University of Engineering & Technology Peshawar, Pakistan



CE301: Structure Analysis II

Module 02: Analysis of S.I Beams Using Flexibility method

By: Prof. Dr. Bashir Alam Civil Engineering Department UET, Peshawar

Topics to be Covered

- Introduction
- Prerequisites for using flexibility method
- Revision of conjugate beam concept
- Member end actions
- Analysis of beam Example 1
- Example 2
- Example 3

□ Introduction:

Beams are analyzed with flexibility method due to

- To solve the problem in matrix notation, which is more systematic
- To compute reactions at all the supports.
- To compute internal resisting shear & bending moment at any section of the continuous beam.

- Prerequisites for Analysis with Flexibility method:
 - It is necessary that students must have strong background of the following concepts before starting analysis with flexibility or any other matrix method.
- Enough concept of Matrix Algebra
- Must be able to find the Statical Indeterminacy
- Concept of Deflection methods (Conjugate Beam & Unit load methods)

Conjugate Beam Method:

Conjugate beam is defined as the imaginary beam with the same dimensions (length) as that of the original beam but load at any point on the conjugate beam is equal to the bending moment at that point divided by EI. The conjugate-beam method is an engineering method to derive the slope and displacement of a beam.

> Slope on real beam = Shear on conjugate beam Deflection on real beam = Moment on conjugate beam

Properties of Conjugate Beam:

- 1. The load on the conjugate beam is the M/EI diagram of the loads on the actual beam.
- 2. A simple support for the real beam remains simple support for the conjugate beam.
- 3. A fixed end for the real beam becomes free end for the conjugate beam.
- 4. The point of zero shear for the conjugate beam corresponds to a point of zero slope for the real beam.
- 5. The point of maximum moment for the conjugate beam corresponds to a point of maximum deflection for the real beam.



Real beams and its Conjugate Beams

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- Member End Actions: Member end actions are the moments and shear at each point where its going to be changed. We can find the member end actions using flexibility method when the redundant actions are known.
- Let us illustrate the procedure of finding member actions by flexibility method with the help of Example 2 in Module 1 as shown in fig.



Flexibility Method for Beams Analysis Vertical reactions at B & moment at A is taken as redundant. $AR_1 \square P_1 \square P_2 P_2$ $B_AR_2 \square C$

Step # 01: Specify the member end actions AM_n by assigning a No. to them. e.g. in the above problem



 $AM_n = is$ the member end action in the indeterminate structure at different location specified with a number "n". n shows the number of member end actions.

Step # 02: Determine the member end actions (shear & moments) in the released structure under the external applied loads (AML_n) at the specified locations.



 AML_n = is the member end actions in the released structure at location "n" when acted upon by the external applied loads.

Step # 03: Determine the member end actions (shear & moments) in the released structure when acted upon by a unit at action 1st at redundant location 1 and then at 2 (AMR_{n1} & AMR_{n2}).

When a unit action is applied at the redundant location 1 as shown.



When a unit action is applied at the redundant location 2 as shown.



 $AMR_{n1} \& AMR_{n2} = is$ the member end actions in the released structure when acted upon by a unit action. n shows the number member action and 1 & 2 shows the unit action/ load position.

 $AM_1 = AML_1 + AMR_{11}AR_1 + AMR_{12}AR_2$

 $AM_2 = AML_2 + AMR_{21}AR_1 + AMR_{22}AR_2$ $AM_8 = AML_8 + AMR_{81}AR_1 + AMR_{82}AR_2$ $\begin{bmatrix} AM_1 \\ AM_2 \\ \vdots \\ AM_8 \end{bmatrix} = \begin{bmatrix} AML_1 \\ AML_2 \\ \vdots \\ AML_8 \end{bmatrix} + \begin{bmatrix} AMR_{11} & AMR_{12} \\ AMR_{21} & AMR_{22} \\ \vdots \\ AMR_{81} & AMR_{82} \end{bmatrix} \begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix}$

[AM] = [AML] + [AMR][AR]

This method will be explained again in the coming problem

Problem 01: Analyze the given beam using flexibility method.



Take EI = constant

S.I = 2 degree So two redundant actions should be chosen. Choose those as redundant which makes the calculation handy.

• **Step # 01:** Select the redundant actions and assign coordinates at those locations.

Vertical reactions at B & C are taken as redundant.



• DRS₁ & DRS₂ are the initial support rotation & settlement corresponding to the redundant actions 1 & 2 which is zero in this case.

• Remove all the loads and redundant constrains to get the primary structure.



Basic determinate structure (BDS) or released structure or Primary structure

Note: when the support settlement and redundant actions are in opposite direction then DRS will have –ve sign.

Step # 02 : Compute the values of displacements (DRL) in the primary structure corresponding to the redundant locations when primary structure acted upon by the actual loads or Compute the values of [DRL].



1st Compute the moments at different locations in the released structure





Finding the values of W_1 , W_2 & W_3 from the fig shown in previous slide

Note



$$\mathsf{C}_1 = \frac{L}{3} \left(\frac{a+2b}{a+b} \right) \quad \mathsf{C}_2 = \frac{L}{3} \left(\frac{2a+b}{a+b} \right)$$

$$W_{1} = \frac{1}{2} \left(\frac{1100 + 600}{EI} \right) 10 = \frac{8500}{EI} k$$
$$W_{2} = \frac{1}{2} \left(\frac{600 + 300}{EI} \right) 10 = \frac{4500}{EI} k$$
$$W_{2} = \frac{1}{3} \left(\frac{300}{EI} \right) 20 = \frac{2000}{EI} k$$
$$X_{1} = \frac{10}{3} \left(\frac{600 + 2(1100)}{600 + 1100} \right) = 5.49'$$
$$X_{2} = \frac{10}{3} \left(\frac{300 + 2(600)}{300 + 600} \right) = 5.56'$$
$$X_{2} = \frac{3}{4} (20) = 15'$$

$$DRL_1 = W_1(X_1 + 10) + W_2(X_2)$$

$$= \frac{8500}{\text{EI}} \left(5.49 + 10 \right) + \frac{4500}{\text{EI}} \left(5.56 \right)$$

$$= \frac{156685}{EI}$$

$$DRL_2 = W_1(X_1 + 30) + W_2(X_2 + 20) + W_3X_2$$

$$= \frac{8500}{\text{EI}} (5.49 + 30) + \frac{4500}{\text{EI}} (5.56 + 20) + \frac{2000}{\text{EI}} (15)$$

3

$$= \frac{446685}{EI}$$
$$[DRL] = \begin{bmatrix} DRL_1\\ DRL_2 \end{bmatrix} = \begin{bmatrix} 156685\\ 446685 \end{bmatrix} \times \frac{1}{EI}$$

- Step # 03 : Compute the values of rotations/displacements in the primary structure corresponding to the redundant locations when primary structure acted upon by the UNIT actions or Compute the values of flexibility matrix [*f*].
 - i. 1st apply a unit value of AR₁ at reference point 1 and Compute the values of flexibility coefficients $(f_{11} \& f_{21})$.



Step # 03 (i): Contd...



Step # 03 (i): Contd...

$$W = \frac{1}{2} \left(\frac{20 + 20}{EI} \right) = \frac{200}{EI} k$$

$$X = \frac{2}{3} (20) = 13.33'$$

$$f_{11} = W(X) \qquad \qquad f_{21} = W(X + 20)$$

$$= \frac{200}{EI} (13.33) \qquad \qquad = \frac{200}{EI} (13.33 + 20)$$

$$= \frac{2666}{EI} \qquad \qquad = \frac{6666}{EI}$$

Note: $f_{11} \& f_{22}$ will be the moment in conjugate beam at Corresponding location

ii. Now apply a unit value of AR₂ at reference point 2 and Compute the values of flexibility coefficients $(f_{12} \& f_{22})$. 1k



$$W_{1} = \frac{1}{2} \left(\frac{20 + 40}{EI} \right) 20 = \frac{600}{EI} k$$
$$X_{1} = \frac{20}{3} \left(\frac{20 + 2(40)}{20 + 40} \right) = 11.11'$$

W₁ & X₁ refer to the trapezoidal part in $\frac{M}{EI}$ digram

$$W_{2} = \frac{1}{2} \left(\frac{40 * 40}{EI} \right) = \frac{800}{EI} k$$

$$W_{2} \& X_{2} \text{ refer to the whole triangle in } \frac{M}{EI}$$

$$W_{2} \& X_{2} \text{ refer to the whole triangle in } \frac{M}{EI}$$

$$f_{12} = W_1(X_1) \qquad f_{22} = W_2(X_2)$$

= $\frac{600}{EI}$ (11.11) = $\frac{200}{EI}$ (13.33 + 20)
 f_{12} only the
zium part is
dered = $\frac{6666}{EI}$ = $\frac{21336}{EI}$ For f_{22} the whole
tringle is taken.

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$$f_{11} = \frac{2666}{EI} \qquad f_{12} = \frac{6666}{EI}$$
$$f_{21} = \frac{6666}{EI} \qquad f_{22} = \frac{21336}{EI}$$

$$[f] = \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix}$$

 $[f] = \frac{1}{EI} \begin{bmatrix} 2666 & 6666 \\ 6666 & 21336 \end{bmatrix}$

Flexibility coefficient matrix

Flexibility Method for Beams Analysis Step # 04: Apply compatibility and principle of superposition at the location of the removed redundants and solve the matrices to compute the values of redundant actions AR. As we know

From this

 $[DRS] = [DRL] + [f] \cdot [AR]$ $[AR] = [f]^{-1} \cdot [DRS - DRL]$ $\begin{bmatrix}AR_{1}\\AR_{2}\end{bmatrix} = \begin{bmatrix}f_{11} & f_{12}\\f_{21} & f_{22}\end{bmatrix}^{-1} \begin{bmatrix}DRS_{1} - DRL_{1}\\DRS_{2} - DRL_{2}\end{bmatrix}$

$$\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix}^{-1} \begin{bmatrix} DRS_1 - DRL_1 \\ DRS_2 - DRL_2 \end{bmatrix}$$

 $\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = EI \begin{bmatrix} 0.0017 & -0.00053 \\ -0.00053 & 0.00021 \end{bmatrix} \begin{bmatrix} 0 - 156685 \\ 0 - 446685 \end{bmatrix} \times \frac{1}{EI}$

$$\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} -29.36 \\ -11.76 \end{bmatrix}$$

-ive sign shows that our assumed redundant actions direction is wrong



Step # 05: Compute the member end actions. As we know that

[AM] = [AML] + [AMR][AR]



a) Compute AML values.



b) Compute the AMR values.

1st apply a unit action at redundant location 1 and then at 2 as shown below. _ 1k







So the AMR values are

	$[AMR_{11}]$	AMR_{12}		r 1	ך 1
	AMR ₂₁	AMR ₂₂		-1	-1
	AMR ₃₁	AMR ₃₂		0	1
$[AMR]_{7,2} =$	AMR ₄₁	AMR_{42}	=	0	-1
*	AMR ₅₁	AMR_{52}		20	40
	AMR ₆₁	AMR_{62}		10	30
	$L_{AMR_{71}}$	AMR_{72}		0	20

Now member end actions will be computed as given below

[AM] = [AML] + [AMR][AR]

$[AM_1]$		$[AML_1]$		AMR_{11}	AMR_{12}	
AM_2		AML_2		AMR ₂₁	AMR ₂₂	
AM_3		AML_3		AMR ₃₁	AMR ₃₂	гЛД
AM_4	=	AML_4	+	AMR ₄₁	AMR_{42}	
AM_5		AML_5		AMR ₅₁	AMR_{52}	LAK ²
AM_6		AML_6		AMR_{61}	AMR_{62}	
L_{AM_7}		$\lfloor AML_7 \rfloor$		$LAMR_{71}$	AMR_{72}	



Complete analyzed structure. Shear force and bending moment diagrams are given on next slide.



Problem 02: Analyze the given beam using flexibility method, if support A rotates by 0.002 rad clockwise, support B settles down by 0.75 in & support C settles down by 1 in.



S.I = 2 degree So two redundant actions should be chosen.

• **Step # 01:** Select the redundant actions and assign coordinates at those locations.

Vertical reactions at B & C are taken as redundants.



• DRS₁ & DRS₂ are the initial support settlement corresponding to the redundant actions 1 & 2.

• Remove all the loads and redundant constraints to get the primary structure.



Basic determinate structure (BDS) or released structure

Note: when the support settlement and redundant action are in opposite direction then DRS will have –ve sign.

- **Step # 02 :** Compute the values of [DRL].
- a) Due to direct loads [DRL']



1st Compute the moments at different locations in the released structure



$$\begin{bmatrix} DRL' \end{bmatrix} = \begin{bmatrix} DRL'1 \\ DRL'2 \end{bmatrix} = \begin{bmatrix} 156685 \\ 446685 \end{bmatrix} \times \frac{1}{EI} \qquad \begin{array}{c} \text{Check problem 1} \\ \text{for details} \\ \text{calculations} \end{array}$$
$$\begin{bmatrix} DRL' \end{bmatrix} = \begin{bmatrix} DRL'1 \\ DRL'2 \end{bmatrix} = \begin{bmatrix} 156685 \\ 446685 \end{bmatrix} \times \frac{1}{166666.67}$$
$$\begin{bmatrix} DRL' \end{bmatrix} = \begin{bmatrix} DRL'1 \\ DRL'2 \end{bmatrix} = \begin{bmatrix} 0.94' \\ 2.68' \end{bmatrix}$$

Flexibility Method for Beams Analysis b) Due to indirect loads [DRL"] 0.002 rad \mathbf{B}^{1} 2 С DRL"₂ 0.002 rad DRL"₁ As we know that for smaller angles $tan\theta = \theta$ $DRL'_1 = 0.002 * 20 = 0.04 \text{ ft}$ $[DRL"] = \begin{bmatrix} DRL"_1 \\ DRL"_2 \end{bmatrix} = \begin{bmatrix} 0.04' \\ 0.08' \end{bmatrix}$ $DRL''_{2} = 0.002 * 40 = 0.08 \text{ ft}$ So final DRL will be

 $[DRL] = \begin{bmatrix} DRL'1\\DRL'2 \end{bmatrix} + \begin{bmatrix} DRL''1\\DRL''2 \end{bmatrix} = \begin{bmatrix} 0.94'\\2.68' \end{bmatrix} + \begin{bmatrix} \overline{0.04'}\\0.08' \end{bmatrix} = \begin{bmatrix} 0.98'\\2.76' \end{bmatrix}$

• **Step # 03 :** Compute the values of flexibility matrix [*f*].



$$f_{11} = \frac{2666}{EI} \qquad f_{12} = \frac{6666}{EI}$$
$$f_{21} = \frac{6666}{EI} \qquad f_{22} = \frac{21336}{EI}$$

For detail calculations see problem 1.

$$[f] = \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix}$$

 $[f] = \frac{1}{EI} \begin{bmatrix} 2666 & 6666 \\ 6666 & 21336 \end{bmatrix}$

Flexibility coefficient matrix

$$[f] = \frac{1}{166666.67} \begin{bmatrix} 2666 & 6666 \\ 6666 & 21336 \end{bmatrix}$$

 $\begin{bmatrix} f \end{bmatrix} = \begin{bmatrix} 0.016 & 0.04 \\ 0.04 & 0.128 \end{bmatrix}$

Step # 04: Compute the values of redundant actions AR. As we
 know that

 $[DRS] = [DRL] + [f] \bullet [AR]$

 $[AR] = [f]^{-1} \bullet [DRS - DRL]$

$$\begin{bmatrix} AR_{1} \\ AR_{2} \end{bmatrix} = \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix}^{-1} \begin{bmatrix} DRS_{1} - DRL_{1} \\ DRS_{2} - DRL_{2} \end{bmatrix}$$

 $\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} 0.016 & 0.04 \\ 0.04 & 0.128 \end{bmatrix}^{-1} \begin{bmatrix} 0.0625 - 0.98 \\ 00833 - 2.76 \end{bmatrix}$

 $\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} -23.15 \\ -13.66 \end{bmatrix}$

-ive sign shows that our assumed redundant actions directions are wrong

Final determinate structure



Now we can apply equilibrium equations to further solve the structure. Or we can compute member end actions using matrix approach as given in the coming slides

Step # 05: Compute the member end actions. As we know that



a). Compute the AML values

$$\begin{bmatrix} AML_{1} \\ AML_{2} \\ AML_{3} \\ AML_{3} \\ AML_{4} \\ AML_{5} \\ AML_{5} \\ AML_{6} \\ AML_{7} \end{bmatrix} = \begin{bmatrix} 50 \\ -30 \\ 30 \\ 10 \\ 600 \\ 300 \end{bmatrix}$$

For detail calculation See problem 1.

b). Compute the AMR values

$$[AMR]_{7*2} = \begin{bmatrix} AMR_{11} & AMR_{12} \\ AMR_{21} & AMR_{22} \\ AMR_{31} & AMR_{32} \\ AMR_{41} & AMR_{42} \\ AMR_{51} & AMR_{52} \\ AMR_{61} & AMR_{62} \\ AMR_{71} & AMR_{72} \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ -1 & -1 \\ 0 & 1 \\ 0 & -1 \\ 20 & 40 \\ 10 & 30 \\ 0 & 20 \end{bmatrix}$$

For detail calculation see problem 1 in this module.

Now

V	[A. A. A. A. A. A. A.	M_1 M_2 M_3 M_4 M_5 M_6 M_7	=	AN AN AN AN AN AN	$\begin{bmatrix} I & L_1 \\ I & L_2 \\ I & L_3 \\ I & L_4 \\ I & L_5 \\ I & L_6 \\ I & L_7 \end{bmatrix}$	÷	Al Al Al Al Al Al Al	MR_{11} MR_{21} MR_{31} MR_{41} MR_{51} MR_{61} MR_{71}	A A A A A A A A	MR ₁₂ MR ₂₂ MR ₃₂ MR ₄₂ MR ₅₂ MR ₆₂ MR ₆₂	$\begin{bmatrix} 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 \\ 2 $	
$\begin{bmatrix} AM_1 \\ AM_2 \\ AM_3 \\ AM_4 \end{bmatrix}$	=		50 7 30 30 0	+	$\begin{bmatrix} 1 \\ -1 \\ 0 \\ 0 \\ 0 \end{bmatrix}$		1 1 1 1	[—23. [—13.	15	=	- 13.17 6.83 16.32 13.68	k k k k

AM_2^{\uparrow}		-30		-1	-1		6.83 k
AM_3^{-}	30			0	1	г <u>001</u> Гл	16.32 k
AM_4	=	0	+	0	-1	$\begin{vmatrix} -23.15 \\ 12.66 \end{vmatrix} =$	13.68 k
AM_5		1100		20	40	r—13.001	89.80′ k
AM_6		600		10	30		-41.90' k
AM_7		300		0	20		26.40′ k



Final analyzed structure

Class Activity: Draw shear force and bending moment diagram for the above given beam .

Problem 03: Analyze the given beam using flexibility method. The supports at B & C are spring supports having stiffness's $S_1 = 15 \text{ k/ft} \& S_2 = 10 \text{ k/ft}$ as shown in fig.

Take



S.I = 2 degree So two redundant actions should be chosen.

• **Step # 01:** Select the redundant actions and assign coordinates at those locations.

Vertical reactions at B & C are taken as redundants.



• DRS₁ & DRS₂ are the initial support settlement corresponding to the redundant actions 1 & 2.



$$DRL_{1} = \frac{156685}{EI}$$

$$DRL_{2} = \frac{446685}{EI}$$

$$DRL_{2} = \begin{bmatrix} 156685 \\ 446685 \end{bmatrix} \times \frac{1}{EI}$$

$$= \begin{bmatrix} 156685 \\ 446685 \end{bmatrix} \times \frac{1}{EI}$$

$$= \begin{bmatrix} 156685 \\ 446685 \end{bmatrix} \times \frac{1}{166666.6}$$

$$= \begin{bmatrix} 0.94 \\ 2.68 \end{bmatrix}$$

• Step # 03 : Compute the values of flexibility matrix [*f*]. Also as there are spring supports at redundant location 1& 2 so add the effect of spring with flexibility matrix.



$$[f] = \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix}$$

For detail calculations see problem 1.

 $[f] = \frac{1}{EI} \begin{bmatrix} 2666 & 6666 \\ 6666 & 21336 \end{bmatrix}$

$$[f] = \frac{1}{166666.67} \begin{bmatrix} 2666 & 6666 \\ 6666 & 21336 \end{bmatrix} = \begin{bmatrix} 0.016 & 0.04 \\ 0.04 & 0.128 \end{bmatrix}$$

Now add the effect of spring with Flexibility matrix, as we know that

Stiffness = 1/ Flexibility

$$[f] = \begin{bmatrix} 0.016 & 0.04 \\ 0.04 & 0.128 \end{bmatrix} + \begin{bmatrix} \frac{1}{15} & 0 \\ 0 & \frac{1}{10} \end{bmatrix} = \begin{bmatrix} 0.083 & 0.04 \\ 0.04 & 0.228 \end{bmatrix}$$

Flexibility coefficient matrix

Step # 04: Compute the values of redundant actions AR. As we
 know that

 $[DRS] = [DRL] + [f] \bullet [AR]$

 $[AR] = [f]^{-1} \bullet [DRS - DRL]$

$$\begin{bmatrix} AR_{1} \\ AR_{2} \end{bmatrix} = \begin{bmatrix} f_{11} & f_{12} \\ f_{21} & f_{22} \end{bmatrix}^{-1} \begin{bmatrix} DRS_{1} - DRL_{1} \\ DRS_{2} - DRL_{2} \end{bmatrix}$$

 $\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} 0.016 & 0.04 \\ 0.04 & 0.128 \end{bmatrix}^{-1} \begin{bmatrix} 0.0625 - 0.98 \\ 00833 - 2.76 \end{bmatrix}$

$$\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} -6.30 \\ -10.87 \end{bmatrix}$$

-ive sign shows that our assumed redundant actions directions are wrong

Final determinate structure



Now we can apply equilibrium equations to further solve the structure. Or we can compute member end actions using matrix approach as given in the coming slides

Step # 05: Compute the member end actions. As we know that



a). Compute the AML values

$$\begin{bmatrix} AML_{1} \\ AML_{2} \\ AML_{3} \\ AML_{3} \\ AML_{4} \\ AML_{5} \\ AML_{6} \\ AML_{7} \end{bmatrix} = \begin{bmatrix} 50 \\ -30 \\ 30 \\ 0 \\ 1100 \\ 600 \\ 300 \end{bmatrix}$$

For detail calculation See problem 1.

b). Compute the AMR values

$$[AMR]_{7*2} = \begin{bmatrix} AMR_{11} & AMR_{12} \\ AMR_{21} & AMR_{22} \\ AMR_{31} & AMR_{32} \\ AMR_{41} & AMR_{42} \\ AMR_{51} & AMR_{52} \\ AMR_{61} & AMR_{62} \\ AMR_{71} & AMR_{72} \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ -1 & -1 \\ 0 & 1 \\ 0 & -1 \\ 20 & 40 \\ 10 & 30 \\ 0 & 20 \end{bmatrix}$$

For detail calculation see problem 1 in this module.

Now

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 L_{AM_7}

V	ΓA	Μ ₁]	<i>∎AN</i>	$[L_1]$		Γ <i>ΑΙ</i>	MR_{11}	AMR_1	2
	A	M_2^{-}	AM	$1L_2$		Al	$MR_{21}^{}$	AMR_2	2
	A	M_3^{-}	AM	$1L_3$		Al	$MR_{31}^{}$	AMR_3	
	A	$M_4 =$	AM	$1L_4$	+	Al	MR_{41}	AMR_4	$2 A R_1 A D $
	A	M_5	AM	L_5		Al	MR_{51}	AMR_5	
	A	M_6	AM	L_6		Al	MR_{61}	AMR_6	2
	L_{A}	M_7	LAN	$[L_7]$		L_{A1}	MR_{71}	AMR ₇	2
$[AM_1]$		r 50 ⁻		r 1		ן1			32.87 k
AM_2		-30		-1	—	1			-12.83 k
AM_3		30		0)	1	г 62	Λ 1	19.13 k
AM_4	=	0	+	0) —	1		$ 0 _{07} = 0 _{07}$	10.87 k
AM_5		1100		20) 4	0	- <u> </u>		539 .2′ k
AM_6		600		10	3	0			210.9′ k

20

82.6′ k

L 0

[300]

Now Shear force and Bending moment diagram



References

- Structural Analysis by R. C. Hibbeler
- Matrix structural analysis by William Mc Guire
- Matrix analysis of frame structures by William Weaver
- Online Civil Engineering blogs