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Q NO # 2.

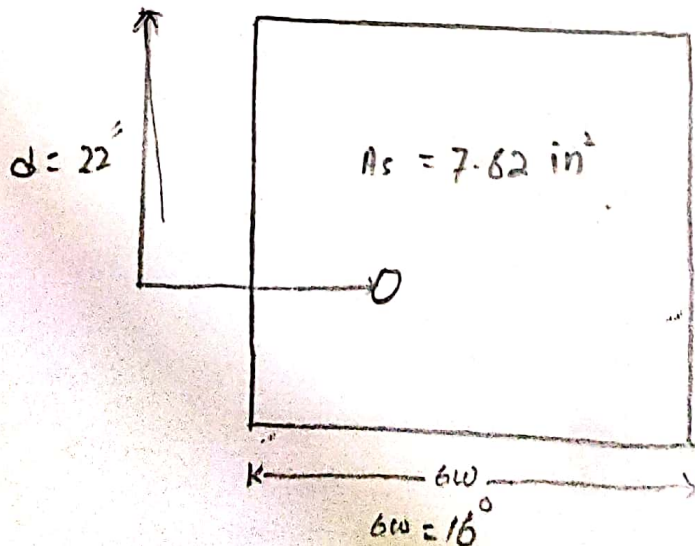
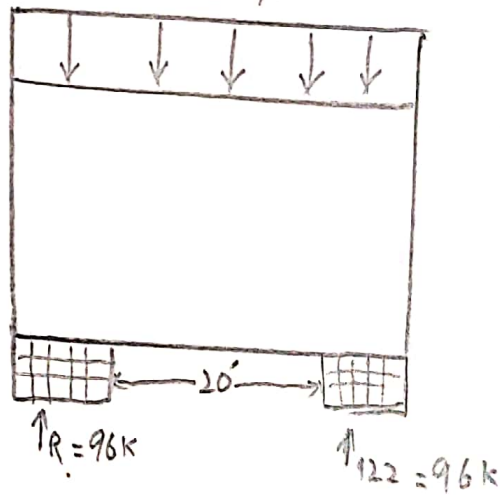
Solution.

First of all we find the Unit load of beam so;

$$\Rightarrow b \times \gamma_c$$

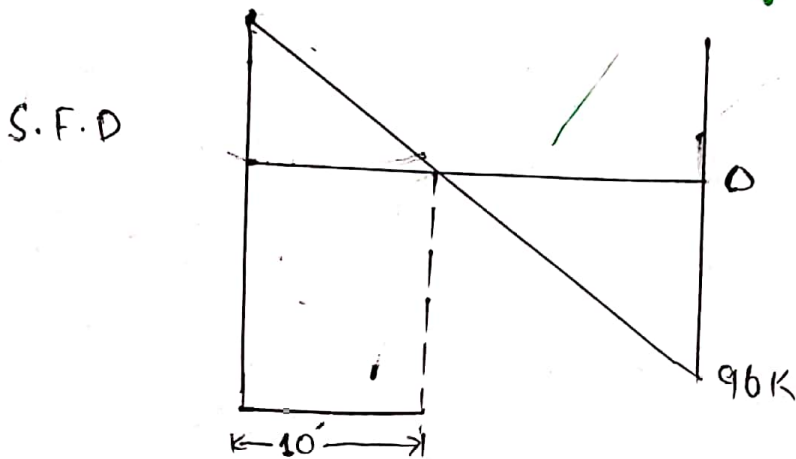
$$\Rightarrow \frac{16}{12} \times 150 \Rightarrow 200 \text{ lb/ft} \Rightarrow 0.2 \text{ k/ft.}$$

So; total factored load = $9.4 + 0.2 \Rightarrow 9.6 \text{ k/ft}$
 $w = 9.6 \text{ k/ft}$



Step # 2

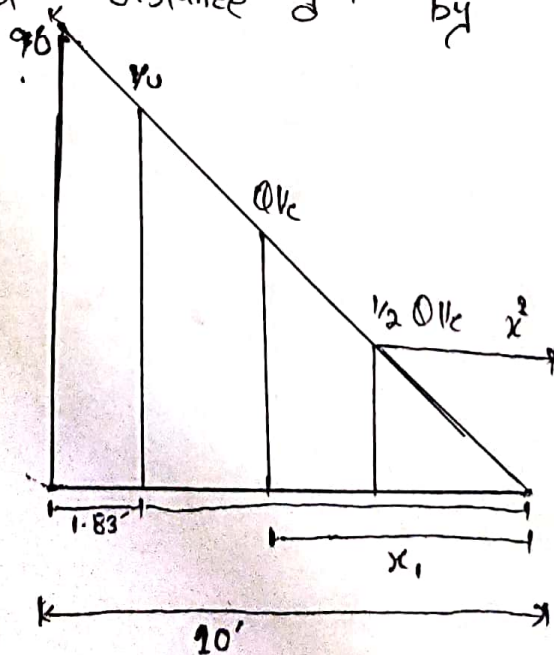
⇒ Draw its shear force diagram:



Step # 3

Find value of critical stress σ_c & its location.

⇒ As we know that critical reaction is located at distance "d" from face of support $a = 22'' = 1.83 \text{ ft}$ value of critical shear at distance "d" by similarity of triangular



From similar Δ 's

$$\Rightarrow \frac{96}{10} = \frac{V_u}{8.17}$$

$$\boxed{V_u = 78.43 \text{ k}}$$

Step # 4

Find the value of " ϕV_c " & " $\frac{1}{2} \phi V_c$ " also its distance from zero shear to right side.

$$\Rightarrow \phi V_c = \phi \times 2 \times \sqrt{f_c'} \times b_w \times d$$

Put value:

$$\Rightarrow \frac{0.75 \times 2 \times \sqrt{4000 \times 16 \times 2}}{1000}$$

$$\Rightarrow \boxed{\phi V_c = 33.40 \text{ k}}$$

\Rightarrow Location of ϕV_c by similarity of Δ 's.

$$\Rightarrow \frac{96}{10} = \frac{33.40}{x_1}$$

$$\Rightarrow \boxed{x_1 = 3.48'}$$

$$\Rightarrow \text{Now } \frac{1}{2} \phi V_c = \frac{33.40}{2} = 16.70 \text{ k}$$

\Rightarrow Location of $\frac{1}{2} \phi V_c$:

$$\Rightarrow \frac{96}{10} \Rightarrow \frac{16.70}{x_2}$$

$$\Rightarrow \boxed{x_2 = 1.74'}$$

Step # 5.

value of ϕV_s [$V_u = \phi V_s + \phi V_c$].

So;

$$\Rightarrow \phi V_s = V_u - \phi V_c$$

$$\Rightarrow \phi V_s = 78.43 - 33.40$$

$$\boxed{\phi V_s = 45.03 \text{ k}}$$

Step # 6.

check on section adequacy:

$$\Rightarrow \phi \times 8 \times \sqrt{f_c} \times b_w \times d \Rightarrow \frac{0.75 \times 8 \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$\Rightarrow \boxed{133.57 \text{ k}}$$

As:

$$\Rightarrow \phi \times 8 \times \sqrt{f_c} \times b_w \times d > \phi V_s \rightarrow \text{It means section is adequate.}$$

Step # 7.

check on min spacing for stirrups:

$$\Rightarrow \phi \times 4 \times \sqrt{f_c} \times b_w \times d \Rightarrow \frac{0.75 \times \sqrt{4000} \times 16 \times 22}{1000} = \boxed{68.79 \text{ k}}$$

As;

$$\phi \times 4 \times \sqrt{f_c} \times b_w \times d > \phi V_s = 45.03 \text{ k}$$

Thus:

max. spacing will be selected from the following four condition.

(i); $l_{max} = 24''$

(ii) $d/2 = 22''/2 = 11''$

(iii) $l_{max} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c} \times b_w}$

$$\Rightarrow AU = \frac{\pi}{4} \left(\frac{3}{8}\right)^2 \Rightarrow \frac{0.22 \times 60000}{0.75 \sqrt{4000 \times 16}}$$

$$= \boxed{17.40''}$$

$$AU = 0.11 \times 2$$

$$AU = 0.22$$

$$\textcircled{4} \quad J_{\max} = \frac{AU \times b_y}{S_0 \times b_w}$$

$$= \frac{0.22 \times 60000}{S_0 \times 16}$$

$$\Rightarrow \boxed{J_{\max} = 16.50}$$

From the above four condition least value of spacing from # 3, U shaped will be selected.

So;

$$J_{\max} = 11'' \text{ c/c}$$

Step # 8.

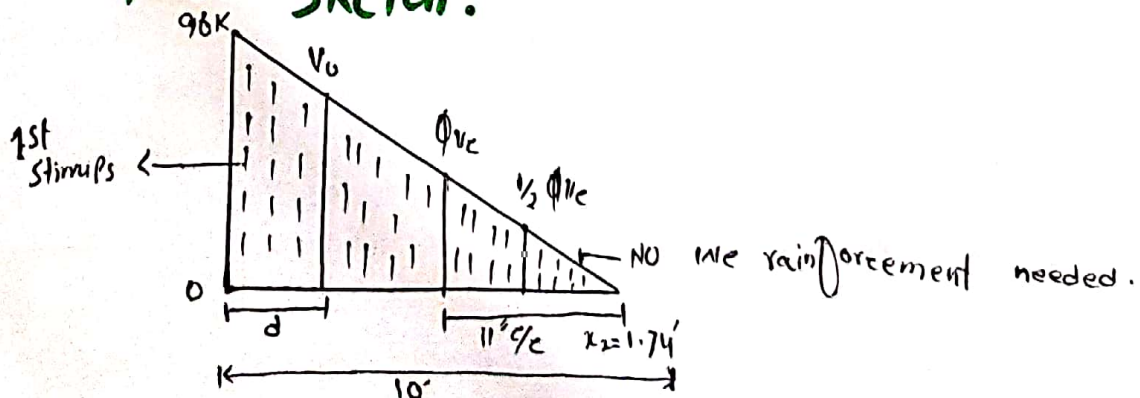
Spacing of stirrup from / at critical section:

$$\Rightarrow S = \frac{\phi \times AU \times f_y \times d}{V_u - \phi v_c} \Rightarrow \frac{0.75 \times 0.22 \times 60 \times 22}{78.43 - 33.40}$$

$$\boxed{S = 48.4'' \approx 5'' \text{ c/c}}$$

Step # 9.

Find Sketch:



(*) As we know that Dist stirrup from face of support =

$$\Rightarrow \boxed{\frac{S}{2} = 2.5 \approx 2''}$$

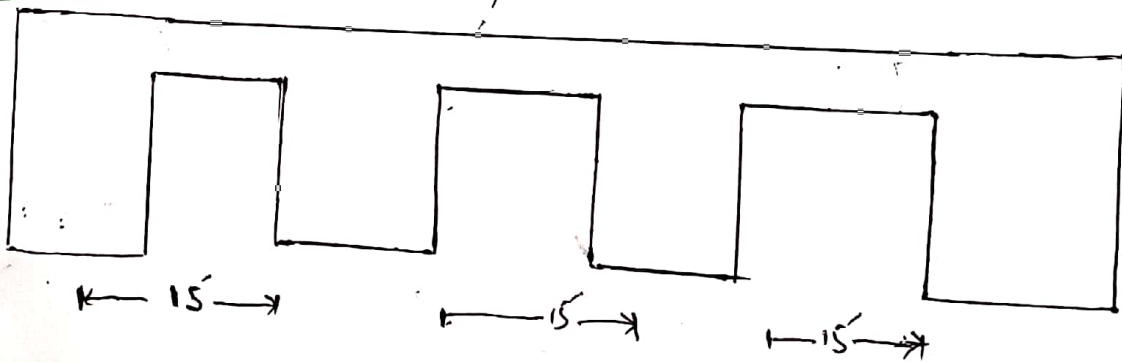
Q No # 1

A reinforcement concrete slab is
 Draw & sketch of you find dia?

⇒ Given data :

- * clear span b/w support = 15'
- * Factored live load = 160 lb/ft²
- * service floor finish load = 20 lb/ft²
- * $f_y = 40$ ksi

Solution :



Step # 1

Minimum Thickness :

by using formula:

$$\Rightarrow t_{min} = L/28 \Rightarrow 15/28$$

$$t_{min} = 6.4 \approx 6.5''$$

As; $f_y \longrightarrow 40$ ksi

⇒ So we will multiply a factor with this thickness.

$$\Rightarrow \text{Factor} = \left[0.4 + \frac{f_y}{100} \right]$$

$$= 0.4 + \frac{40}{100} = 0.8$$

$$\Rightarrow f_y: 40$$

$$\boxed{\text{Factor} = 0.8}$$

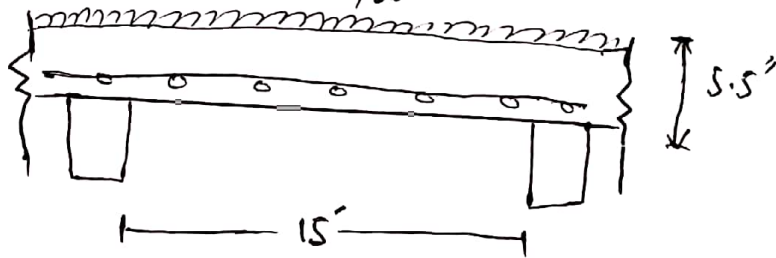
hence the minimum thickness will be;

$$6.5 \times 0.8$$

$$\boxed{t_{\min} = 5.2 \approx 5.5''}$$

Step # 2.

Effective Depth.



By formula:

$$\Rightarrow d = t - \text{clear cover} - \frac{1}{2} (\text{dia of main bars})$$

$$= 5.5 - 0.75 - \frac{1}{2} \left(\frac{5}{8} \right)$$

$$\boxed{d = 4.5''}$$

Step # 3

self weight of slab:

By formula:

$$\Rightarrow \frac{t}{12} \times \gamma_{\text{concrete}}$$

$$\Rightarrow \frac{5.5}{12} \times 150 \Rightarrow \boxed{68.75 \text{ lb/ft}^2}$$

Step # 4.

Total Factored load :

$$\Rightarrow \text{Factored Live load} = 160 \text{ lb/ft}^2$$

So the Factored dead load will be :

$$\Rightarrow \text{D.L} = 1.2 (20 + 68.75) = 106.5 \text{ lb/ft}^2$$

$$\begin{aligned} \text{Total Factored load} &= \text{D.L} + \text{L.L} \\ &= 106.5 + 160 \\ &= 266.5 \text{ lb/ft}^2 \Rightarrow 0.2665 \text{ k/ft}^2 \end{aligned}$$

Step # 5

Ultimate moment :

By using formula:

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (15)^2 \times 12}{8}$$

$$M_u = 89.94 \text{ kips-inches}$$

Step # 6.

Area of steel of main bars by Trial & repeat method:

Trial # 1 :

Let depth of compression block.

$$\begin{aligned} a &= 0.2 \times t \\ &= 0.2 \times 5.5 \end{aligned}$$

$$a = 1.1''$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - 1/2)}$$

$$A_{st} = 0.63 \text{ in}^2$$

Trial # 2 :

$$a = \frac{A_{st} \times f_y}{0.55 \times f'_c \times b} = \frac{0.63 \times 40}{0.85 \times 4 \times 12} \Rightarrow 0.62 \text{ in}^2$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{0.6}{2})}$$

$$A_{st} = 0.59 \text{ in}^2$$

Trial # 3 :

$$a = \frac{0.59 \times 40}{0.83 \times 4 \times 12} \Rightarrow 0.57$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{0.57}{2})} \Rightarrow$$

$$A_{st} = 0.59 \text{ in}^2$$

So we will use $A_{st} = 0.59 \text{ in}^2$.

Step # 7:

Area of steel for distribution reinforcement:
By formula:

$$A_{min} = 0.002 \times b \times w \Rightarrow (\text{Grade 40 steel}).$$

$$= 0.002 \times 12 \times 5.5 \Rightarrow$$

$$A_{min} = 0.132 \text{ in}^2$$

Step # 8. Spacing for main bars:

By formulas:

Spacing:

$$\frac{A_b}{A_{st}} \times 12$$

We use #6 bar dia = (6/8)"

$$Area = \pi/4 (6/8)^2 = 0.442 \text{ in}^2$$

Step # 9.

Spacing for distribution bars:

$$Spacing \Rightarrow \frac{A_b}{A_{st}}$$

We use #5 bars so,

$$\Rightarrow \text{dia} = (5/8)" , \text{Area} = \pi/4 (5/8)^2 \Rightarrow \boxed{0.31 \text{ in}^2}$$

$$Spacing = \frac{0.31}{0.132} \times 12$$

$$\Rightarrow \boxed{28.1 \approx 28" \text{ c/c}}$$

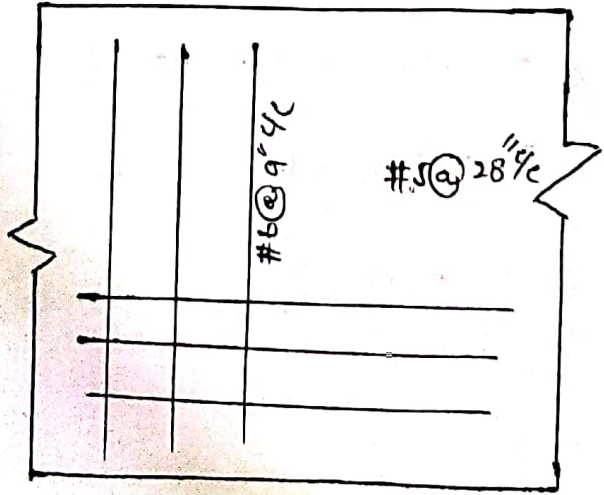
Step # 10.

Find sketch:

⇒ f'c = 4 ksi , fy = 40 ksi

⇒ Main steel #6 at 9" c/c.

⇒ Distribution steel #5 at 28" c/c.



QNO# 3

calculate the axial ultimate
diagram.....?

Solution:

step # 1 . Find gross area of concrete:

$$\Rightarrow A_g = b \times b \text{ (since it is square tied column)}$$

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

step # 2 ~~As = 7.2~~
Find Area of steel.

Since:

$$A_s = 5\% \text{ of } A_g$$

$$= 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

step # 3 . ultimate load carrying capacity .

$$\Rightarrow P_u = \phi \times 0.80 \times [0.85 \times f'_c \times (A_g - A_s) + A_s \times f_y]$$

$$= 0.65 \times 0.80 \times [0.85 \times 4 [(144 - 7.2) + 7.2 \times 60]$$

$$\phi = 0.65$$

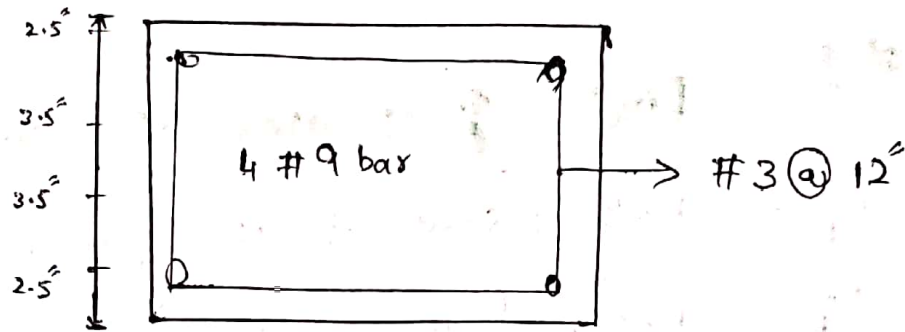
$$P_u = 466.50 \text{ k}$$

Step # 4 . Sketch & design of ties (r/c) distance .

⇒ From the below value we choose the
least value of all this ;

- (i) $16 \times \text{dia of long bar} = 16 \times 9/8 = 18''$
- (ii) $48 \times \text{dia of Tie bar} = 48 \times 3/8 = 18''$
- (iii) least column dimension = $12''$

So; (c/c) distance b/w ties = $12''$



⇒ Since it is a tied square column so there is no spiral stirrup used, the stirrup used is rectangular shape due to the specification of the structure. Thus we will use ties stirrups instead.

Q No # 54

Design a square footing Sketch Diagram?

Solution:

step # 1.

Let :

$$h = 24''$$

step # 2.

Total weight = wt of soil + wt of R.e.

$$\Rightarrow (3 \times 120) + (2 \times 150)$$

$$= 660 \text{ psf} = \boxed{0.660 \text{ ksf}}$$

step # 3.

Effective bearing capacity:

$$q_e = q_a - \gamma h$$

$$= 2.50 - 0.660$$

$$\boxed{q_e = 1.84 \text{ ksf}}$$

step # 4.

Required Area for Foundation.

$$\text{Area} = \frac{\text{Service load}}{q_e} = \frac{100 + 120}{1.84} \Rightarrow \boxed{119.56 \text{ m}^2}$$

step # 5

Since Foundation is square;

$$\Rightarrow \text{Area} = b \times b = 119.57 \Rightarrow \boxed{B \approx 11}$$

Step # 6.

upward bearing capacity of soil:

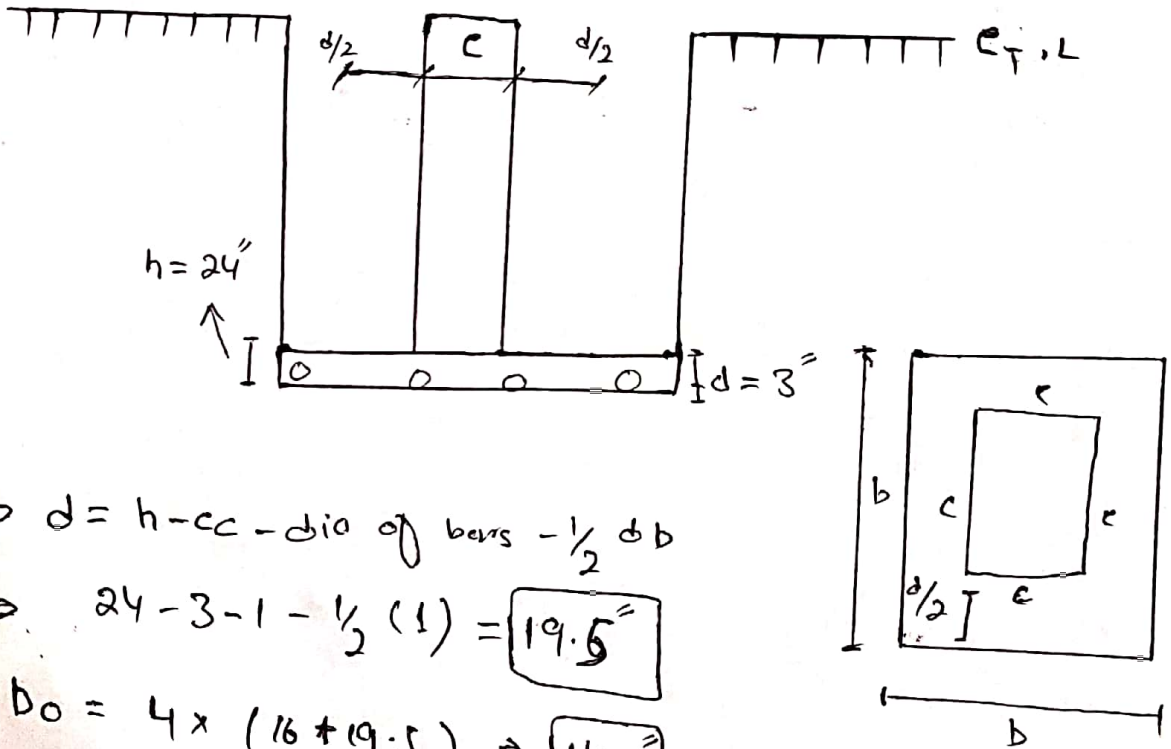
$$\Rightarrow q_{up} = \frac{\text{factored load}}{(B)^2} \Rightarrow \frac{(1.2 \times 100) + (1.6 \times 120)}{(11)^2}$$

$$q_{up} = 2.58 \text{ k/ft}^2$$

Step # 7.

Punching shear:

$$b_o = 4 \times (c + d)$$



$$\Rightarrow d = h - c - \text{dia of bars} - \frac{1}{2} \phi b$$

$$\Rightarrow 24 - 3 - 1 - \frac{1}{2} (1) = 19.5$$

$$b_o = 4 \times (16 + 19.5) \Rightarrow 142$$

Take . # 8 bars
dia = $\frac{3}{8} = 1$

Step # 8.

$$V_{u2} = q_{up} \times \left[B^2 - (c + d)^2 \right]$$

$$= 2.58 \times \left[(11)^2 - \left(\frac{16 + 19.5}{12} \right)^2 \right]$$

$$V_{u2} = 289.60 \text{ k}$$

Step # 9.

$$\begin{aligned}\phi V_{c/p} &= \phi \times 4 \times \sqrt{f_c} \times b \times d \\ &= \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5}{1000}\end{aligned}$$

$$\boxed{\phi V_{c/p} = 525.38}$$

Step # 10.

Beam shear / one way shear check.

$$\Rightarrow V_{u1} = q_{up} \times B \times \left[\frac{B}{2} - \frac{c}{2} - d \right]$$

$$V_{u1} = 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{2} - 19.5 \right]$$

$$\boxed{V_{u1} = 90.95 \text{ k}}$$

Step # 11.

Self capacity:

$$\begin{aligned}\Rightarrow \phi V_c &= \phi \times 2 \times \sqrt{f_c} \times b \times d \\ &= \frac{0.75 \times 2 \times \sqrt{4000} \times [11 \times 12 - 16]}{1000}\end{aligned}$$

$$\Rightarrow \phi V_c = 110.04 \text{ k} > V_{u1} \Rightarrow \text{OK}$$

Step # 12

Ultimate moment:

$$\Rightarrow M_u = \frac{q_{up} \times B}{8} \times (B - c)^2 \Rightarrow \frac{2.58 \times 11}{8} \times \left(\frac{11 - 16}{12} \right)^2$$

$$\Rightarrow M_u = 331.49 \text{ k}' \Rightarrow \boxed{3977.93 \text{ k}^2}$$

Step # 13

Area of steel for main bars by Trial & Repeat method:

Trial # 1

Let:

$$a = 0.2 \times h$$

$$= 0.2 \times 24 = \boxed{4.8''}$$

A_s :

$$= \frac{M_u}{\phi \times f_y \times (d - \frac{a}{2})} \Rightarrow \frac{3977.93}{0.90 \times 60 \times (11 - \frac{4.8}{2})}$$

$$\Rightarrow \boxed{A_s = 8.56 \text{ in}^2}$$

Trial # 2

$$\Rightarrow a = \frac{A_s \times f_y}{0.85 \times f'_c \times b} \Rightarrow \frac{8.56 \times 60}{0.85 \times 3 \times 11 \times 12}$$

$$\boxed{a = 7.197 \text{ in}^2}$$

Trial # 3

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} \Rightarrow \boxed{1.28''}$$

$$\Rightarrow A_s = \frac{3977.93}{0.90 \times 60 \left(11 - \frac{1.28}{2}\right)} = \boxed{7.1 \text{ in}^2}$$

\Rightarrow So that area = 7.1 m².

step # 14.

check the min reinforcement by the following 03 method:

$$(a) A_{smin} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24$$

$$A_{smin} = 5.70 \text{ in}^2$$

$$(b) A_{smin} = \frac{200}{f_y} \times B \times d \Rightarrow \frac{200}{6000} \times (11 \times 12) \times 19.5$$

$$A_{smin} = 8.58 \text{ in}^2$$

$$(c) A_{smin} = \frac{3 \times \sqrt{f'_c}}{f_y} \times B \times d \Rightarrow \frac{3 \times \sqrt{3000}}{6000} \times (11 \times 12) \times 19.5$$

$$A_{smin} = 7.03 \text{ in}^2$$

\Rightarrow From the above value greater value will be selected their $A_{smin} = 8.58 \text{ in}^2$.

step # 15.

using # 8 bar:

$$\Rightarrow A_b = 0.785 \text{ in}$$

$$\Rightarrow \text{No of bars} = \frac{A_s}{A_b} = \frac{8.58}{0.785} \Rightarrow \boxed{10.92} \Rightarrow 11 \text{ bars in each direction}$$

The End!