

# **IQRA NATIONAL UNIVERSITY**



## **Power Electronics**

### **Final Assignment Spring 2020**

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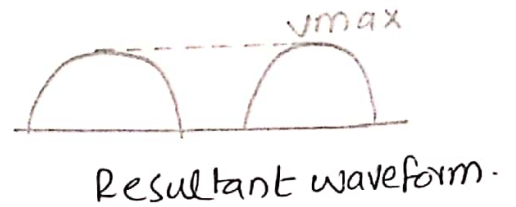
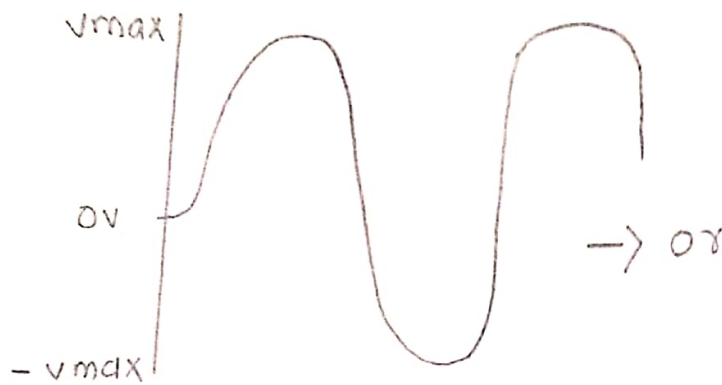
Question No (1)

Difference between single phase half wave and full wave bridge rectifier.

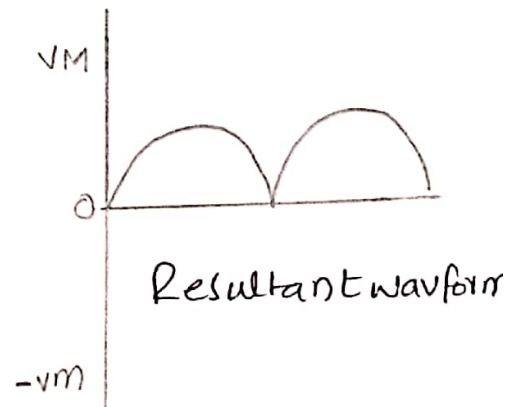
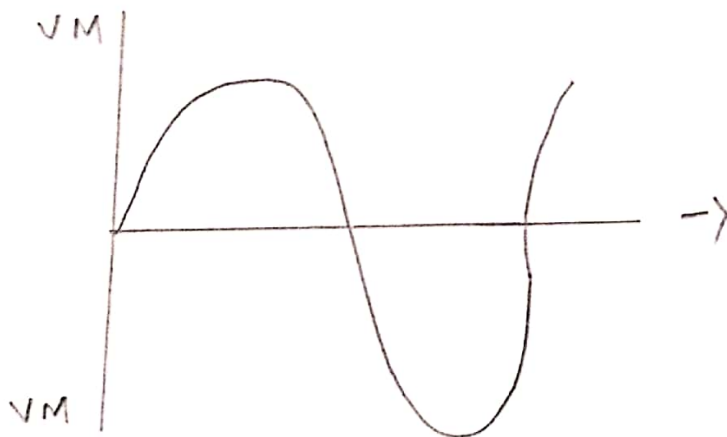
- ① Half wave rectifier which convert only one half of AC cycle into pulsating DC while full wave rectifier is an electronic circuit which convert entire cycle AC into pulsating DC.
- ② Half wave utilize only half of AC cycle for the conversion while full wave utilize full wave of AC cycle.
- ③ Half wave is unidirectional the conduction is one direction only either convert positive or negative that why called half wave rectifier is bidirectional it convert for positive as well as negative half of the cycle.

④ output wave form of single phase half wave

②



and single phase wave bridge rectifier



⇒ ① Similarity between single phase wave and full wave bridge rectifier.

① Peak inverse voltage of single half wave and full wave rectifier are same which is  $V_{in}$  and same in both rectifiers.

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③

⇒ Both utilize the single phase for the operation.

② Single phase uncontrolled and controlled rectifier difference and similarities.

⇒ uncontrolled they are naturally turn on whenever a positive voltage is applied between its terminal and when you stop by applying its negative voltage.

⇒ while in controlled rectifier that conduction start at any angle in positive half cycle normally 0 to 180 degree once the conduction start can be turn on and off.



Question No (2)

Given  $70\text{V}$

$R = 13\Omega$

Solution :- For half wave

①  $v_{dc}$

$$\frac{v_m}{\pi} \rightarrow \text{①}$$

where  $v_m = 70\text{V}$  and  $\pi = 3.14$

Putting these values in eq ①

$$v_{dc} = \frac{70}{3.14}$$

$$v_{dc} = 22.29$$

For full wave bridge

$$\frac{2v_m}{\pi}$$

Putting value

$$v_{dc} = \frac{2(70)}{3.14} \Rightarrow \frac{140}{3.14}$$

**$v_{dc} = 44.58$**

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(5)

$\Rightarrow$  (2)  $\bar{I}_{dc}$

For half wave

$$\bar{I}_{dc} = \frac{V_m}{\pi R}$$

$$\bar{I}_{dc} = \frac{70}{(3.14)13}$$

$$\bar{I}_{dc} = \frac{70}{40.82}$$

$$\bar{I}_{dc} = 1.714A$$

$\Rightarrow$  For full wave

$$\bar{I}_{dc} = \frac{I_m}{\pi} \rightarrow (2) \text{ Where } I_m = \frac{V_m}{R}$$

$$I_m = \frac{70}{13}$$

$$I_m = 5.3A$$

$\Rightarrow$  Put it in eq (2)

$$\bar{I}_{dc} = \frac{5.3}{3.14}$$

$$\bar{I}_{dc} = 1.714 \text{ Amp}$$

$$\Rightarrow (3) \quad v_{rms}$$

⑥

For half wave

$$v_{rms} = \frac{v_m}{2}$$

$$= \frac{70}{2}$$

$$v_{rms} = 35V$$

For Full wave

$$v_{rms} = \sqrt{2} v_s \rightarrow (3)$$

$$\text{As } v_s = \frac{v_m}{\sqrt{2}}$$

$$= \frac{70}{\sqrt{2}}$$

$$= \frac{70}{1.414}$$

$$v_s = 49.50$$

putting value of  $v_s$  in eq (3)

$$v_{rms} = (\sqrt{2}) (49.50)$$

$$= (1.414) (49.50)$$

$$v_{rms} = 70.00V$$

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$\Rightarrow \bar{I}_{rms}$  : (For half wave and full wave) (7)

For half wave

$$\bar{I}_{rms} = \frac{V_m}{2R}$$

$$= \frac{49}{2(13)}$$

$$= \frac{49}{26}$$

$$= 1.884A$$

$$\bar{I}_{rms} = 1.884 \text{ Amp}$$

$\Rightarrow$  For full wave

$$\bar{I}_{rms} = \frac{I_m}{2} \rightarrow \text{eq (4)}$$

$$\text{where } I_m = \frac{V_m}{R}$$

$$= \frac{70}{13}$$

$$I_m = 5.38A$$

Put values of  $I_m$  in eq (4)

$$\bar{I}_{rms} = \frac{5.38}{2}$$

$$\bar{I}_{rms} = 2.69$$



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(5) I would like to refer the (8)  
uncontroll full wave bridge rectifire  
because the efficiency of the full  
wave bridge rectifire is better  
than in half wave rectifire and  
out put frequency also grater than  
half wave rectifire.



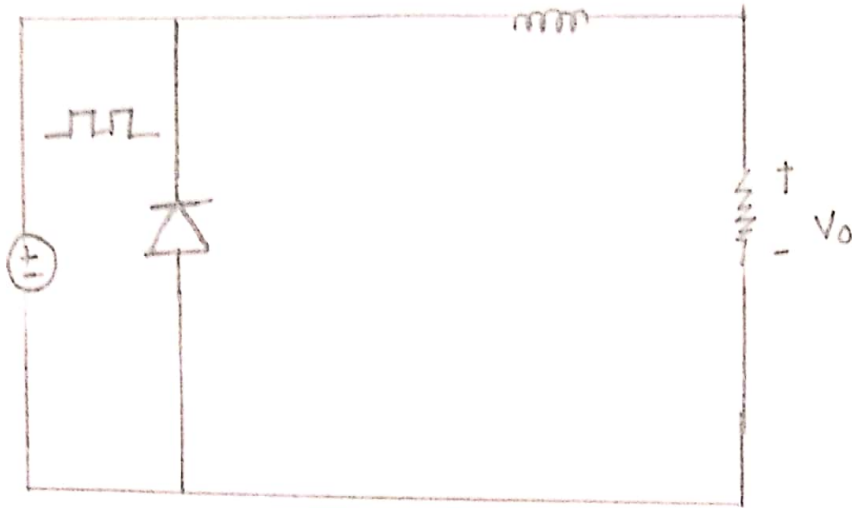
Question No (3)

④

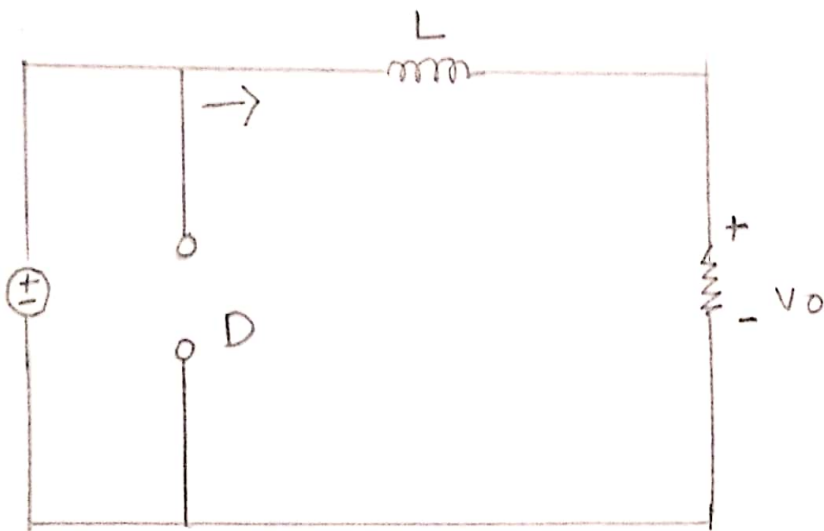
Buck chopper

- ① output voltage is less than input voltage.
- ② The thyristor in the circuit acts as a switch
- ③ When thyristor is ON supply voltage appear across the load
- ④ When thyristor is OFF the voltage across the load will be zero.
- ⑤ Practical arrangement includes an inductor  $L$  and diode which are used to eliminate current pulsation providing a smooth DC amount of current
- ⑥ With  $S$  closed  $D$  is off and it remain off and it remain off as long as  $S$  is ON

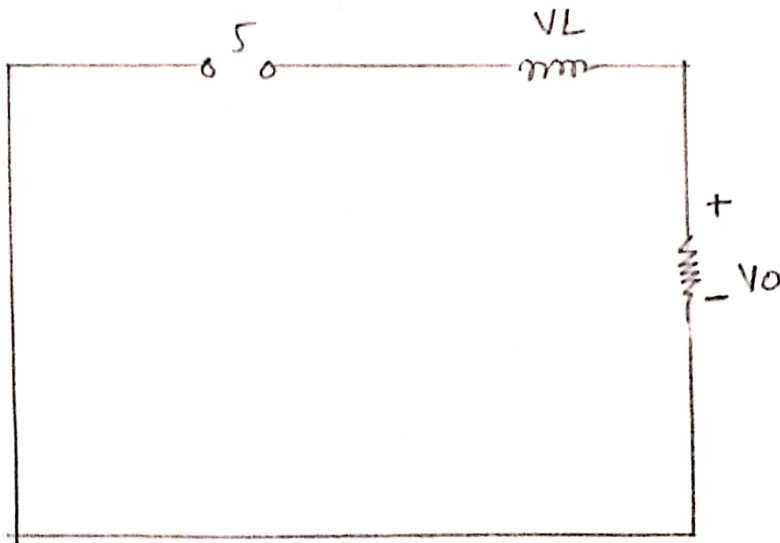
- ⑦ The i/p current buildup exponentially and flow through  $L$  and Load
- ⑧  $V_0$  equal to  $V_1$
- ⑨ with  $S$  off or open the current through  $I$  decay to zero
- ⑩ This cause inductive voltage with opposite polarity across  $L$ .
- ⑪  $V_2$  forward bias diode  $D$
- ⑫ Current flows through  $L$  and Load and diode  $D$
- ⑬ This arrangement permit the use of simple filter inductance  $L$  to provide a satisfactorily smooth DC Load Current
- ⑭ With high switch frequency smaller inductance is sufficient to get desired output.



=> Circuit of Buck Converter.



=> Circuit when closed



=> Circuit when Switch is open

## ⇒ Given Data

$$v_{in} = 50V$$

$$D = 0.70\%$$

$$R = 13\Omega$$

$$\text{Frequency (f)} = 20\text{kHz}$$

①  $v_{out}$

we know that

$$v_{out} = \alpha \times v_s \quad \text{OR} \quad D \times v_s \rightarrow \textcircled{1}$$

Here  $\alpha = D = \text{Duty Cycle}$

$$\text{which } 70\% = 0.70$$

putting all value in eq  $\textcircled{1}$

$$v_{out} = (0.70)(50)$$

$$\boxed{v_{out} = 35V}$$

②  $I_{out}$

$$I_{out} = V/R$$

$$= \frac{35}{13}$$

$$\bar{I}_{out} = 2.69 \text{ A}$$

(3)  $\bar{I}_{in}$

We know that

$$\bar{I}_o = \frac{\bar{I}_i}{\alpha_{ORD}}$$

$$\bar{I}_i = \bar{I}_o \times D$$

$$\bar{I}_i = 2.69 \times 0.70$$

$$\bar{I}_i = 1.88 \text{ A}$$

(4) Inductor

We know that

$$L = \frac{T_{OFF} \times R}{2}$$

Let Suppose  $T_{OFF} = 0.009$

$$L = \frac{0.006 \times 13}{2}$$

$$L = 0.039 \text{ H}$$

Question NO (4)Boost chopper

- ① The output voltage is more than the input voltage by several times.
- ②  $L$  is used to provide smooth input current.
- ③ The SCR (S) acts as the switch which works in PWM mode.
- ④ With  $S$  ON the  $L$  is connected to the supply.
- ⑤ Load voltage  $v_2$  jumps instantaneously to  $v_1$  but current through  $L$  increases linearly and stored energy.
- ⑥ When  $S$  is open the current through the  $L$  collapses and energy is stored and  $L$  is transferred to  $C$  through  $D$ .

(7) The induced voltage across the inductor reverse and adds to source voltage increasing output voltage

(8) The current that was flowing through S now flow through L, D and C to load.

(9) Energy stored in inductor is released to load

(10) When S closed D become reverse bias the capacitor energy supplied the load voltage and cycle again

$$V_0 = V_1 + V_L$$

(11)  $V_0$  is always higher than  $V_1$  as polarity of inductor voltage  $V_L$  is same as  $V_1$



(12) if inductor  $L$  is very large

(16)

Source current  $I_i$  is ripple free

and considered constant  $w_{on} = v_i t_{on}$

(13) Assuming  $C$  to be large enough

to neglect the voltage ripple

$v_o$  is considered constant

$$w_{off} = (v_o - v_i) * I_i * t_{off}$$

(14) Since losses are neglect the energy

stored transferred during  $T_{off}$  by

$L$  min be equal to energy

gained during  $T_{on} = w_{off} = v_i I_i t_{on} =$

$$= (v_o - v_i) * I_i * t_{off}$$

$$v_o = v_i \left( 1 + \frac{T_{on}}{t_{off}} \right) = v_i \left( \frac{T}{T - t_{on}} \right)$$

$$v_i \left( \frac{1}{1 - \frac{T_{on}}{T}} \right) = v_o \left( \frac{1}{1 - d} \right)$$

Thus  $v_o$  is always greater than  $v_i$

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$\Rightarrow$  Thus  $v_0$  is always greater than  $v_1$  (17)

$$\rightarrow P_1 = P_0 \rightarrow v_1 I_1 = \frac{v_0^2}{R} \rightarrow I_1 = \frac{v_0^2}{v_1} * \frac{1}{R}$$

$$\rightarrow I_0 = I_1 \times \frac{T_{OFF}}{T} \Rightarrow I_0 = I_1 (1-d)$$

$$\rightarrow P_0 = P_1 \Rightarrow v_1 I_1 \Rightarrow \frac{v_0^2}{R} = \frac{v_1^2}{(1-d)^2} * \frac{1}{R}$$

$$\rightarrow I_1 = \frac{v_1}{(1-d)^2} * \frac{1}{R}$$

$$\rightarrow I_1 = \frac{I_{max} + I_{min}}{2} = I_1$$

$$I_{max} + I_{min} = 2 * I_1$$

$\rightarrow$  voltage across  $L$  is

$$v_L = v_1 = L * \frac{di}{dt}$$

$$\Delta I_1 = \frac{v_1}{L} * T_{ON} \text{ or } I_{max} - I_{min}$$

$$\Rightarrow \frac{v_1^2}{L} T_{ON}$$

$$\text{Again } I_{max} + I_{min} = 2 * I_1$$

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=> Solving

(18)

$$\bar{I}_{\max} = V_I \left[ \frac{1}{R(1-d)^2} + \frac{T_{ON}}{2L} \right]$$

$$\bar{I}_{\min} = V_I \left[ \frac{1}{R(1-d)^2} - \frac{T_{ON}}{2L} \right]$$

$$I_{P-D} = \bar{I}_{\max} - \bar{I}_{\min} = \frac{V_I T_{ON}}{L}$$

For continuous current mode

$$\bar{I}_{\min} = V_I \left[ \frac{1}{R(1-d)^2} - \frac{T_{ON}}{2L} \right]$$

$$\Rightarrow \frac{1}{R(1-d)^2} = \frac{T_{ON}}{2L} \Rightarrow L = \frac{R T_{ON} (1-d)^2}{2}$$



$\Rightarrow$  Given Data

$$V_{in} = 50V$$

$$\text{duty cycle } D = 0.70\%$$

$$\text{Resistor } R = 13\Omega$$

$$\text{Frequency } F = 20\text{kHz}$$

①  $V_{out}$

As we know

$$V_o = V_i \left( \frac{1}{1-d} \right)$$

$$V_o = 50 \left( \frac{1}{1-0.70} \right)$$

$$V_o = 50 \left( \frac{1}{0.30} \right)$$

$$V_o = 166.66$$

②  $I_{out}$

$$I_o = I_i (1-d) \rightarrow \text{①}$$

First finding  $I_{in}$

(3)  $I_{in}$ 

$$\bar{I}_1 = \frac{V_i}{(1-d)^2} * \frac{1}{R}$$

$$\Rightarrow \frac{50}{(1-0.70)^2} * \frac{1}{13}$$

$$\bar{I}_{in} = \frac{50}{(0.3)^2} * \frac{1}{13}$$

$$= \frac{50}{0.09} * \frac{1}{13}$$

$$= 555.55 * \frac{1}{13}$$

$$= 42.73 \text{ A}$$

Putting this value in eq ①

$$I_{out} = I_1 (1-d)$$

$$I_o = 42.73 (1-0.70)$$

$$I_o = 42.73 (0.30)$$

$$\bar{I}_o = 12.8 \text{ A}$$

Question NO (5)

⇒ Buck - Boost Chopper

- it combines the concept of both step-up and step-down choppers
- The output voltage is either higher or lower than input voltage
- The switch is either an SCR or GTO or IGBT
- When  $S$  is ON  $D$  is reverse biased and  $I_D$  is zero
- While  $S$  is OFF the source is disconnected.
- The current through inductor does not change instantaneously and it forward biases the diode providing path for the load.

→ With  $S = ON$  ( $T_{ON}$ );  $W_{ON} = V_1 * I_1 * T_{ON}$

With  $S = OFF$  ( $T_{OFF}$ );  $W_{OFF} = V_1 * I_1 * T_{OFF}$

→ Ignoring losses,  $W_{ON} = W_{OFF} =$   
 $V_1 * I_1 * I_{OW}$

$$\Rightarrow V_1 * I_1 * T_{OFF}$$

$$\rightarrow V_0 = V_1 \frac{dt}{(1-d)T} = V_1 \frac{d}{(1-d)}$$

$$I_L = \frac{I_{max} + I_{min}}{2}; I_1 = I_L d = \frac{(I_{max} + I_{min})}{2} d$$

The average and put  $P_1 = V_1 I_1 =$   
 $\frac{(I_{max} + I_{min})}{2}$

$$\times d \Rightarrow P_0 = \frac{V_0^2}{R}$$

$$\rightarrow I_{max} = V_1 \left[ \frac{1}{R(1-d)^2} + \frac{I}{2L} \right] d$$

$$\rightarrow I_{min} = V_1 \left[ \frac{1}{R(1-d)^2} - \frac{I}{2L} \right] d$$

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$\Rightarrow$  For Continuous Current Condition <sup>(23)</sup>

$$I_{\min} = 0 = v_1 \left[ \frac{1}{R(1-d)^2} - \frac{T}{2L} \right] d$$

$$\Rightarrow L = \frac{RTd}{2} (1-d)^2$$





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(24)

$\Rightarrow$  Data

$$v_{in} = 50 \text{ V}$$

$$v_{out} = 70\% \quad 0.70$$

$$\text{Resistor (R)} = 13 \Omega$$

$$\text{Frequency } f = 20 \text{ KHz}$$

① Duty cycle (D)

we know that

$$\frac{v_o}{v_i} = \frac{-D}{1-D}$$

$$v_o = \frac{v_i d}{(1-d)}$$

$$0.70 = \frac{50 d}{(1-d)}$$

$$(0.70)(1-d) = d50$$

$$0.70 - 0.70d = d50$$

$$0.70 = d50 + 0.70d$$

$$\Rightarrow 50.7d$$

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(25)

$$\Rightarrow 50 \cdot 7d = 0.70$$

$$d = 0.0138$$

(2)  $I_{out}$

we know that

$$I_{max} + I_{min} = \frac{2dV_i}{R(1-d)^2}$$

Putting values

$$\Rightarrow \frac{2(0.0138)(50)}{13(1-0.0138)^2}$$

$$\Rightarrow \frac{2(0.0138)(50)}{13(0.97)^2}$$

$$\Rightarrow \frac{1.38}{12.23}$$

$$I_{max} + I_{min} \Rightarrow 0.11 \text{ Ampere (A)}$$

$$\Rightarrow \textcircled{3} \quad \bar{I}_i = I_L \times d$$
$$\Rightarrow 0.11 \times 0.0138$$
$$\Rightarrow 0.0015 \text{ A}$$

④ Inductance

$$L = \frac{R \bar{I} d}{2} (1-d)^2$$

Putting values

$$L = \frac{13(5 \times 10)^{-5}}{2} \times (1 - 0.0138)^2$$

$$L = \frac{13(5 \times 10^{-5})}{2} \times (0.97)$$

$$L = 0.00031 \text{ H}$$

Answer:-

Thank You