

## Chapter 5

# Single-Mode Fibers – Basics

- **How a single-mode fiber works (工作原理)**
- **Attenuation (衰减)**
- **Dispersion & bandwidth (色散与带宽)**

# 5.1 How a Singlemode Fiber Works

## ◆ The principle of action

for fundamental mode  $LP_{01}$  , Cutoff number:  $V_c=0$

for  $LP_{11}$  , Cutoff number:  $V_c=2.405$

**Singlemode operation:** (单模工作)

$$V < 2.405 \quad \text{or} \quad \lambda > \lambda_c$$

where:

$$V = \frac{\pi d}{\lambda} \sqrt{n_1^2 - n_2^2} \approx \frac{\pi d n}{\lambda} \sqrt{2\Delta}, \quad \Delta = \frac{n_1 - n_2}{n}$$

$$\lambda_c = \frac{\pi d \sqrt{n_1^2 - n_2^2}}{2.405}$$

Decrease d:  $<10\mu\text{m} \leftarrow 50/62.5\mu\text{m}$ , and even  $1000\mu\text{m}$

Increase  $\lambda$ :  $>1300\text{nm} \leftarrow 650\text{nm}$

Decrease  $\Delta$ :  $<0.4\% \leftarrow 1-2\%$

**Smaller critical propagation angle and NA!**

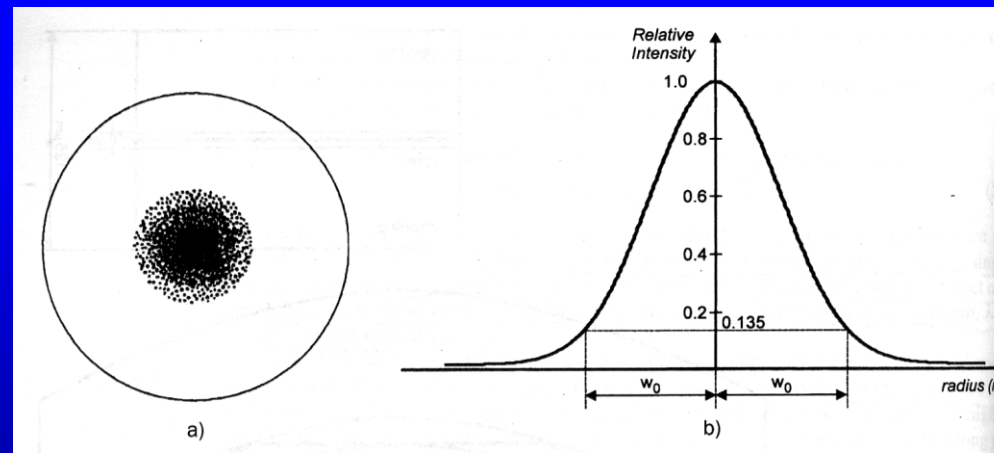
## ◆ Gaussian Beam (高斯光束)

-> A beam of light does not have strict cross-sectional boundaries.

-> The most popular model used in singlemode fiber is Gaussian curve:

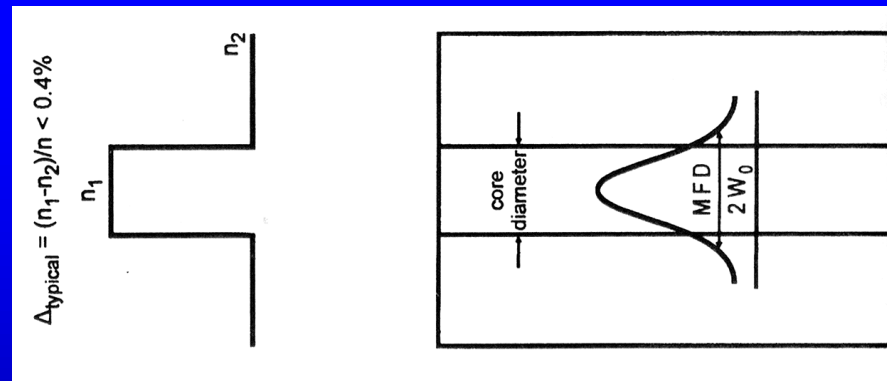
$$I(r) = I(0)e^{-\frac{2r^2}{w_0^2}}$$

where  $2w_0$  is the mode-field diameter. (模场直径)



## ◆ Core, Cladding, and Mode Field Diameter (模场直径)

- > Manufactures use the mode-field diameter, MFD, rather than the core diameter.
- > The essential portion of the light (typically, about 20%) is carried by the cladding.
- > The refractive index profile might be too complex to precisely detect the border between the core and the cladding.



Typical dimensions of MFD and the core diameters in step-index single-mode fibers are 9.3 and 8.3  $\mu\text{m}$ .

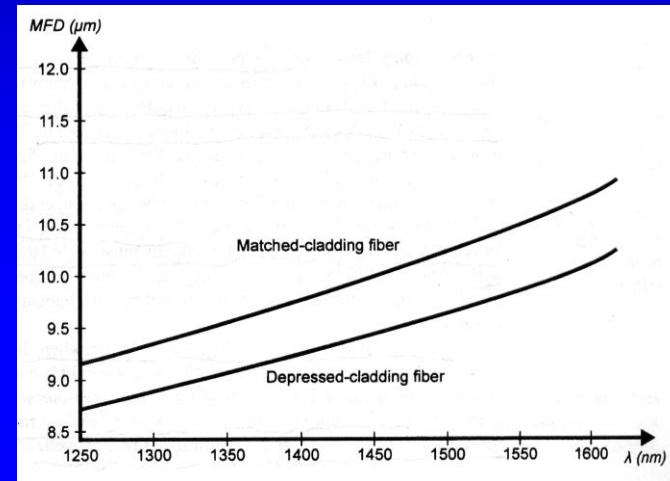
-> The fiber's effective refractive index is the combination of the core and cladding refractive index. (有效折射率) ✓

-> The mode-field diameter depends on operating wavelength.

Longer wavelength →

Larger MFD →

Worse Confinement



-> If two fibers have different mode-field diameters, one will have extra insertion loss: (插入损耗)

$$Loss_{CoulingMFD} (dB) = -10 \log [4 / (MFD_1 / MFD_2 + MFD_2 / MFD_1)^2]$$

Closer MFD → Better Matching → Less Insertion Loss

## ◆ Cutoff wavelength (截止波长)

-> Cutoff wavelength written as the refractive index:

$$\lambda_c = \{\pi d \sqrt{[(n_1)^2 - (n_2)^2]}\} / 2.405 \quad \text{correct in page 143.}$$

-> Cutoff wavelength written as the numerical aperture: (数值孔径)

$$\lambda_c = 1.306 d NA \quad \text{correct in page 144.}$$

-> *The optical fiber can be singlemode or multimode, which depends on the operation wavelength.*

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## 5.2 Attenuation (衰减)

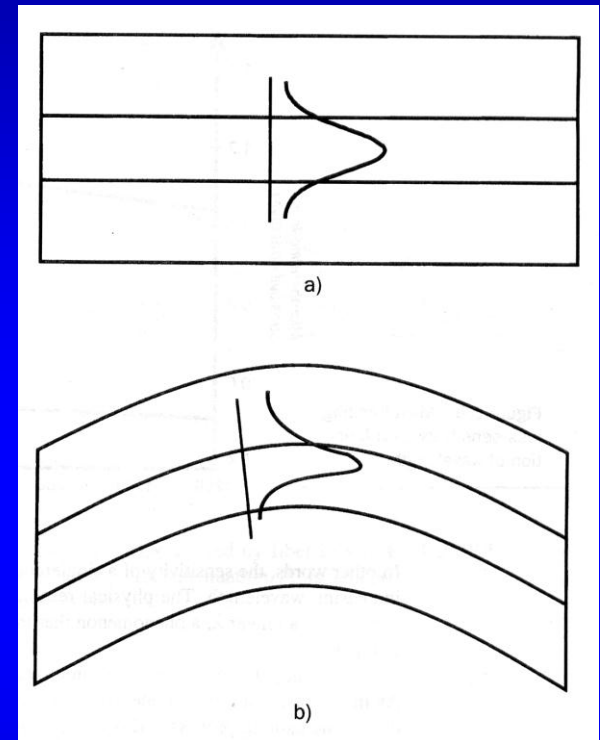
### ◆ Bending loss (弯曲损耗)

#### ● Macrobending loss (宏弯损耗)

-> Change of the mode field

- A longer “tail” appears at the outer side of the cladding (*depending on wavelength*)

-> Traveling velocity analysis (-> loss)



A singlemode fiber is more sensitive to bending than is a multimode fiber!

## -> Properties of Macrobending Loss

*i.* changing in exponential form with bending radius (指数形改变)

*ii.* relate to operation wavelength

*iii.* depend on parameter  $\Delta$  or NA

*ii & iii:* less normolized MFD, less bending loss,  $MAC=MFD/\lambda_c$

## ● Microbending Loss: (微弯损耗)

-> Mechanism is the same of multimode fiber : *stress induced by cabling process, or thermal stress.* (成缆工艺, 热应力)

-> Dependence on wavelength: *Larger wavelength, more micro-bending loss (because the MFD increases)*



## ◆ Scattering ( 散射 )

- > Mechanism : Small changes in the core's refractive index
- > Scattering loss determines the spectral dependence

## ◆ Absorption ( 吸收 )

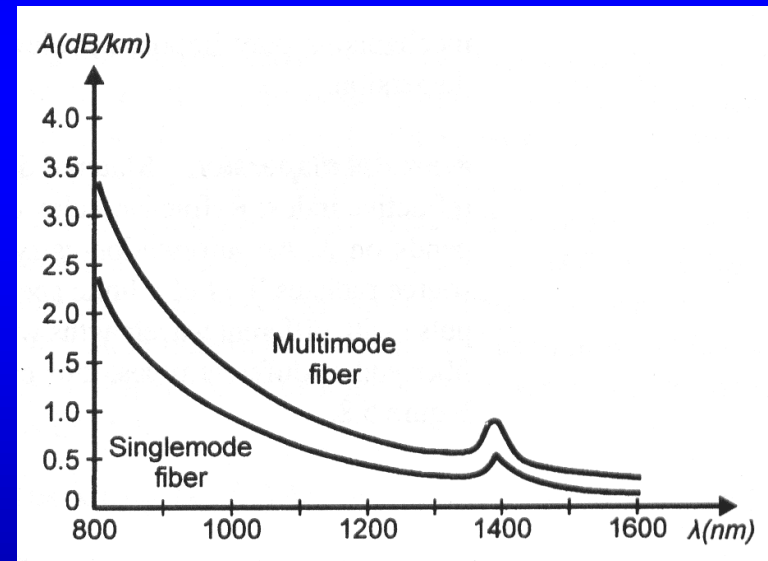
### -> Mechanism

The absorption by  $\text{SiO}_2$ , and imperfections (e.g.  $\text{OH}^-$ )

### -> Less absorption loss !

(Smaller MFD of  $\text{LP}_{01}$  in SMF;

*Another important advantage of SMF, except for the absence of inter-modal dispersion )*



## 5.3 Dispersion and Bandwidth

Dispersion in a singlemode fiber : (no intermodal dispersion)

*chromatic dispersion + polarization-mode dispersion* (色度色散+偏振模色散)

### ◆ Chromatic Dispersion

(*material dispersion + waveguide dispersion*) (材料色散+波导色散)

-> Pulse signal bandwidth:  $\Delta\lambda \ll \lambda_0$

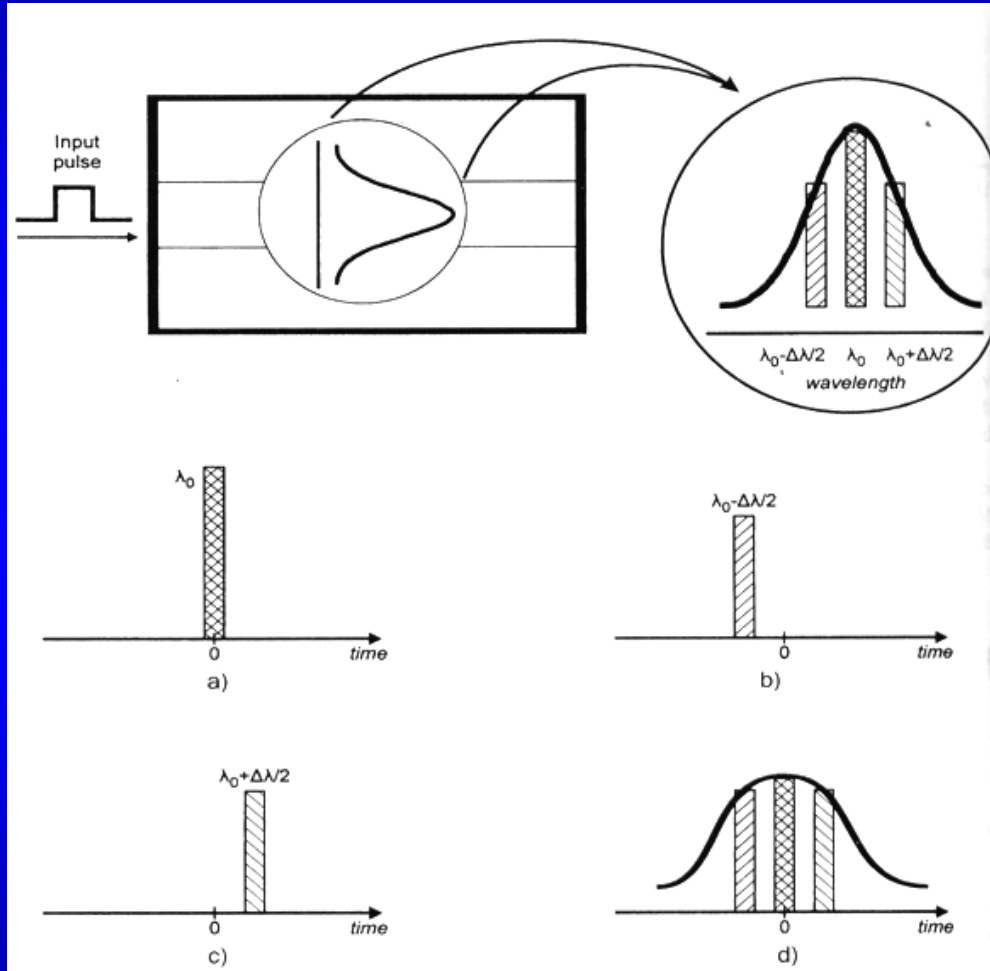
-> Signal spreading:  $\Delta t = t(\lambda_0 + \frac{\Delta\lambda}{2}) - t(\lambda_0 - \frac{\Delta\lambda}{2})$

$$= \left. \frac{dt}{d\lambda} \right|_{\lambda=\lambda_0} \Delta\lambda$$

-> Dispersion characteristics: (unit: ps /nm.km)

$$D(\lambda) = \frac{1}{L} \frac{dt}{d\lambda} = \frac{d}{d\lambda} \left( \frac{1}{V_g} \right) \quad \text{or,} \quad \Delta t = LD(\lambda_0)\Delta\lambda$$

# ● Material Dispersion (材料色散)



(a) Pulse fraction delivered by  $\lambda_0$  component.

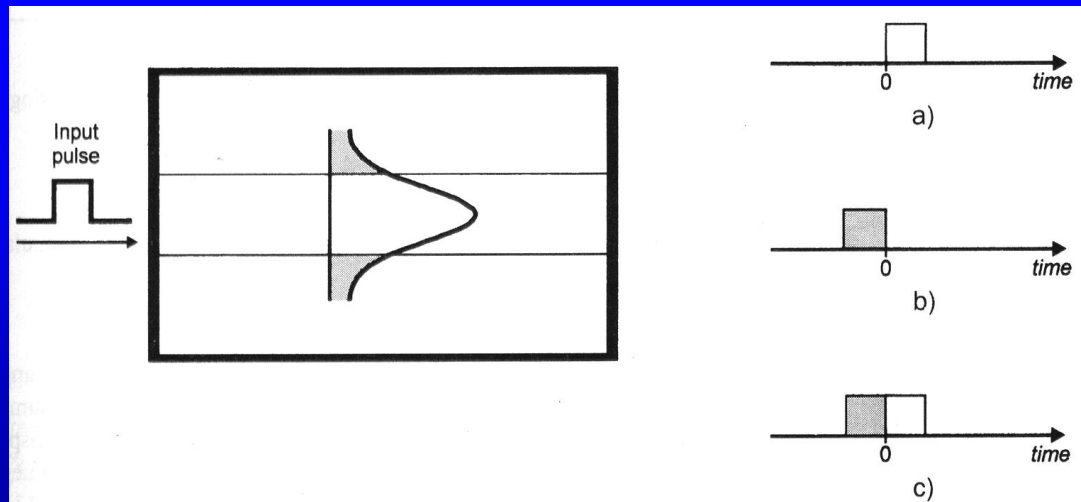
(b) Pulse fraction delivered by  $\lambda_0 - \Delta\lambda/2$ ;

(c) Pulse fraction delivered by  $\lambda_0 + \Delta\lambda/2$ ;

(d) Output pulse.

## ● Waveguide Dispersion (波导色散)

- > Waveguide dispersion is one of major components of chromatic dispersion in singlemode fibers. (占重要部分)
- > Pure waveguide dispersion occurs merely from restricting light within a certain structure.
- > Waveguide dispersion depends on the mode-field distribution between the core and the cladding. (Dependent on wavelength !)



● Chromatic dispersion in a singlemode fiber

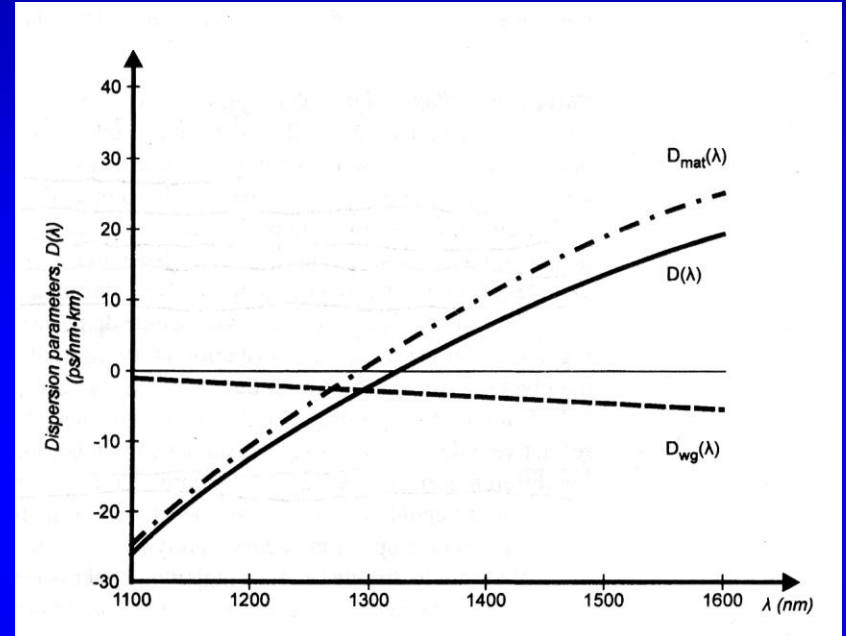
$$D = D_{mat} + D_{wg}$$

Basic Properties:

(1)  $D_{mat} < 0$ , when  $\lambda < 1300\text{nm}$ ;

$D_{mat} > 0$ , when  $\lambda > 1300\text{nm}$ .

(2)  $D_{wg} < 0$  and  $|D_{wg}|$  increase with  $\lambda$ .



-> The material and waveguide dispersion cancel with each other, which results in a zero-dispersion wavelength occurs around 1310nm.

(零色散波长)

## ⊙ Question:

**How to explain  $D_{wg} < 0$  in the single-mode fiber ?**

It means: 
$$\frac{d}{d\lambda} \left( \frac{1}{v_g} \right) < 0 \Rightarrow \frac{dv_g}{d\lambda} > 0$$

or,  $v_g$  increase with  $\lambda$ .

Indeed, the guided mode will spread to cladding with increasing of wavelength  $\lambda$ .

From the structure of optical fiber, one can learn that

$$c/n_2 > c/n_1 \longrightarrow \lambda \uparrow, v_g \uparrow$$

## ☉ Example:

Dispersion of singlemode optical fibers

$$\lambda_0 = 1.31\mu m, \quad \Delta\lambda = 1nm, \quad L = 1km$$

$$D = -2 ps / nm \cdot km$$

$$|\Delta t| = D\Delta\lambda L = 0.002ns$$

*Comparing to multimode optical fiber:*

Step-index:  $\Delta t \sim 5.6ns / km$

Graded-index:  $\Delta t \sim 0.21ns / km$

## ◆ Conventional, Dispersion-Shifted, and Dispersion-Flattened Fibers (常规, 色散位移, 色散平坦光纤)

One has learned:

$$\lambda \sim 1.31 \mu m \quad D \approx 0$$

$$\lambda \sim 1.55 \mu m \quad D \sim 15 \text{ ps} / \text{nm} \cdot \text{km} \text{ (but, with minimum attenuation!)}$$

Problem: How to decrease the dispersion around  $\lambda \sim 1.55 \mu m$

$$D = D_{mat} + D_{wg}$$

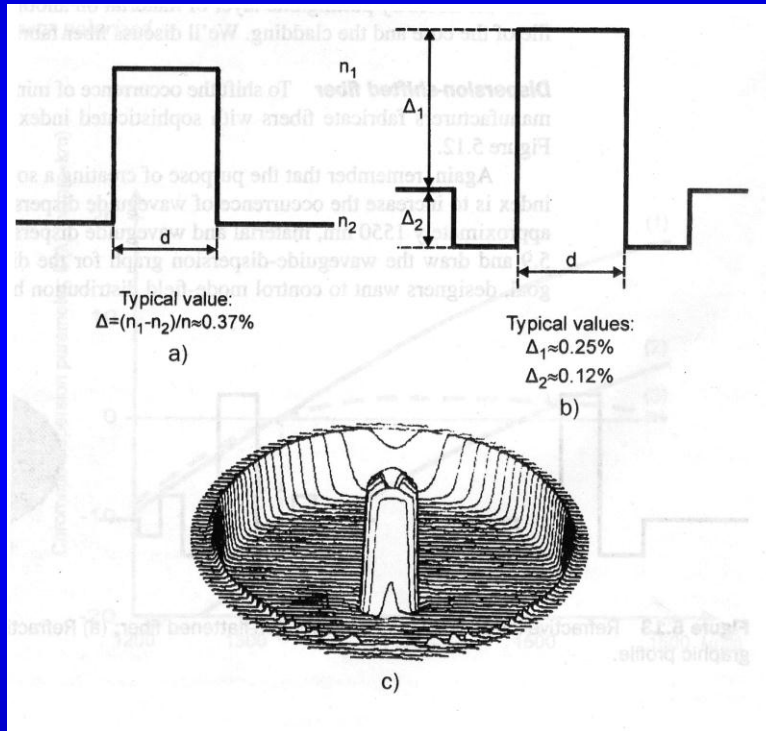
$D_{mat}$ : is difficult to be changed

$D_{wg}$ : depends on fiber structure, which can be changed

Effective way:  $\longrightarrow$  change fiber structure  $D_{wg} \approx -D_{mat}$



- Conventional Fibers : zero-dispersion wavelength is around 1300 nm.



a) matched cladding fiber  
( 匹配包层光纤 )

b) depressed cladding fiber  
( 凹陷包层光纤 )

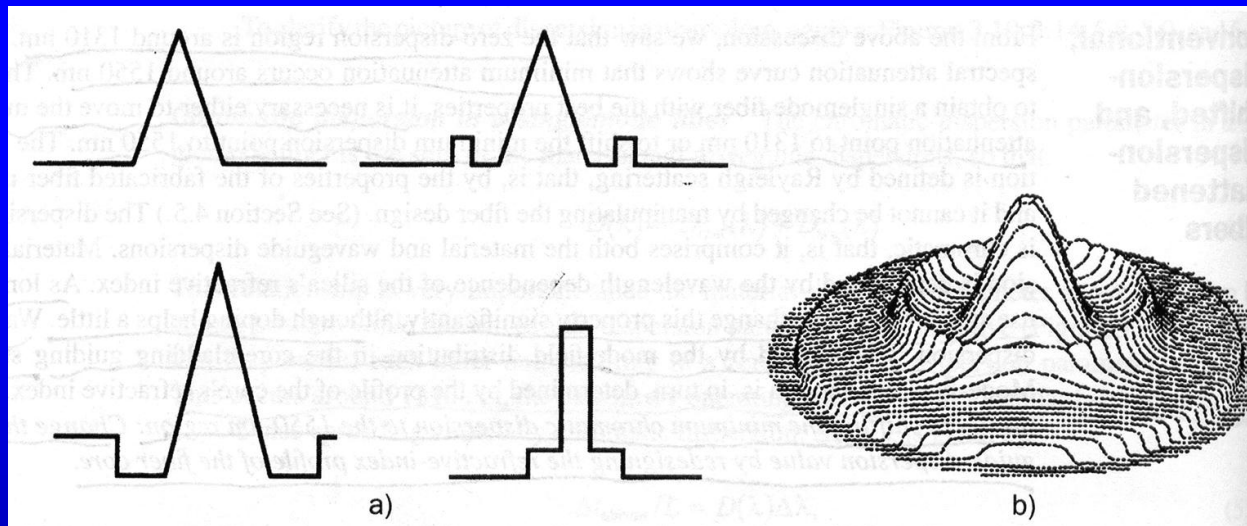
-> to reduce coupling to  
*cladding modes*

- Dispersion-Shifted Fibers (色散位移光纤)

-> To shift the minimum dispersion, designers can control *mode-field distribution* by changing the profiles of the core and cladding.

-> The triangular-shaped core refractive index is the most popular.

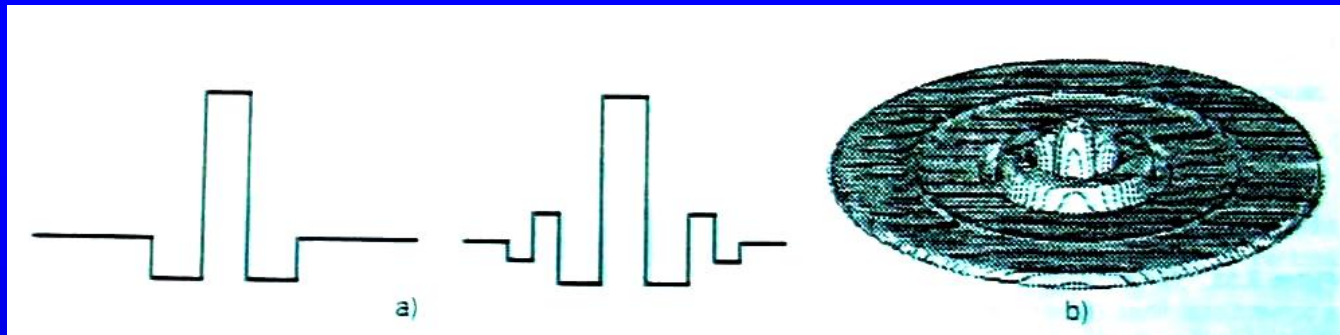
(三角形芯层折射率分布)



- Dispersion-Flattened Fibers (色散平坦光纤)

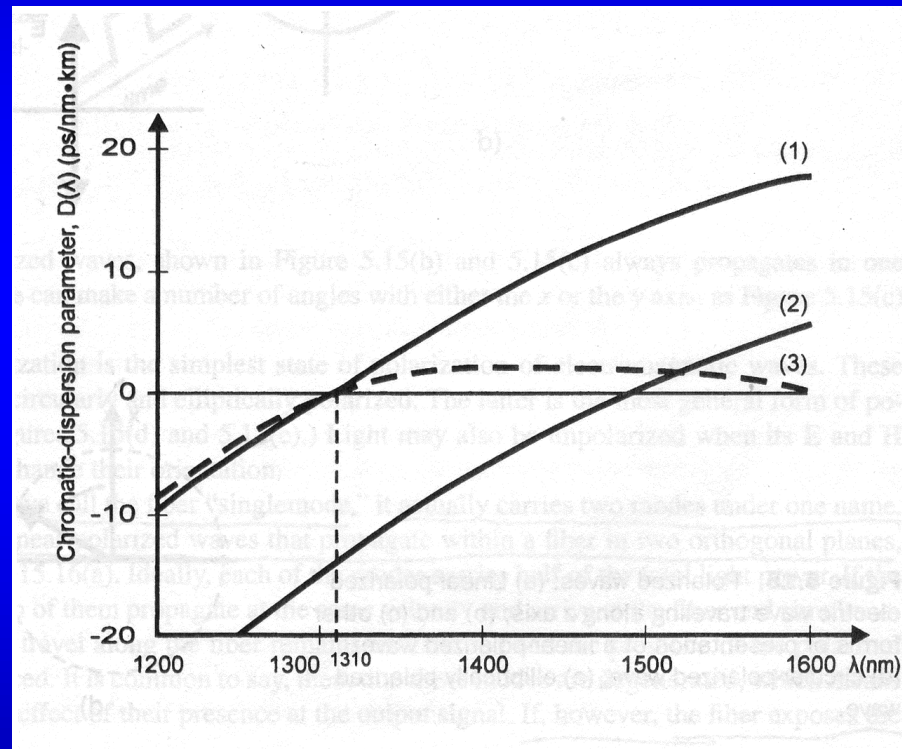
-> WDM system need the zero-dispersion property distributed along a region of wavelengths.

-> In 1988, it is made out by Philips Ltd.. (飞利浦公司)



## Chromatic-Dispersion Parameters

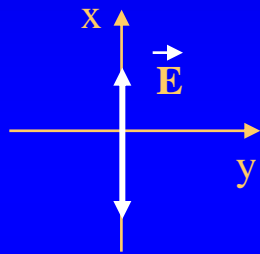
for (1) conventional, (2) dispersion-shifted, (3) dispersion-flattened fibers



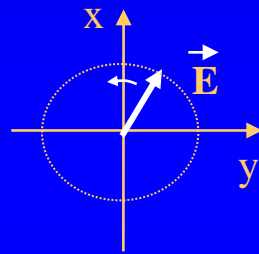
## ◆ Polarization-Mode Dispersion (PMD) (偏振模色散)

-> **Ideal circular optical fibers:** (*without birefringence* 没有双折射)

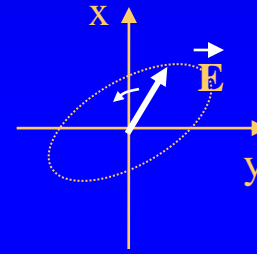
- (1) Fundamental mode is linear polarized; (线偏振)
- (2) Propagation in optical fiber is independent on polarization



(a)



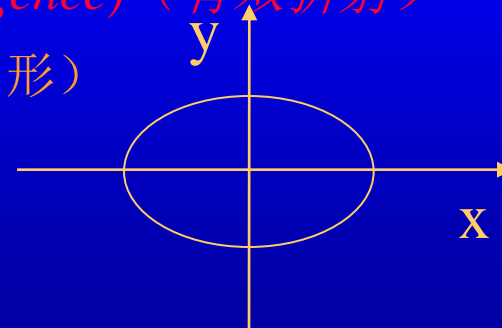
(b)



(c)

-> **Real optical fiber:** (*with birefringence*) (有双折射)

- (1) existence of non-circularity; (非圆形)
- (2) close to elliptic shape. (椭圆形)



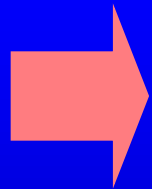
Input arbitrary polarized pulse:

$$\vec{E} = E(\hat{x} \cos \theta + \hat{y} \sin \theta)$$

LP<sub>01</sub>: HE<sub>11</sub>\*2

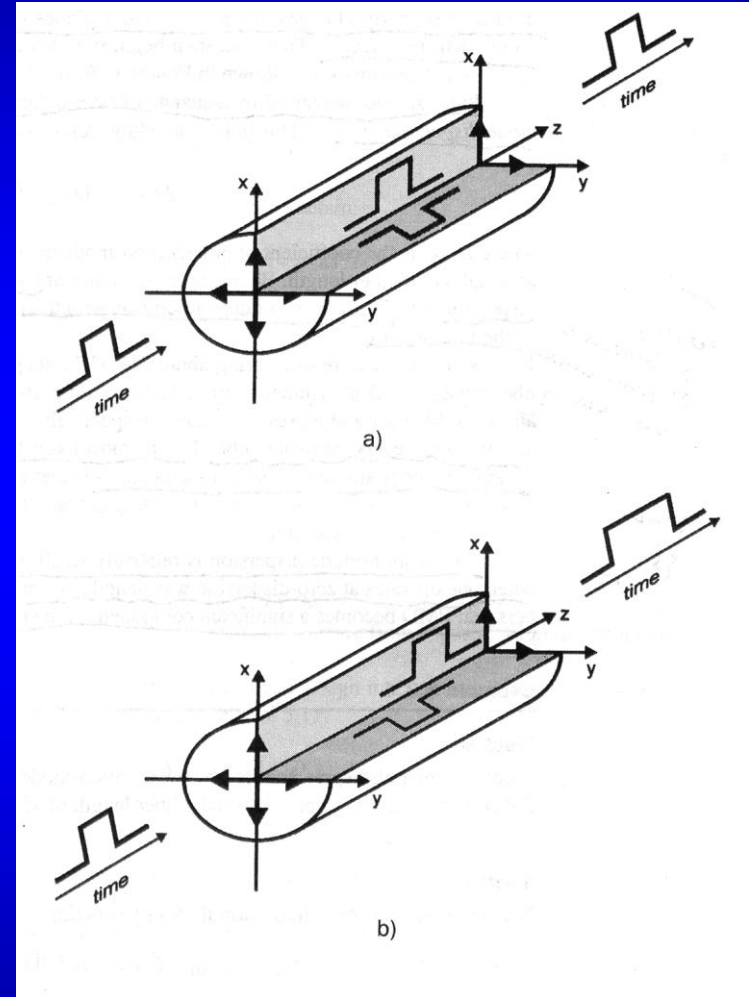
Excite two linear-polarizations of signal pulse to propagate with different velocities (不同速度)

$$\beta_x \neq \beta_y$$



Pulse spreading (脉冲展宽)

***Polarization Mode Dispersion (PMD)***



## -> Causes of PMD

Some asymmetry induced by the stress from fabrication, cabling process, external force, bending, etc. (引入非对称)

-> **PMD is a stochastic process!** (随机过程)

$$\Delta t_{PMD} \approx D_{PMD} \sqrt{L} \quad (\text{statistical result}) \quad (\text{统计结果})$$

->  **$D_{PMD}$  does not depend on operation wavelength!**

->  **$D_{PMD}$  does depend on the square root of the fiber length!**

## ◆ Bandwidth of a Singlemode Fiber (带宽)

$$BR < \frac{1}{4\Delta t}$$

-> SMF:  $\Delta t = D(\lambda)\Delta\lambda L \Rightarrow BR = 1/(4D\Delta\lambda L)$

: Example-1:

$$\lambda_0 = 1310 \text{ nm}, \quad \Delta\lambda = 1 \text{ nm}, \quad BR_{chrom}|_{1300 \text{ nm}} = ?$$

$$D = -2 \text{ ps} / \text{nm} \cdot \text{km}$$

$$BR_{chrom} \times L = 1 / (4 \times 2 \text{ ps} / \text{nm} \cdot \text{km} \times 1 \text{ nm}) = 125 \text{ Gbps} \cdot \text{km}$$

$$\Rightarrow BR_{chrom} = 1.25 \text{ Gbps} \quad (\text{for } 100 \text{ km link})$$

: Example-2:

$$D_{PMD} = 0.5 \text{ ps} / \sqrt{\text{km}}, \quad BR_{chrom}|_{1300 \text{ nm}} = ?$$

$$BR_{PMD} = 1 / (4 \times \Delta t) = 1 / (4 \times 5 \text{ ps}) = 50 \text{ Gbps} \quad (\text{for } 100 \text{ km})$$



# Homework

- 5.5, 5.6, 5.13, 5.17, 5.18

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