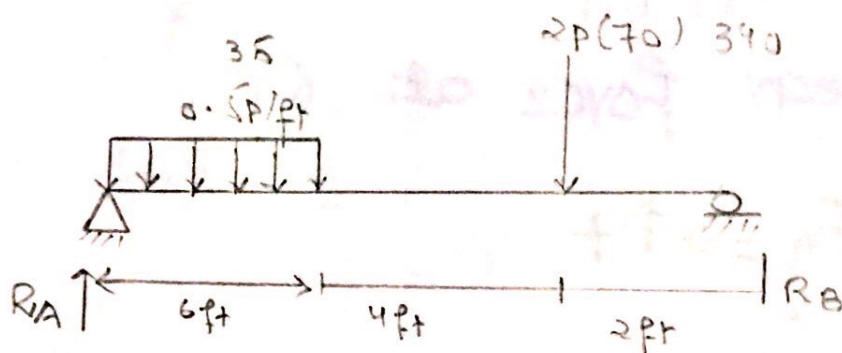
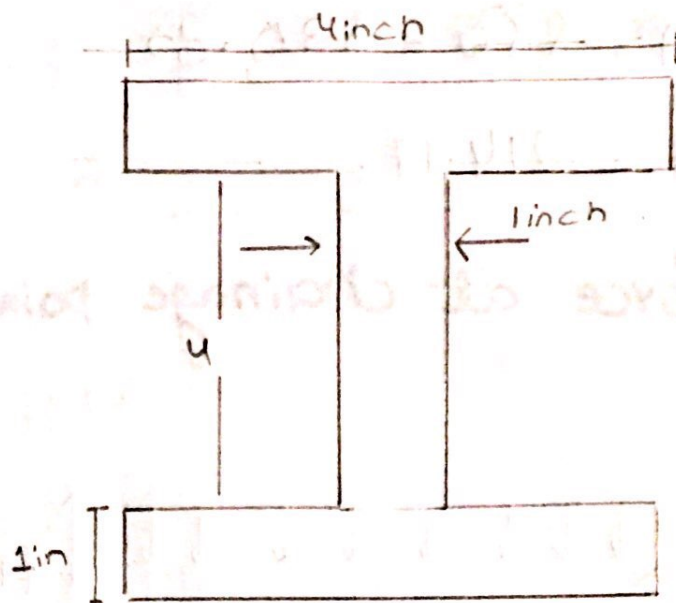


7970, Sec# B

1



$\Sigma F_y = 0$ ↑ + upward is positive

$$R_A + R_B = 35 \times 6 - 340 = 0$$

$$R_A + R_B = 550.$$

$\Sigma M_A = 0$ ↺ + Anticlockwise is positive.

$$R_B(12) - 340(10) - 35(6) \times 3 = 0$$

$$R_B(12) - 3400 - 630 = 0$$

$$R_B = \frac{4030}{12} = 335.83$$

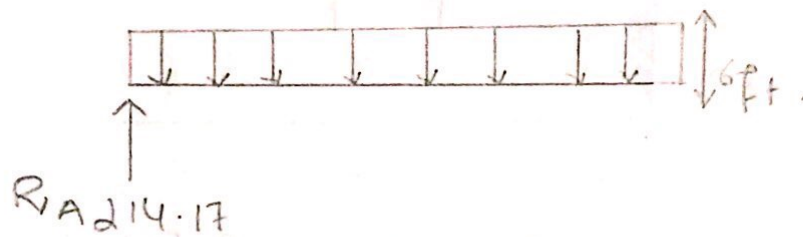
Now: *

$$R_B + R_A = 550$$

$$R_A = 550 - 335.83$$

$$R_A = 214.17$$

Now shear force at chainage point of Beam:



Shear force at 6 ft.

$$\sum F_y = 0 \uparrow +$$

$$-V_{6ft} + 214.17 - 35 \times 6 = 0$$

$$V_{6ft} = 4.17$$

$\sum F_y = 0$ Shear force at 10 feet.

$$214.17 - 35 \times 6 - 340 - V_{10ft} = 0$$

$$-335.83 = V_{10ft}$$

$$V_{10ft} = -335.83$$

Moment at Change Points: * #3
Find Zero shear point:

$$\frac{214.17}{x} = \frac{4.17}{6-x}$$

$$214.17(6-x) = 4.17x$$

$$1285.02 - 214.17x = 4.17x$$

$$1285.02 = 4.17x + 214.17x$$

$$1285.02 = 218.34x$$

$$x = \frac{1285.02}{218.34}$$

$$x = 5.8854$$

→ As we know that moment is max where shear force is zero.

Take section at 5.8854 from left support. And Find moment.

$$\sum M_{5.885} = 0 \curvearrowright +$$

$$M_{5.885} - 214.17(5.885) + 35 \times 6 \left(\frac{5.885}{3} \right) = 0$$

$$M_{\max} = M_{5.885} = 848.440$$

$$\Sigma M_{\text{left}} =$$

$$= -214.17 \times 6 + 35(6) \left(\frac{6}{3} \right)$$

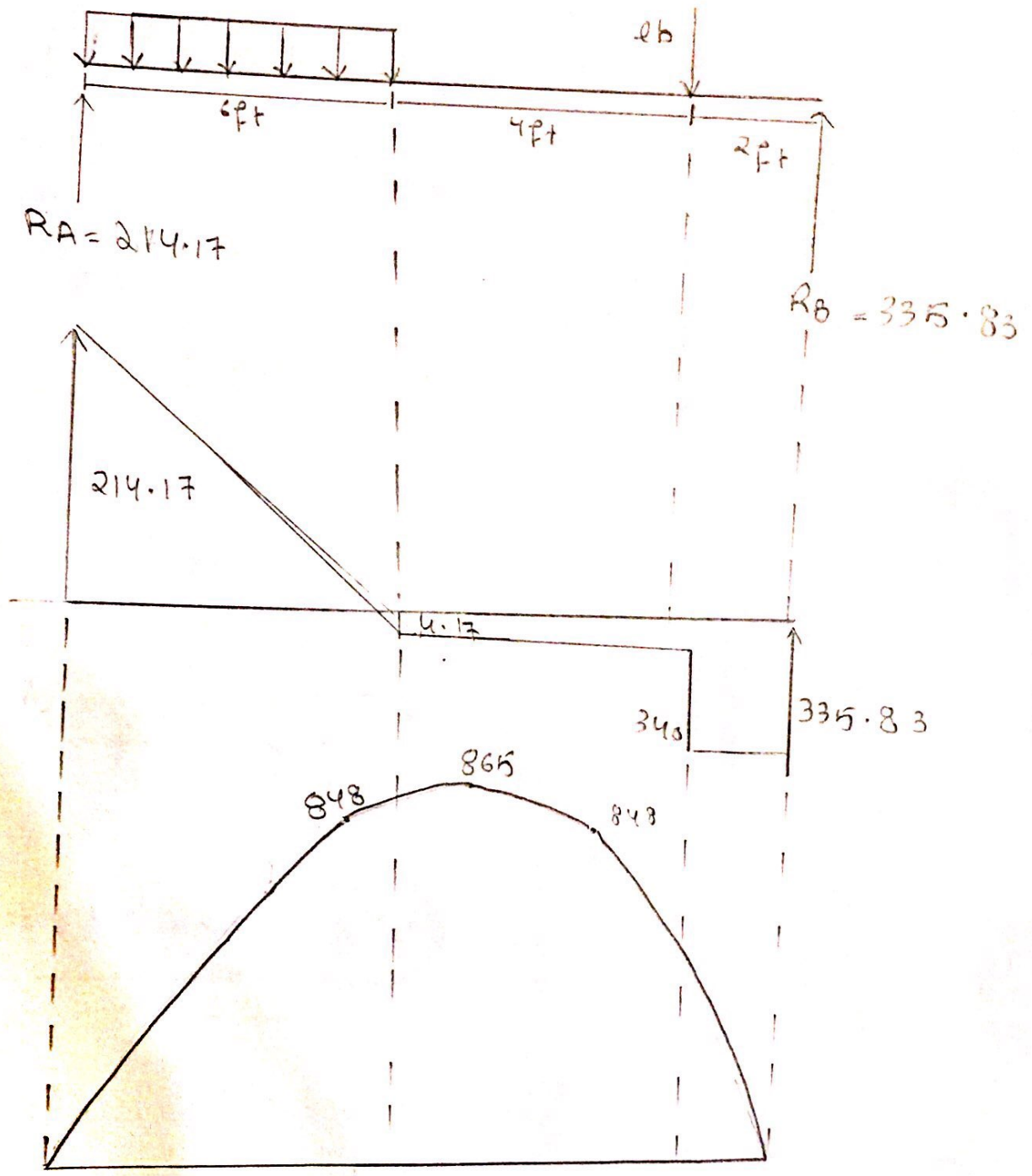
$$= 865.02$$

$\Sigma M_{\text{right}} = 0$ (Moment For Centre
uniformly distributed
load)

$$M/3 - 214.17(3) + 35(6)(3) = 0$$

$$M/3 - 642.51 + 630 = 0$$

$$M/3 = 12.51$$



Moment of Inertia :-

#15

$$\rightarrow y_1 = 5.5$$

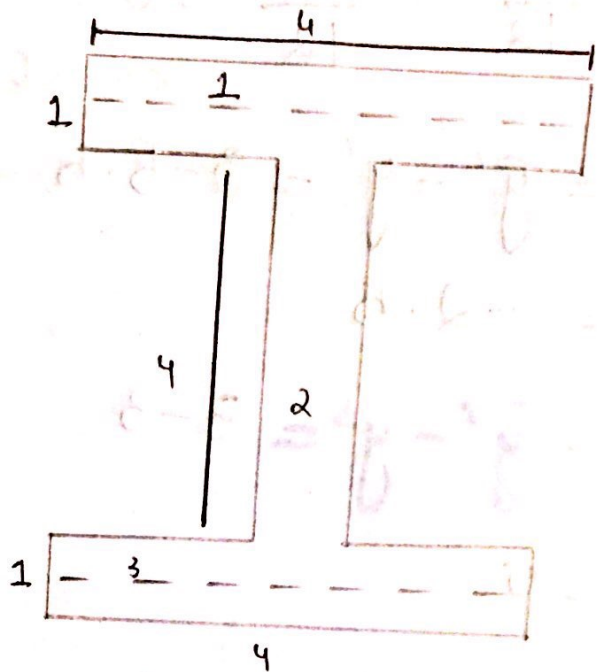
$$y_2 = 3$$

$$y_3 = 0.5$$

$$A_1 = 4 \text{ in}^2$$

$$A_2 = 4 \text{ "}$$

$$A_3 = 4 \text{ "}$$



$$\bar{y} = \frac{A_1 \times y_1 + A_2 \times y_2 + A_3 \times y_3}{A_1 + A_2 + A_3}$$

$$\bar{y} = \frac{4 \times 5.5 + 4 \times 3 + 4 \times 0.5}{4 + 4 + 4}$$

$$\bar{y} = 3''$$

$$I_1 = \frac{bh^3}{12} \Rightarrow \frac{4 \times 1^3}{12}$$

$$I_1 = 0.33 \text{ inch}^4$$

$$I_2 = \frac{bh^3}{12} \Rightarrow \frac{1 \times 4^3}{12}$$

$$I_2 = 5.33 \text{ inch}^4$$

$$I_3 = \frac{bh^3}{12} = \frac{4 \times 1^3}{12} = 0.33 \text{ inch}^4$$

$$d_1 = \bar{y}' - y' = 3 - 5.5$$

$$d_1 = -2.5$$

$$d_2 = \bar{y}' - y'' = 3 - 3$$

$$d_2 = 0$$

$$d_3 = \bar{y} - y''' = 2.5$$

→ I_x

$$I_{1x} = I_1 + A_1 d_1^2$$

$$I_{1x} = 0.33 + 25$$

$$I_{1x} = 25.33 \text{ inch}^4$$

$$I_{2x} = I_2 + A_2 d_2^2$$

$$I_{2x} = 5.33 + 0 = 5.33 \text{ inch}^4$$

$$I_{3x} = I_3 + A_3 d_3^2$$

$$I_{3x} = 0.33 + 25$$

$$I_{3x} = 25.33$$

$$I_{xx} = I_{1x} + I_{2x} + I_{3x}$$

#8

$$I_{xx} = 25.3 + 5.33 + 25.33$$

$$I_{xx} = 55.66 \approx 56 \text{ inch}^4.$$

$$\text{For } v = 335.83$$

Case No: 1*

$$\begin{aligned} \tau_{\text{Top Fiber}} &= \frac{V \phi}{I \cdot b} \\ &= \frac{335.83 \times 0}{56} \\ &= 0 \text{ psi} \end{aligned}$$

Case No 2A: For 1 inch below Top fiber

$$\begin{aligned} \tau_{1A} &= \frac{335.83 \times 10}{56(4)} \quad \therefore b = 4 \\ &= 7.09 \text{ psi} \quad 14.95 \text{ psi} \end{aligned}$$

Case No 2B:*

$$\tau_{1B} = \frac{335.83 \times 10}{56(1)} \quad \therefore b = 1$$

$$\tau_{1B} = 59.83 \text{ psi}.$$

$$\sigma = \frac{My}{I}$$

#9

$$\text{Moment} = 865.02$$

$$\text{Moment of Inertia} = I = 56$$

Case No: 1 (Stress at top fiber)

$$\begin{aligned}\sigma_{\text{top}} &= \frac{My}{I} \\ &= \frac{865.02 \times 3}{56} \\ &= 46.340 \text{ psi}\end{aligned}$$

Case No: 2 (1 inch below top fiber)

$$\begin{aligned}\sigma_1 &= \frac{My}{I} \\ &= \frac{865.02 \times 2}{56} \\ &= 30.89 \text{ psi}\end{aligned}$$

Case No: 3 Stress At Centroidal Axis

$$\tau_{\text{max}} = \frac{VQ}{Ib}$$

$$\phi = \phi_1 + \phi_2$$

$$\phi = (10 + 1(2))$$

10

$$\phi = 12$$

So,

$$\tau_{\max} = \frac{335 \cdot 083 \times 12}{56(1)}$$

$$= 71.8035 \text{ psi}$$

Case No 4A: - * 1 inch Above Bottom

$$\tau_{2A} = \frac{V\phi}{It} \quad \dots b = 4$$

$$= \frac{335 \cdot 083 \times 10}{56 \times 4}$$

$$= 14.95$$

Case No 4B: *

$$\tau_{2B} = \frac{V\phi}{It} \quad \dots b = 1$$

$$u = \frac{335 \cdot 083 \times 10}{56 \times 1}$$

$$u = 59.83$$

Case No 3: (At Geometrical Centroid) # 11

$$\sigma_{\text{centre}} = \frac{My}{I} \quad \therefore y = (0)$$

$$= 0 \text{ psi}$$

Case No 4: * (1 inch above the bottom fiber)

$$\sigma = \frac{865 \cdot 0.2 \times 2}{56}$$

$$\sigma = 30.89 \text{ psi}$$

Case No: 5 * At Bottom fiber.

$$\sigma_{\text{Bottom}} = \frac{My}{I}$$

$$\sigma_{\text{Bottom}} = \frac{865 \cdot 1.502 \times 3}{56}$$

$$= 46.36 \text{ psi}$$

Case 5: * At Bottom fiber.

12.

$$\tau_B = \frac{V\phi}{It}$$

$$\tau_B = \frac{335.083 \times 0}{56(4)}$$

$$\tau_B = 0 \text{ psi.}$$

Case 6: *

Shear force at 6 ft from left support.

$$V_{6ft} = 4.17$$

$$\phi = 12.$$

$$\tau_{max} = \frac{4.17 \times 12}{56 \times 1}$$

$$\tau_{max} = 0.8935 \text{ psi.}$$

Case No: 7* (At a distance ^{# 13} & 1 inch below

→ For $b = 4$

$$\tau_A = \frac{4.17 \times 10}{56(4)}$$

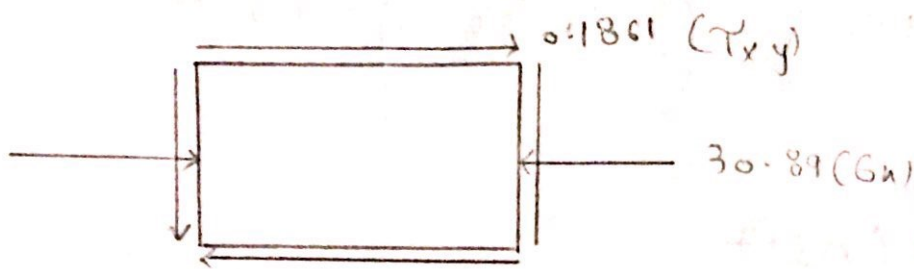
$$= 0.1861 \text{ psi}$$

→ For $b = 1$

$$\tau_B = \frac{4.17 \times 10}{56 \times 1}$$

$$= 0.7446 \text{ psi}$$

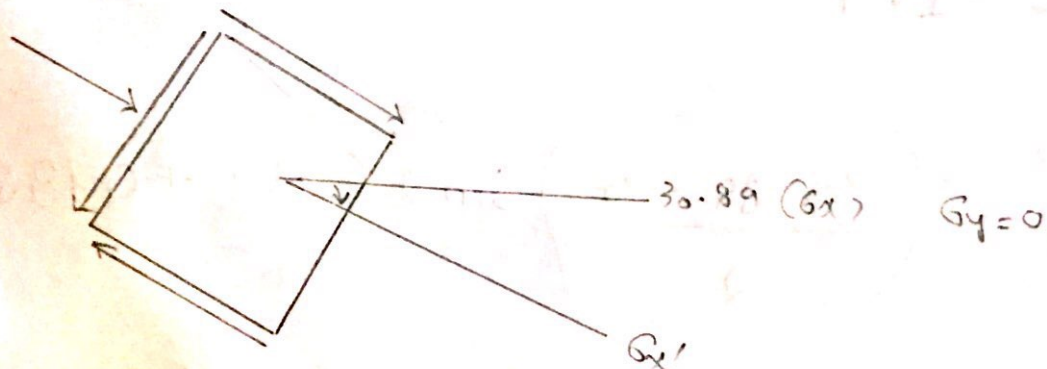
Shear Stress Transformation: #14



$$\sigma_{av} = \frac{\sigma_x + \sigma_y}{2} = \frac{30.89 + 0}{2}$$

$$\sigma_{av} = 15.445$$

Let θ Assume = -15°



$$\sigma_{x'} = \frac{-30.89 + 0}{2} + \left(\frac{-30.89 - 0}{2} \right) \cos 2\theta + 0.1861 \sin 2\theta$$

$$\sigma_{x'} = -15.445 - 15.445 (0.886) + 0.1861 (-0.5)$$

$$G_x = -29.2 \quad \#145$$

$$G_y' = \left(\frac{-30.89 + 0}{2} \right) - \left(\frac{-30.89 - 0}{2} \right) \cos 2\theta \\ - 0.1861 \sin 2\theta$$

$$G_y = -15.445 + 15.445 (0.866) - 0.1861 (-0.5)$$

$$G_y' = -1.9$$

$$T_u' y' = - \left(\frac{-30.89 - 0}{2} \right) \sin 2 (-15^\circ) + 0.1861 \cos 2(-15^\circ)$$

$$= 15.445 (-0.5) + 0.1861 (0.866)$$

$$= -7.5$$

PRINCIPLE STRESS:*

$$\tan 2\theta_p = \frac{\tau_{xy}}{\sigma_x - \sigma_y / 2}$$

$$\tan 2\theta_p = \frac{0.1861}{15.445}$$

$$\tan 2\theta_p = -0.012$$

$$\theta_p = \tan^{-1} \left(\frac{-0.012}{2} \right)$$

$$\theta_p = \tan^{-1} (-0.06)$$

$$\theta_p = -3.43$$

Now \rightarrow

$$\sigma_n' = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$\sigma_n' = \frac{-30.89 + 0}{2} + \left(\frac{-30.89}{2} \right) \cos 2(-3.43) + 0.1861 \sin 2(-3.43)$$

#17.

$$\sigma_{u'} = -15.445 - 15.445(0.99) + 0.1861(-0.11)$$

$$\sigma_{u'} = -30.7 \text{ PSI}$$

$$\sigma_{y'} = \frac{\sigma_u + \sigma_y}{2} - \frac{\sigma_u - \sigma_y}{2} \cos 2\theta - \tau_{xy} \sin 2\theta$$

$$\sigma_{y'} = \frac{-30.89 + 0}{2} - \left(\frac{-30.89 - 0}{2} \right) \cos 2(-3.43) - 0.1816 \sin 2(-3.43)$$

$$\sigma_{y'} = -15.445 + 15.445(0.99) - 0.1861(-0.11)$$

$$\sigma_{y'} = -0.13 \text{ PSI.}$$

Shear Stress: *

#18

$$\tan 2\theta_B = -\frac{(\sigma_x - \sigma_y)/2}{\tau_{xy}}$$

$$\tan 2\theta_B = -\frac{(-30.89 - 0)/2}{0.1861}$$

$$= \frac{15.445}{0.1861} \Rightarrow 82.9$$

$$\theta_B = \tan^{-1}\left(\frac{82.9}{2}\right)$$

$$\theta_B = \tan^{-1}(41.45)$$

$$\theta_B = 88.61^\circ$$

Now \rightarrow

$$\tau_{x'y'} = -\frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta$$

$$= -\left(\frac{-30.89 - 0}{2}\right) \sin 2(88.61) + 0.1861 \cos 2(88.61)$$

$$= +15.445 (0.048) + 0.1861 (-0.99)$$

$$\tau_{x'y'} = 0.55 \text{ psi.}$$

MOHR'S CIRCLE: * # 19.

Centre Co-ordinates:

$$(h, k) = \left[\frac{G_x + G_y}{2}, 0 \right]$$

$$(h, k) = \left[\frac{-30.89 + 0}{2}, 0 \right]$$

$$" = [-15.445, 0]$$

$$\text{Radius, } R = \sqrt{\left(\frac{G_x - G_y}{2}\right)^2 + T_{xy}}$$

$$r = \sqrt{(15.445)^2 + 0.1861^2}$$

$$r = 15.446. \text{ Radius.}$$

MOHR'S Circle

$$\sigma_x = -30.89 \text{ PSI}, \sigma_y = 0$$

$$\tau_{xy} = 0.1861 \text{ PSI}$$

Scale:

$$2 \text{ PSI} = 2 \text{ cm.}$$

Then,

$$\text{Radius} = \frac{\sigma_x}{2} = \frac{15.446}{2}$$

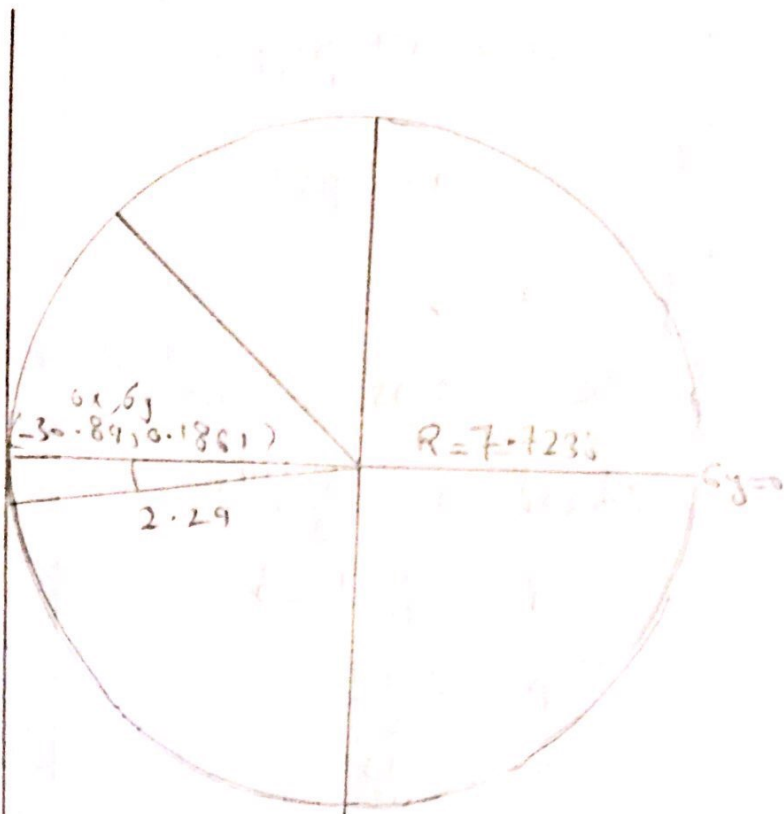
$$\text{Radius} = 7.723 \text{ cm.}$$

$$\theta = \tan^{-1} \left(\frac{0.1861}{30.89 + 15} \right)$$

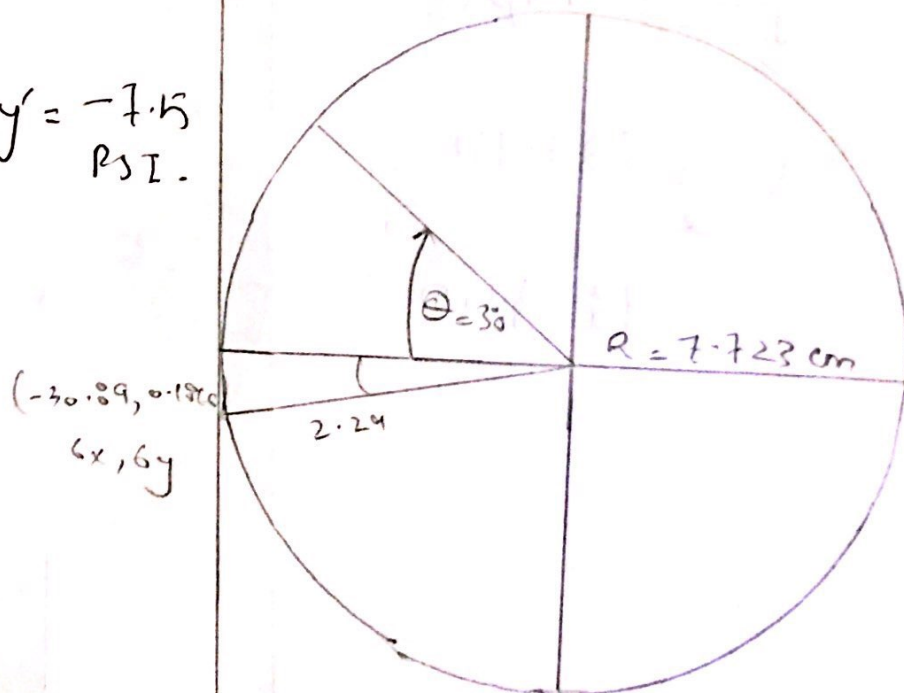
$$30.89 + 15$$

$$\theta = \tan^{-1} (6.94) = 2.29^\circ$$

$$\sigma_{x'} = -29.2 \text{ PSI}, \tau_{x'y'} = -7.15 \text{ PSI.}$$



For New Orientation.
 -15° Clockwise.



→ For Principal Stress

$$\sigma_{x'} = -212.84 \text{ psi}$$

$$\sigma_{y'} = -30.7 \text{ psi}$$

$$\sigma_{y'} = 0$$

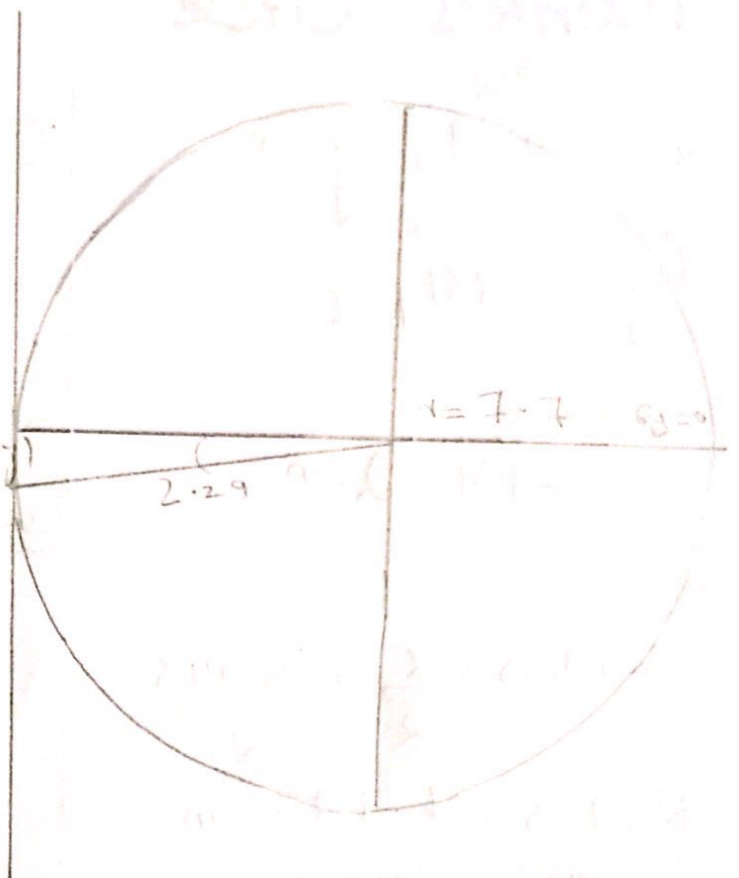
Scale = 1 psi = 2 mm

$$\text{Radius} = \frac{15.446}{2}$$

$$r = 7.723$$

$$\theta_p = \frac{2.29}{2}$$
$$= 1.145$$

$(\sigma_{x'}, \tau_{xy'})$

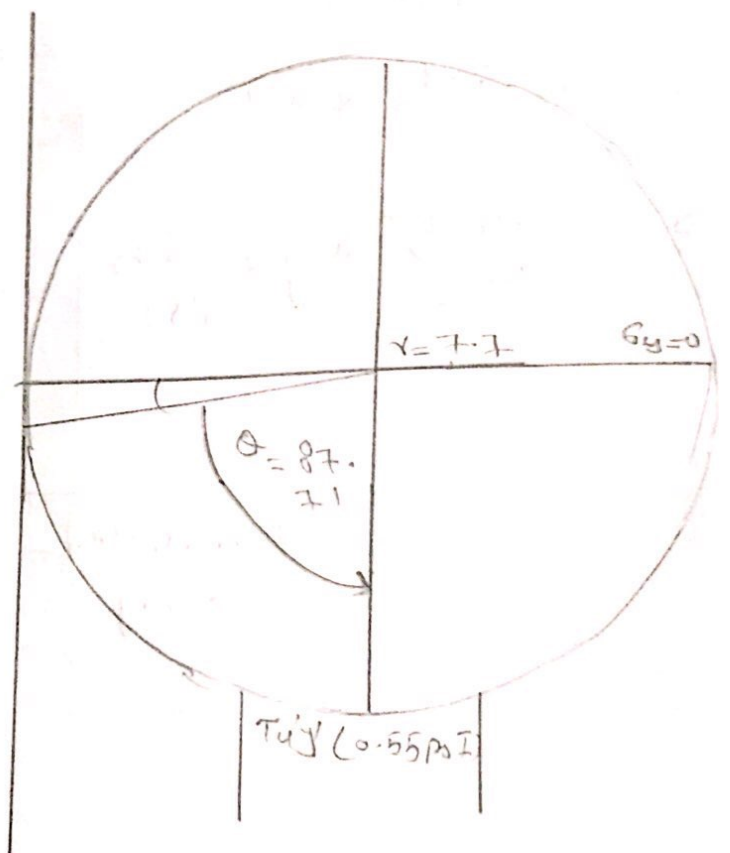


→ For Shear Stress

$$\tau_{xy'} = 0.55 \text{ ksi}$$

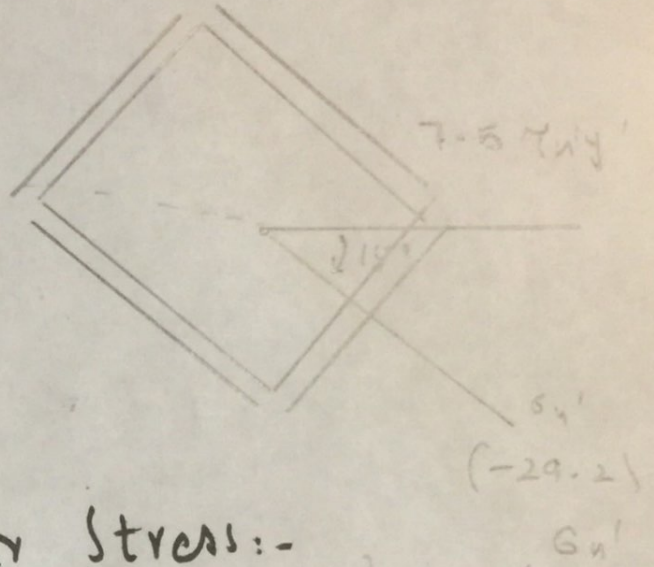
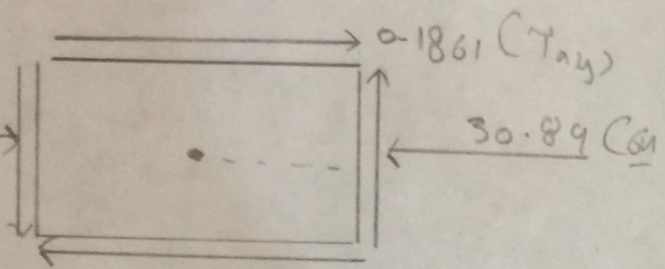
$$\theta_s = \frac{1}{2} (87.71)$$
$$= 43.855$$

$\sigma_{x'}$



Result Comparison:

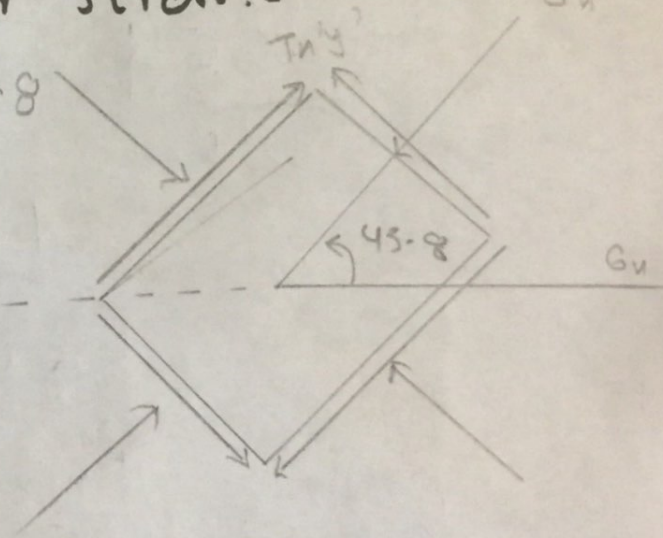
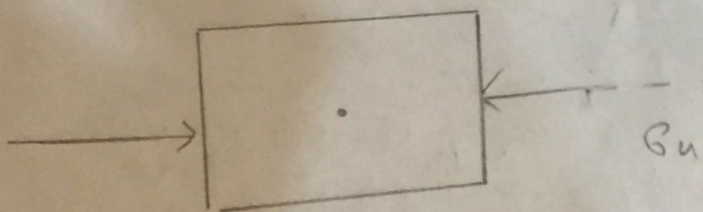
$\theta = 0^\circ$, $\theta = -15^\circ$ Clockwise



Principle And shear stress:-

$\theta = 1$

$\theta = 43.8$



SHEAR Force And Bending Stress Diagram:

Variation: *

