Chapter 3 Optical Fibers – (Multimode) Basics

> How to conduct light ?
> Attenuation (衰减) ?
> Dispersion (色散) ?
> Bandwidth (带宽) ?

# History

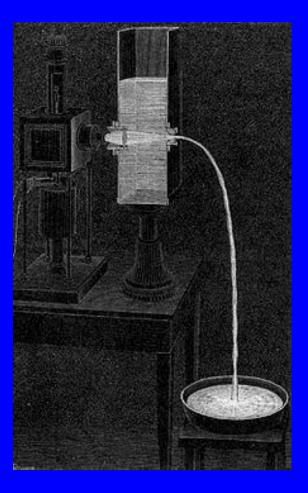
- > Although glass fibers were made in the 1920s, their use became practical in the 1950s when the cladding layer was used.
- > In 1966, 高錕 suggested to reduce the loss of optical fiber for fiber-optic communications.
- > In 1970, Corning Ltd. fabricated the step-index optical fiber.
- In 1972, the attenuation of optical fiber was improved from 20dB/km to <u>4 dB/km</u> with the improvement of material and fabication procedure.
- Further progress resulted by 1979, the loss of fiber was reduced to be only 0.2dB/km near the 1.55-um spectral region.



### **3.1 How optical fibers conduct light**

**Daniel Colladon** first described this "light fountain" or "light pipe" in an 1842 article titled *On the reflections of a ray of light inside a parabolic liquid stream*. This particular illustration comes from a later article by Colladon, in 1884.

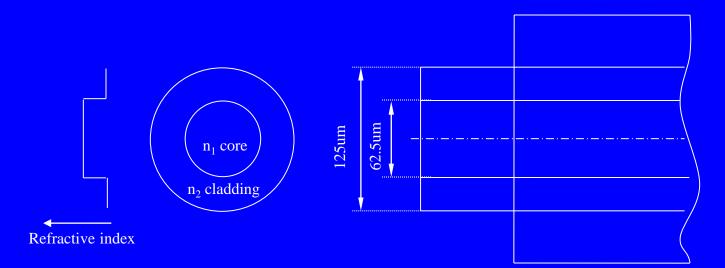
What's the principle?



### ◆ Step-Index Fiber (阶跃光纤) Bare Fiber: Fiber Core + Cladding + Coating

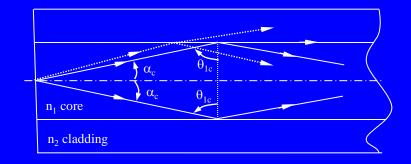
Core: Doped silica  $\rightarrow n_1$ Cladding: Pure SiO<sub>2</sub>  $\rightarrow n_2$ Coating: Plastic or carbon

To achieve TIR:  $n_1 > n_2$ 



### ◆ Total Internal Reflection (全内反射)

Critical incident angle:  $\theta_{lc}$ (临界入射角) Critical propagation angle:  $\alpha_c$ (临界传播角)



To save light inside an optical fiber, the propagation angle of rays should have

$$\alpha_z \leq \alpha_c$$

From Snell's Law, one has:

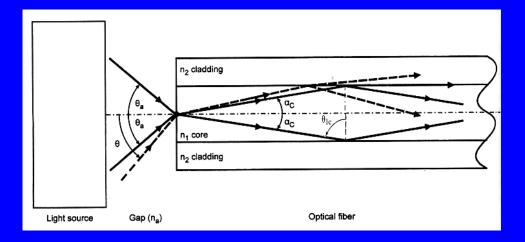
sin  $\theta_{1c} = n_2/n_1$ , and cos  $\alpha_c = n_2/n_1$ .

Thus, one can derive:

$$a_c = \sin^{-1} \sqrt{[1 - (n_2 / n_1)^2]}$$

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### Launching the Light



Critical incident angle:  $\sin \theta_{1c} = \frac{n_2}{n_1}$ Critical propagation angle:  $\alpha_c = \sin^{-1} \sqrt{1 - \left(\frac{n_2}{n_1}\right)^2}$ -> Acceptance angle (接收角):  $\theta_a$  or  $2 \theta_a$  $\sin \theta_a = n_1 \sin \alpha_c$ 

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### ◆ Numerical Aperture (数值孔径)

 $NA = \sin \theta_a$ : Describe the ability of an optical fiber to gather light from a source, and preserve this light insider the fiber.

 $= n_1 \sin(\alpha_c)$ 

$$= n_1 \sqrt{(1 - (\frac{n_1}{n_2})^2)} = \sqrt{(n_1)^2 - (n_2)^2}$$

 $n = (n_1 + n_2)/2$  : Average refractive index.

 $\Delta = (n_1 - n_2) / n$  : Relative difference of the refractive indexes.

->  $NA = n\sqrt{2\Delta}$ 

:  $n_1$  and  $n_2$  are not important in themselves, but only in their average and relative difference.

### Example:

Type-1:  $n_1 = 1.48$  $n_2 = 1.46$  $\frac{\Delta n}{2} = 1\%$ n  $\Theta_{1C} = 80.57^{\circ}$  $\alpha_c = 9.43^{\circ}$  $\Theta_a = 14.033^{\circ}$ 

NA = 0.2425

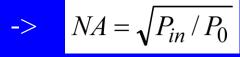
Type-2:  $n_1 = 1.495$  $n_2 \approx 1.402$  $\frac{\Delta n}{m} \approx 6\%$ n  $\Theta_{1C} = 69.68^{\circ}$  $\alpha_{c} = 20.32^{\circ}$  $\Theta_a = 31.27^{\circ}$ 

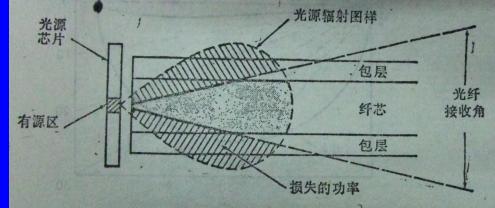
NA = 0.5192



-> for a fiber launched by a LED source (Lambertian source: 朗伯光源)

 $P(\theta) = P_0 \cos \theta$  $\frac{P_{in}}{P_0} = \frac{\int_0^{2\pi} \int_0^{\theta_a} P_0 \cos \theta \sin \theta d\theta d\varphi}{\int_0^{2\pi} \int_0^{\frac{\pi}{2}} P_0 \cos \theta \sin \theta d\theta d\varphi} = \frac{\sin^2 \theta_a}{\sin^2 \frac{\pi}{2}} = (NA)^2$ 





### Question :

Numerical aperture, NA, is the characteristic of an optical fiber to gather light from a source.

When the core diameter is larger, NA should be

a. larger

b. smaller

c. the same



# **Nobel Prize in Physics**

In 1965, Charles K. Kao with Hockham concluded that the fundamental limitation for glass light attenuation is below **20** *dB/km* (*decibels per kilometer*, is a measure of the attenuation of a signal over a distance), which is a key threshold value for optical communications.

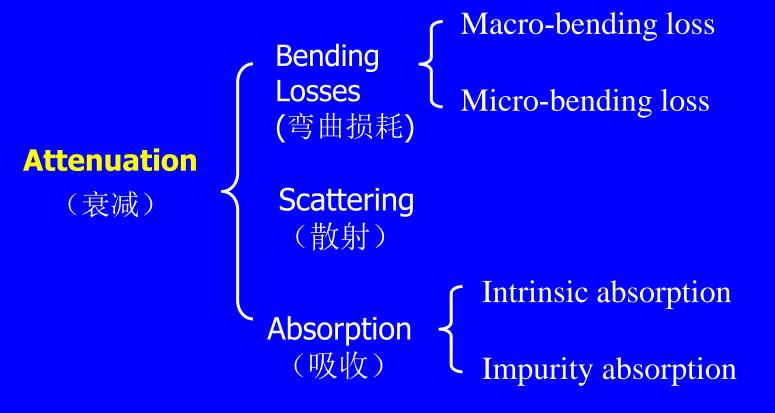




Attenuation !!

## **3.2 Attenuation**

: power loss for reasons other than failure to achieve total internal reflection.



### Bending loss

-> The flexibility of optical fiber is an advantage, but it brings some problems too!-> It will induce the failure of TIR.

### • Macro-bending:

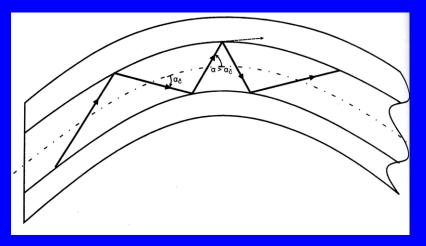
The curvature of the entire fiber changes the propagation angle to be more than critical angle.

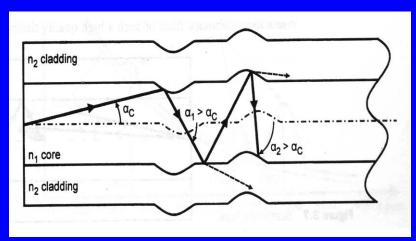
-> minimum bending radius: 19mm or 13mm

### • Micro-bending:

The microconvexity or microdent will change the propagation directions.

-> coating or external force 2012/4/3





### Scattering loss

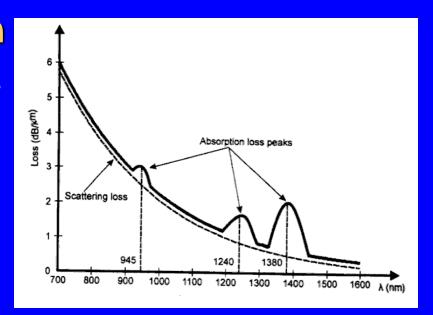
Change of propagation direction induced by small changes in the core's refractive index

-> induce the failure of TIR again

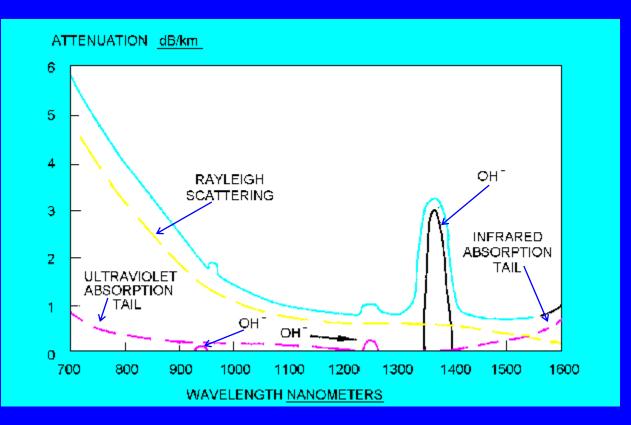
Rayleigh scattering :  $\infty \lambda^{-4}$ 

### (Material) Absorption

OH<sup>•</sup> molecules: 3 absorption peaks Transparent windows: 850 nm: 4 dB/km 1300nm: 0.5 dB/km 1550 nm: 0.3 dB/km



### Attenuation of Optical Fibers



->: Dry fiber (无水光纤), or all-wave fiber (全波光纤), is optical fiber which hydroxide anion is eliminated.

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### Calculation of Total Attenuation

\_● Loss in linear or decibels (分贝): (fiber, devices, …)

 $Loss = \frac{P_{out}}{P_{in}}$  $Loss(dB) = -10\log_{10}(\frac{P_{out}}{P_{in}}) \quad : \text{ notice the minus sign!!}$ 

Attenuation (loss) per fiber-length : (fiber!)
 (also called "Attenuation", cable-loss factor, attenuation coefficient)

$$A(dB / km) = \frac{loss(dB)}{fiberlength(km)}$$
$$p_{out} = p_{in} \times 10^{-\frac{AL}{10}}$$

• Maximum transmission distance

$$L = (\frac{10}{A}) \log_{10}(\frac{P_{in}}{P_{out}})$$

- -> the maximum transmission distance imposed by attenuation,
  -> the minimum value of P<sub>out</sub> is determined by the sensitivity of the receiver
- **Power unit** *dBm* : choose 1mW as the reference power

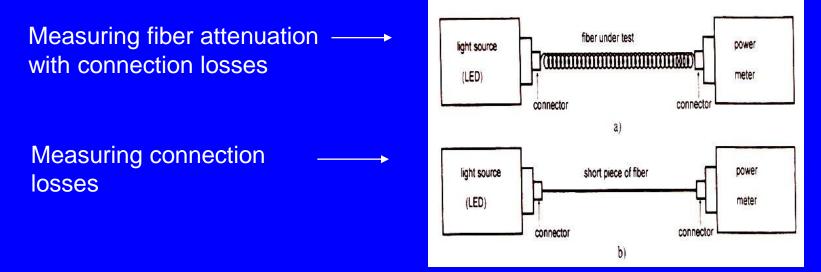
 $P_{out}(dBm) = +10\log(P_{out} / 1mW)$ 

(line 4, p. 56)

P55, Paragraph 2 from the second section: "First, it is a key....."

### Measuring Attenuation

### Cut Method (截断法)



 $Loss(dB) = P_{in}(dBm) - P_{out}(dBm)$ 

-> Measure the powers when the device under the test is "in and out".

#### More about Cut Method (截断法):

-> The precision of this method is mainly determined by two factors:

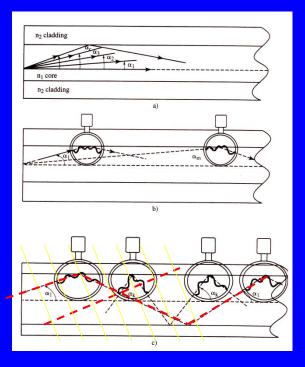
(a) How accuracy you can reproduce connection losses(b) How negligible is the attenuation introduced by a short piece of fiber.

-> When measuring attenuation in a multimode fiber, special care should be taken to use a light beam filling the entire cross-sectional area of the core (called overfilled launching) to make sure that (all possible modes are excited).

# **3.3 Intermodal and Chromatic Dispersion**

Optical signal:-> Pulse width, bandwidth -> distortion?

◆ Modes (模式)



- -> Modes as different beams with different propagation distances.
- -> Different beams experience different phase shifts (1. Different phase fronts.
  2. Reflection phase shift.)
- -> Optical fiber supports only those modes that complete the full zigzag at the same repeated phase (stable!). The other one is not stable.

Wave  $\alpha_1$  reproduces itself after the whole cycle of propagation, but wave  $\alpha_k$  does not.

### More about Modes :

- -> These different beams with different propagation angles are called **modes**.
- -> We distinguish modes by their propagating angles and we use the word **order** to designate the specific mode.
- -> The smaller the mode's propagating angle, the lower the order of the mode.
- -> The zero-order mode is also called fundamental mode.
- -> The mode traveling at critical propagation angle is the highest order mode possible for this fiber.

### ◆ V-number (V参数,归一化截止频率)

(Normalized cut-off frequency, characteristic waveguide parameter)

$$V = \frac{\pi d}{\lambda} NA$$

-> More light can be accommodated for larger core diameter d, larger NA and shorter wavelength

$$V = \frac{\pi d}{\lambda} \sqrt{\left(n_1\right)^2 - \left(n_2\right)^2}$$

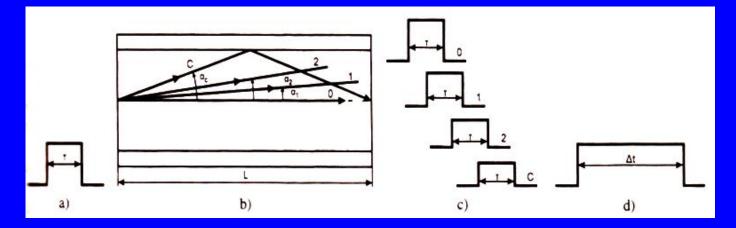
For a large V number ( >20 ), the number of modes can be estimated by

 $\boxtimes$  Step-index fiber:  $N = \frac{V^2}{2}$ 

 $\boxtimes$  Graded-index fiber:  $N = \frac{V^2}{4}$ 

### ◆ Intermodal dispersion (模间色散)

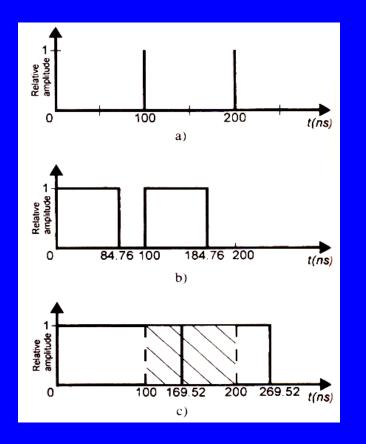
(different modes travels at different speeds)



a) Original pulse;b) Modes in an optical fiber;c) Pluses delivered by an individual mode;d) Resulting pulse

- -> The zero-order (fundamental) mode needs time :  $t_0 = \frac{L}{v}$ ,  $v = c/n_1$ ;
- -> The highest-order (critical) mode needs time :  $t_c = \frac{L}{v \cos \alpha_c} (\cos \alpha_c = \frac{n_2}{n_c})$
- E> Pulse spreading (脉冲展宽) stemming from intermodal dispersion:  $\Delta t_{SI} = t_c - t_0 = \frac{L}{2cn_2} (NA)^2$  : NA=0.275,  $n_1 = 1.487 \Rightarrow \Delta t/L = 84.76$  ns/km

### Restriction on Bit Rate



#### a) Input pulses;

Bit rate : 10Mbit/s, =>time cycle duration : 100 ns

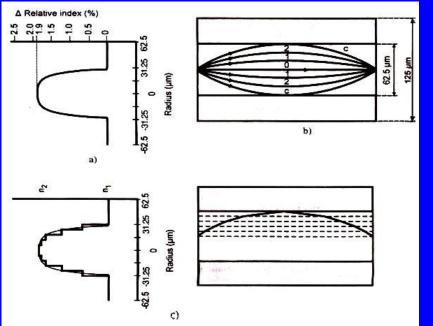
b) Pulses after 1 km transmission Pulse spreading:  $\Delta t = 84.76$  ns

c) Pulses after 2 km transmission

-> The maximum bit rate (for a transmission of 1 km) =  $1/\Delta t = 11.8$ Mbit/s.

-> Larger L => larger  $\Delta t$  => smaller bit rate.

### ◆ First Solution: Graded-index Fiber (渐变光纤)



a) Refractive index profile

b) Mode propagation

c) Principle of action (fabrication) of graded index multimode fiber.

-> The refractive index of fiber core varies with the radius;

-> The beam traveling the farthest distance has the highest velocity and the beam traveling the shortest distance propagates at the slowest velocity.

#### Calculating pulse spreading for graded-index fiber

 $\Delta t_{GI} = (LN_1\Delta^2)/(8c)$  \* where N<sub>1</sub> is core group index of refraction ->  $n_1$  is a variable, i.e.  $n_1(r)$ 

$$\Delta t_{GI} = \frac{(LNA^4)}{(32cN_1^3)}$$

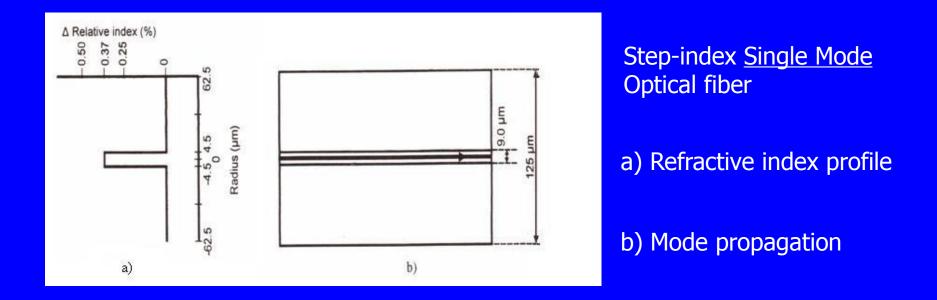
where approximation  $n_1 = N_1$  was used.

$$\Delta t_{GI} = \Delta t_{SI} \left(\frac{\Delta}{8}\right)$$

: A graded-index fiber has a modal dispersion  $\Delta/8$  times less than that of a step-index fiber.

\* Joseph C. Palais, Fiber Optic Communications, 4th ed., Englewood Cliffs, N.J.: Prentice Hall, 1998.

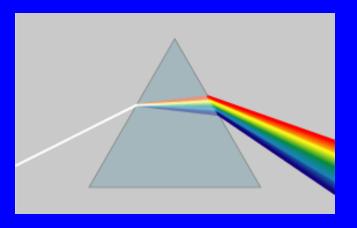
### ◆ A Better Solution : Single-mode Fiber (单模光纤)



-> Typically, the core diameter d is 8.3 um and the relative index  $\Delta$  is 0.37%. (for multimode fiber, d is around 62.5 um, and  $\Delta$  is 2%)

-> A real single-mode condition is :  $V \le 2.405$ 

### ◆ Chromatic Dispersion (色度色散)



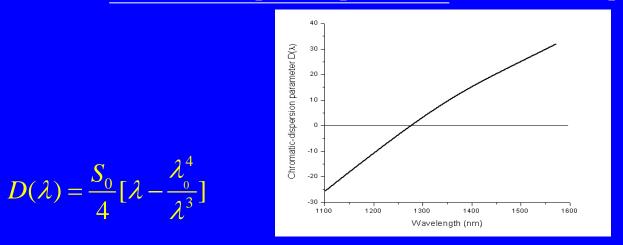


- -> Refractive index depends on wavelength,  $n = n(\lambda)$
- -> The velocity of light within a material is: v = c/n
- -> The light with different wavelength travels along the fiber at different velocities.
- -> They will arrive at the receiver end at different times, even if all of these beams propagates along the same path.

#### Calculating pulse spreading

 $\Delta t_{chrom} = D(\lambda) \cdot L \cdot \Delta \lambda$ 

where  $D(\lambda)$  is the chromatic-dispersion parameter (色散参数) in ps/nm.km.



 $-> \lambda_0$  is the zero-dispersion wavelength : the wavelength at which D( $\lambda$ ) is zero.

-> S<sub>0</sub> is the zero-dispersion slope in ps/(nm<sup>2</sup>.km).

Total pulse spreading caused by modal and chromatic dispersion

$$\Delta t_{total} = \sqrt{(\Delta t_{modal}^2 + \Delta t_{chrom}^2)}$$

### 3.4 Bit Rate (比特率) and Bandwidth (带宽)

• **Bit rate:** The number of bits that can be transmitted per second over a channel.

$$BR = \frac{1}{T}(Hz)$$
 : T — time interval between adjacent signals.

• **Bandwidth:** The frequency range within which a signal can be transmitted without significant deterioration.

BW = BR or, BW = BR/2

which depends on the line codes, such as the non-return to zero (NZR) etc..

### Dispersion and Bit Rate

for a practical standpoint, a coefficient 1/4 is general accepted in the industry.

 $BR < 1/(4\Delta t)$  i.e.  $T > 4\Delta t$ 

-> for a step-index multimode fiber, one has

 $\overline{BR}_{SI} = \frac{1}{(4\Delta t_{SI})} = \frac{c}{(4Ln_1\Delta)} = \frac{cn_2}{(2LNA^2)}$ 

-> for a graded-index multimode fiber, one has

 $BR_{GI} = 2c / (N_1 L \Delta^2)$ 

-> If considering chromatic dispersion, one has

 $BR_{chrom} = 1/(4D(\lambda)L\Delta\lambda)$ 

-> If considering the total bit rate, one has

$$BR_{total} = 1/4\sqrt{(\Delta t_{modal}^2 + \Delta t_{chrom}^2)}$$

### Reading a data sheet

Data sheet maybe different from each other, but four parts must be included.

- "Optical Characteristics" section
- "Geometric Characteristics" section
- "Environmental Specifications" section
- "Mechanical Specifications" section

### Homeworks

### **\***3.7, 3.12, 3.21, 3.22, 3.25, 3.29, 3.30, 3.33, 3.47

- **3.7** The core refractive index is 1.4513 and the cladding index is 1.4468. What is (1) the critical propagation angle? (2) the acceptance angle? (3) the numerical aperture?
- **3.12** For a specific fiber, NA = 0.2375 and n1 = 1.4860. Find  $n_2$  (n cladding).
- **3.21** What does the term "transparent windows" mean? Specify three peak wavelengths for the transparent windows in modern optical fibers.
- **3.22** An optical fiber with attenuation of 0.25 dB/km is used for 20-km transmission. The light power launched into the fiber is 2mW. What is the output power?
- 3.25 Find the maximum transmission distance for a fiber link with an attenuation of 0.3 dB/km if the power launched in is 3mW and the receiver sensitivity is 100 μW.

### Homeworks

- **3.29** What is the number of modes for a graded-index fiber if d is 50  $\mu$ m, NA is 0.200, and the operating wavelength is 1300 nm?
- **3.30** How many modes can support a step-index optical fiber whose  $d=8.3 \ \mu \ m, n_{1core}=1.4513, n_{2clad}=1.4468, and \lambda=1550 \ nm?$
- **3.33** Consider modal dispersion. For a step-index multimode fiber with *NA*=0.200 and *n*<sub>1</sub>=1.486: a) Evaluate pulse spreading per 1 km length; b) Calculate the maximum number of bits per second that can be transmitted over 1 km.
- **3.47** A graded-index fiber has n1 = 1.486 and NA = 0.200. What is the bit rate for a 1-km link?

### **Reference:**

- 1. Keiser, Gerd., <u>Optical fiber communications</u>, Publisher Boston, Mass. : McGraw-Hill, c2000.
- 2. G. P. Agrawal, <u>Fiber-optic communication systems</u>, Publisher New York : John Wiley, c2002
- 3. Haus, Hermann A., <u>Waves and fields in optoelectronics</u>, Publisher Englewood Cliffs, NJ : Prentice-Hall, c1984.

### **Contact:**

Dr. Shiming Gao Tel: 88206516-211 E-mail: gaosm@zju.edu.cn

