $V_{\text{TH}}$  in series with the 3- $\Omega R_{\text{TH}}$ .

#### **Conversion Formulas**

In summary, the following formulas can be used for these conversions:

Thevenin from Norton:

 $egin{array}{ll} R_{
m TH} &= R_{
m N} \ V_{
m TH} &= I_{
m N} imes R_{
m N} \end{array}$ 

Norton from Thevenin:

$$R_{
m N} = R_{
m TH}$$
  
 $I_{
m N} = V_{
m TH}/R_{
m TH}$ 

Another example of these conversions is shown in Fig. 10–12.



