

Q No. 1

① 7809

A reinforced concrete ^{slab} is built integrally with its supports and consists of three equal spans, each with clear span of 15 ft. The factored live load is 160 psf and service floor finished load is 20 psf. Design slab using $f'_c = 4000 \text{ psi}$ and $f_y = 40 \text{ ksi}$. Draw sketch of your final diagram.

Solution :=

⇒ Three equal span concrete slab

⇒ Clear span = 15 ft

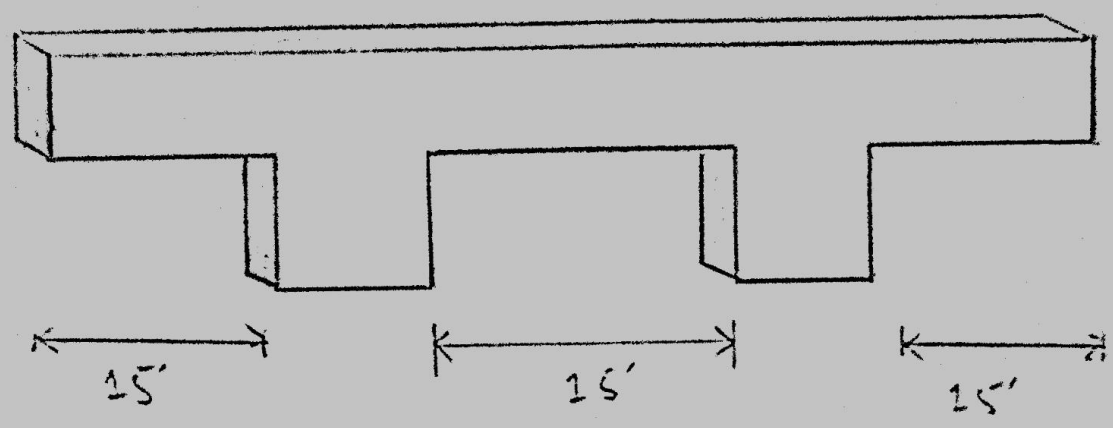
⇒ Factored live load = 160 lb/ft²

⇒ Service floor finished load = 20 psf

(2)
7809

$$\Rightarrow f'c = 4000 \text{ psi}$$

$$\Rightarrow Fy = 40 \text{ ksi}$$



STEP NO # 1 ::

Minimum Thickness

The minimum thickness formula

$$\text{is } t_{\min} = \frac{L}{28} = \frac{15}{28} = 6.4 \approx 6.5''$$

As we know that

$$Fy = 40 \text{ ksi}$$

So multiply a factor with this thickness

(3)
7809

$$\text{Factor} = \left(0.4 + \frac{f_y}{100} \right)$$

$$\text{Factor} = \left(0.4 + \frac{400}{100} \right)$$

$$\text{Factor} = 0.8$$

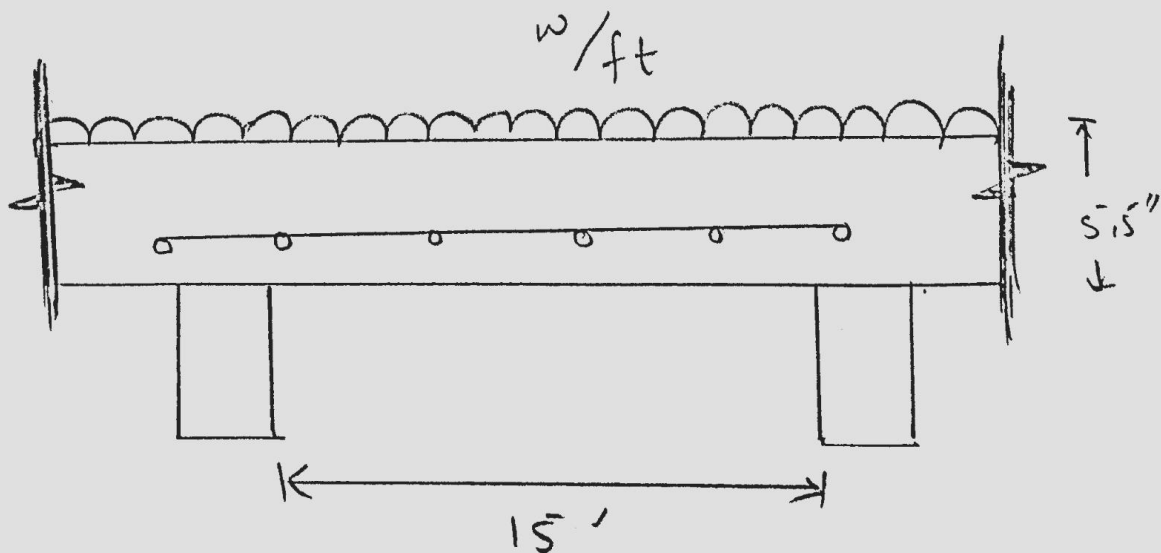
So minimum thickness
will be

$$6.5 \times 0.8$$

$$t_{\min} = 5.2 \approx 5.5''$$

STEP No # 2 ::

A Effective Depth.



(4)
7809

By Formula.

$$d = t - \text{clear cover} - \frac{1}{2} (\text{dia of main bar})$$

~~$$d = t - \text{clear cover}$$~~

$$d = 5.5 - 0.75 - \frac{1}{2} \left(\frac{5}{8} \right)$$

$$d = 4.5''$$

STEP NO # 3 ::

Self weight of Slab

we have formula

$$\frac{t}{12} + \gamma_{\text{concrete}}$$

$$\frac{5.5}{12} \times 150$$

\Rightarrow

$$68.75 \text{ lb/ft}^2$$

(5)
2002

STEP NO: 4:-

Total Factored Load.

factored live load = 160 lb/ft²

So

factored dead load = 1.2(20 + 68.75)
= 106.5 lb/ft²

Total Factored load = DL + LL
= 106.5 + 160
= 266.5 lb/ft²

Total Factored load = 0.2665 k/ft²

6
7869

STEP NO# 5:

Ultimate moment

As we know that

$$M_u = \frac{w_u \times L^2}{8} \times 12$$

$$M_u = \frac{0.2665 \times (15)^2}{8} \times 12$$

$M_u = 89.94 \text{ kip-inches}$

STEP No # 6:

Main Bar steel Area.

Trail No # 1

let depth of compression block

7
7909

$$a = 0.2 \times t$$

$$a = 0.2 \times 5.5$$

$$a = 1.1''$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times \left(d - \frac{a}{2}\right)}$$

$$A_{st} = \frac{89.94}{0.90 \times 46 \times \left(4.5 - \frac{1.1}{2}\right)}$$

$$A_{st} = 0.63 \text{ in}^2$$

Trail #2

$$a = \frac{A_s \times f_y}{0.85 \times f'_c \times b}$$

8
7809

$$a = \frac{Ase \times fy}{0.55 \times fc' \times b}$$

$$a = \frac{0.63 \times 40}{0.85 \times 4 \times 12}$$

$$a = 0.62 \text{ in}^2$$

$$A_{st} = \frac{M_u}{\phi \times fy \times \left(d - \frac{a}{2} \right)}$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times \left(4.5 - \frac{0.6}{2} \right)}$$

$$A_{st} = 0.59 \text{ in}^2$$

Trail #3

$$a = \frac{0.59 \times 40}{0.85 \times 4 \times 12} = 0.57''$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times \left(4.5 - \frac{0.57}{2} \right)}$$

$$A_{st} = 0.59 \text{ in}^2$$

So we will use ~~are~~

$$A_{st} = 0.59 \text{ in}^2$$

(9)
7809

STEP NO # 7 ∴

Area of steel for distribution reinforcement

$$A_{min} = 0.002 \times b \times t$$

$$= 0.002 \times 12 \times 5.5$$

$$A_{min} = 0.132 \text{ in}^2$$

↳ For Grade 40 steel.

STEP NO # 8 ∴

Spacing for main bar.

$$\text{Spacing} = \frac{A_b}{A_s} \times 12$$

10
7809

Use ~~10#~~ #6 bar dia = $\left(\frac{6}{8}\right)''$

$$\text{Area} = \frac{\pi}{4} \left(\frac{6}{8}\right)^2$$

$$\text{Area} = 0.442 \text{ in}^2$$

STEP No# 9 ∴

Spacing for distribution bars.

$$\text{Spacing} = \frac{A_b}{A_{st}}$$

Use #5 bars so

$$\text{dia} = \left(\frac{5}{8}\right)''$$

(11)
7809

$$\text{Area} = \frac{\pi}{4} \left(\frac{5}{8}\right)^2$$

$$\text{Area} = 0.31 \text{ in}^2$$

$$\text{Spacing} = \frac{0.31}{0.132} \times 12$$

$$\text{Spacing} = 28.1'' \approx 28'' \text{ c/c}$$

STEP No # 10 :-

Sketch.

$$f'_c = 4 \text{ ksi}$$

$$F_y = 40 \text{ ksi}$$

Main steel #6 at 9" c/c

Distribution steel #5 at 28" c/c

12
7809

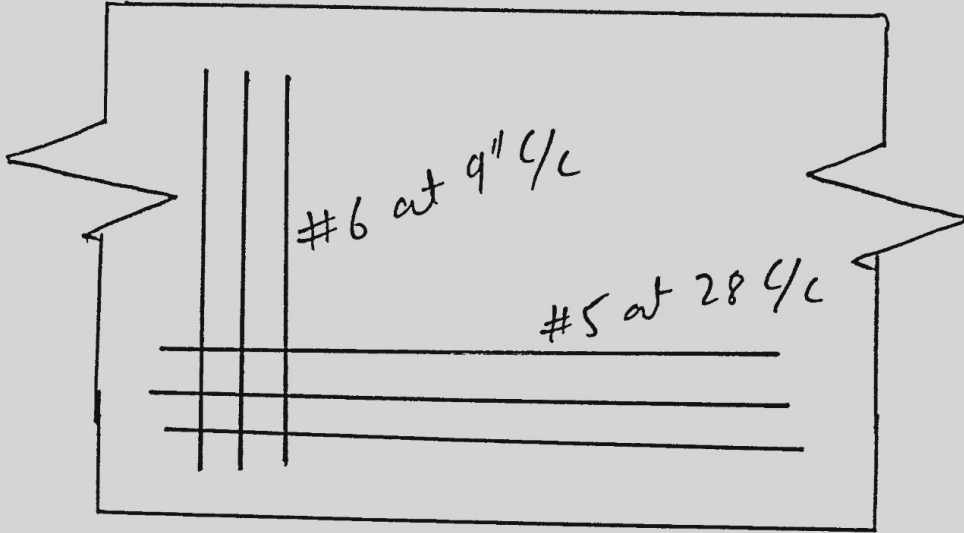


Diagram.

Q No. 2

(13)

A simply supported rectangular beam 16 inch wide having an effective depth of 22 inches carries a total factored load of 9.4 kips/ft. (excluding self weight of beam) on a 20-ft. clear span. It is reinforced with 7.62 in^2 of tensile steel which continues uninterrupted into the support. If $f'_c = 4000 \text{ psi}$ and $f_y = 60000 \text{ psi}$. using #3 vertical - U stirrup. Design the web reinforcement. Draw a sketch of your final diagram.

Solution :-

P.T.O

14
7809

Given Data :-

$$\text{width of beam} = 16''$$

$$\text{Effective depth} = 22''$$

$$\text{Total Factored load} = 9.4 \text{ Kips/ft}$$

$$\text{clear span} = 20 \text{ ft}$$

$$f'_c = 4000 \text{ psi}$$

$$f_y = 60000 \text{ psi}$$

Solution :-

unit load of beam

$$\underline{\text{is}} = b \times r_c$$

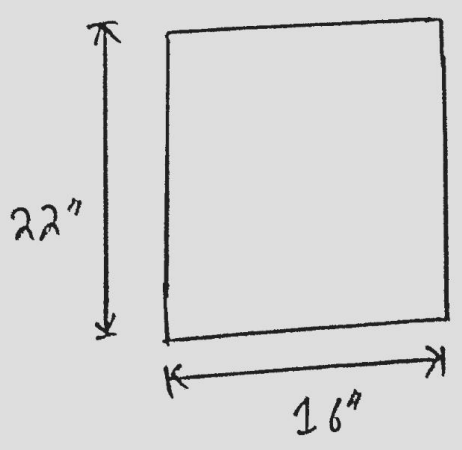
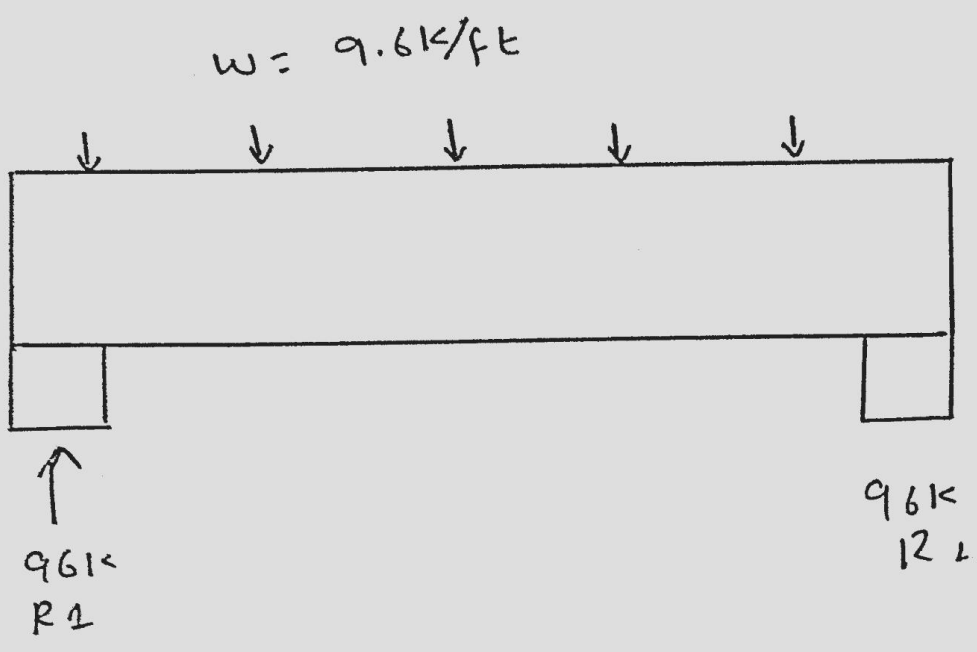
$$= \frac{16}{12} \times 150$$

$$= 200 \text{ lb/ft}$$

$$= 0.2 \text{ K/ft}$$

15
7809

Total Factored load = $9.4 + 0.2$
 $= 9.6 \text{ k/ft.}$



16
7869

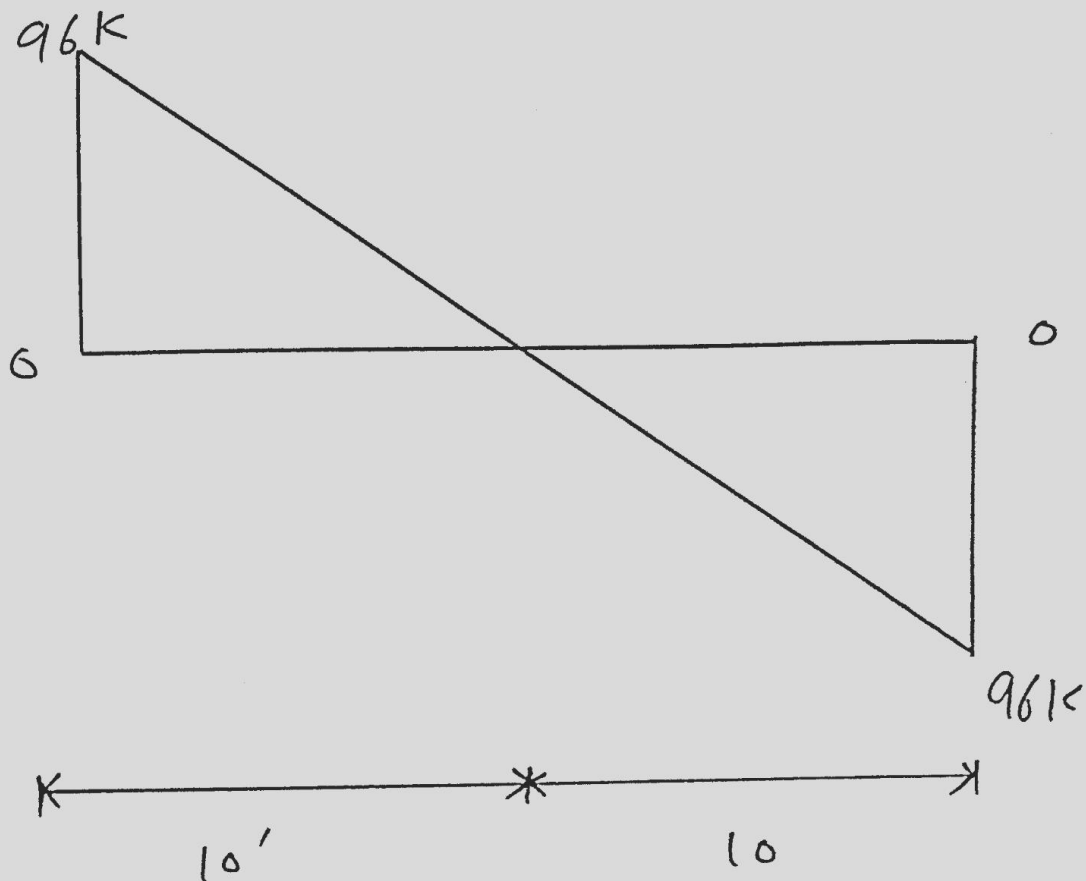
STEP NO # 1 :-

Finding value of R_1 and R_2

$$\underline{\text{total load} = \frac{9.6 \times 20}{2} = 96\text{K}}$$

STEP NO # 2 :-

Shear Force diagram.

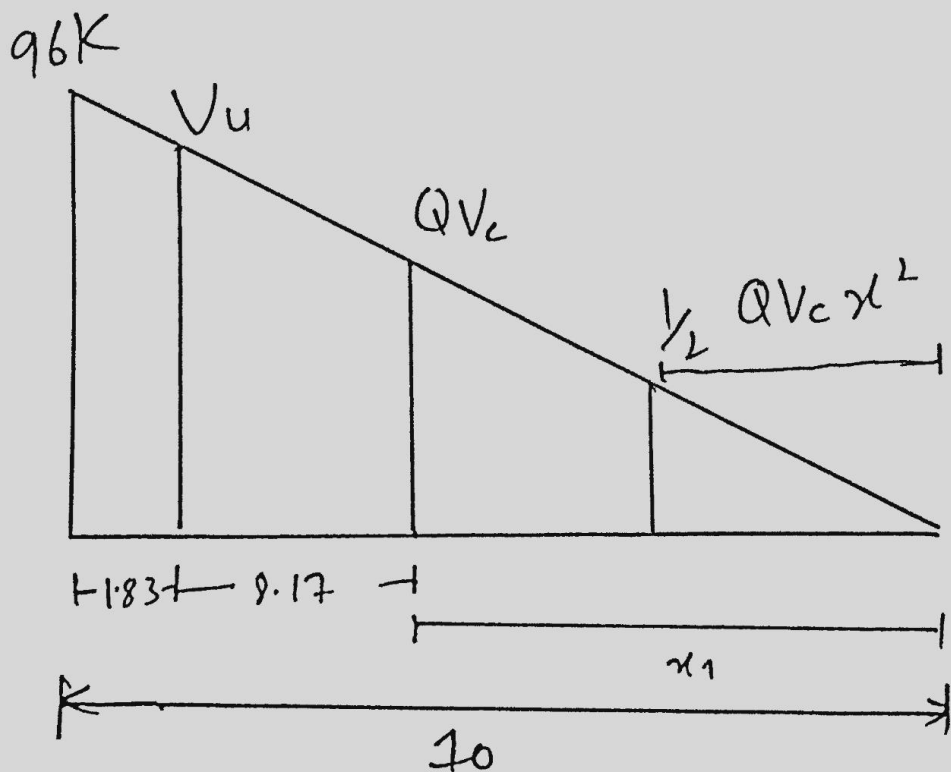


17
7809

STEP NO# 3 :-

value of Criticle stress and its location.

Critical location is located distance d from face of support $d = 22'' = 1.83'$
value of Criticle stress at distance \hat{d} by similarity triangle.



18
7809

From similar Δ 's $\frac{96}{70} = \frac{V_u}{8.17}$

$$V_u = 78.43k$$

STEP NO # 4 :

Finding ϕV_c and $\frac{1}{2} \phi V_c$

and also finding its
distance from zero shear

to right side.

$$\phi V_c = \phi \times L \times \sqrt{f'_c} \times b_w \times d$$

$$\phi V_c = \frac{0.75 \times 2 \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$\phi V_c = 33.40k$$

⇒ Location of ϕV_c by 19
Similarity of $\Delta S'$ 7809

$$\frac{96}{400} = \frac{33.40}{x_1}$$

$$x_1 = 3.48'$$

Now

$$\Rightarrow \frac{1}{2} \phi V_c = \frac{33.40}{2} = 16.70 \text{ k}$$

Location of $\frac{1}{2} \phi V_c$

$$= \frac{96}{10} = \frac{16.70}{x_2}$$

$$x_2 \pm 1.74'$$

20
7809

STEP No # 5 :-

Finding values of

$$\phi V_s [V_u = \phi V_s + \phi V_c]$$

So

$$\phi V_s = V_u - \phi V_c$$

$$\phi V_s = 78.43 - 33.40$$

$$\phi V_s = 45.03 \text{ k}$$

STEP No # 6 :-

Check section Adequacy.

$$\phi \times 8 \times \sqrt{f'_c} \times b \times d = \frac{0.75 \times 8 \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$= 133.57 \text{ k}$$

$133.57 \text{ k} > \phi V_s$ (mean section is adequate)

STEP No# 7 :=

(21)
7909

Check mini Spacing For
Stirrups.

$$\phi \times 4 \times \sqrt{f'_c \times b_w \times d} \Rightarrow \frac{0.75 \times 4 \times \sqrt{4000 \times 16 \times 22}}{1000}$$

$$= \boxed{66.79} > \phi_{vs} = 44.031k$$

Spacing will be selected from these four conditions.

① $S_{max} = 24''$

② $\frac{d}{2} = \frac{22}{2} = 11''$

③ $S_{max} = \frac{A_u \times f_y}{0.75 \times \sqrt{f'_c} \times b_w}$

22
7809

$$A_u = \frac{\pi}{4} \left(\frac{3}{8}\right)^2 \therefore A_u = 0.11 \times 2 = 0.22$$

$$J_{max} = \frac{0.22 \times 60000}{0.75 \times \sqrt{4000 \times 16}}$$

$$\begin{aligned} \textcircled{4} \quad J_{max} &= \frac{A_u \times f_y}{50 \times b_w} \\ &= \frac{0.22 \times 60000}{50 \times 16} \\ &= 16.50 \end{aligned}$$

From the above 4
Condition least value of
spacing for #3 U Stripped
will be selected so
 $S_{max} = 12" c/c$

STEP No # 8 :-

(23)
7909

Spacing of stirrup from
critical section:

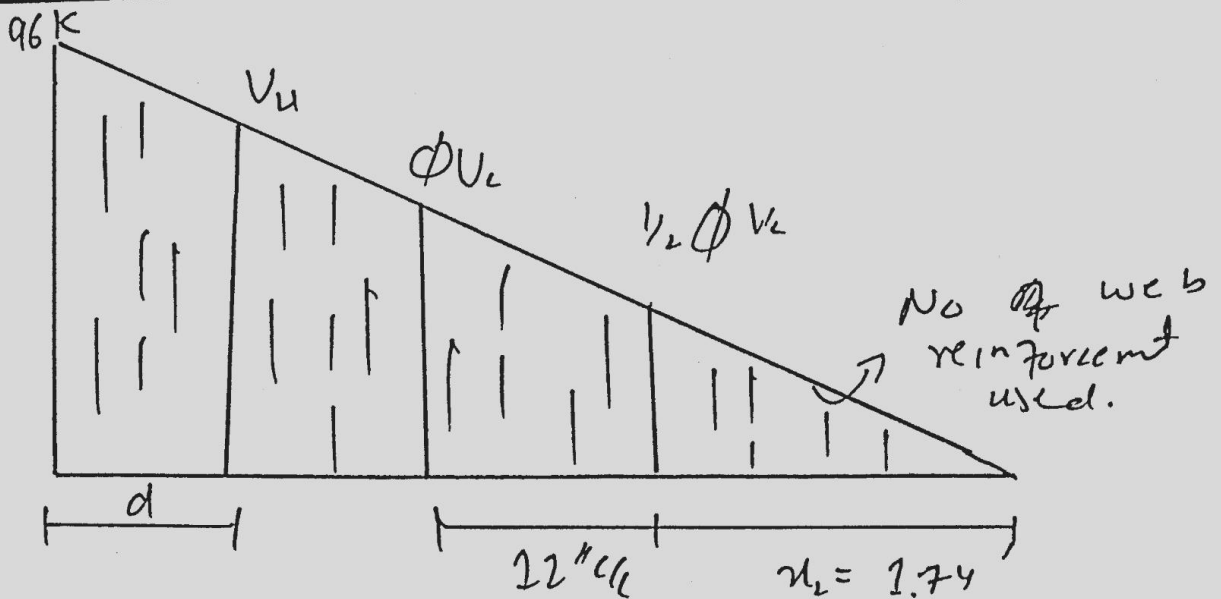
$$J = \frac{\phi \times A_{ux} \times f_y \times d}{V_u - \phi V_c}$$

$$V_u - \phi V_c$$

$$J = \frac{0.75 \times 0.22 \times 80 \times 22}{78.43 - 33.40}$$

$$J = 4.84 \approx 5'' \text{ c/c}$$

STEP No # 9 :-



First stirrup from face of
support $= \frac{J}{2} = 2.5 \approx 2''$

Q No. 3

24 7809

Calculate the axial ultimate load carrying capacity of a 12 inch square tied column reinforcement with 4 # 9. Ties are # 3 inches. use $f'_c = 4000 \text{ psi}$ and $f_y = 60 \text{ ksi}$. Also design necessary spirals.

Solution :-

P.T.O

25
7809

STEP No # 1 ::

Gross area of concrete

$A_g = b \times b$ (since it is square column)

$$A_g = 12 \times 12$$

$$A_g = 144 \text{ in}^2 \text{ (Actual)}$$

STEP No # 2 ::

Area of steel.

$$A_s = 5\% \text{ of } A_g$$

$$A_s = 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

(26) 7909

STEP NO#3 ::

Ultimate load Carrying Capacity.

$$P_u = \phi \times 0.80 \times [0.85 \times f'_c \times (A_g - A_s) + A_s \times f_y]$$

$$P_u = 0.65 \times 0.80 [0.85 \times 4 [144 - 7.2] + 7.2 \times 6]$$

$$P_u = 466.50$$

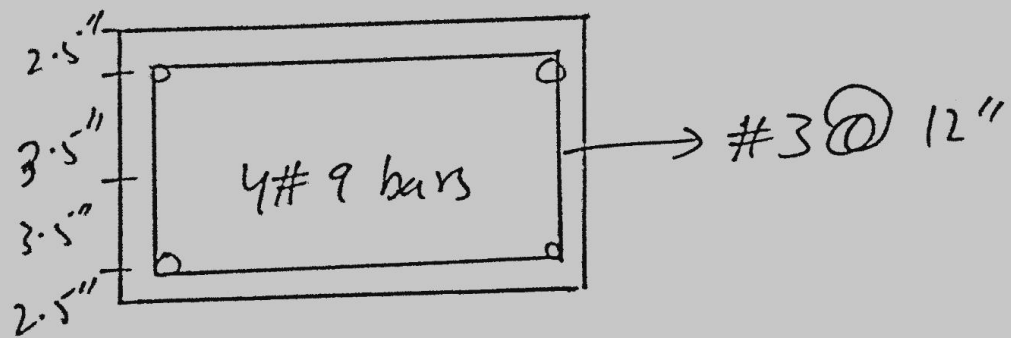
STEP NO#4 ::

Sketch and design of ties

From the below value we will chose the least value in all values.

27
7809

- ① $16 \times \text{dia}$ of long bar = $16 \times 9/8 = 18''$
- ② $48 \times \text{dia}$ of the bar = $48 \times 3/8 = 18''$
- ③ Least colum dimension = $12''$
so c/c distance b/w ties = $12''$



Since it is a tied square column so there is no spiral stirrup used the stirrups use is of rectangular shape due to the specification of the structure thus we will use ties stirrups instead

Q No. 4

(28) 7-8-09

Design a square footing to support a 16 inches square tied concentrically loaded column. The column carries an un-factored axial D.L of 400 kips and an axial L.L of 120 kips. The base of footing is 5ft. below final grade and the allowable soil pressure is 2.50 ksf. Use $f'_c = 3 \text{ ksi}$, $f_y = 60 \text{ ksi}$ and $\gamma_{\text{soil}} = 120 \text{ pcf}$. Draw sketch of your final diagram.

Solution \square

29
7809

STEP No# 1 ∴

$$h = 24''$$

STEP No# 2 ∴

$$\text{Total weight} = \text{wt of soil} + \text{wt of RF}$$

$$= 3 \times 120 + 2 \times 150$$

$$= 660 \text{ psf}$$

$$\text{Total weight} = 0.660 \text{ ksf}$$

STEP No# 3 ∴

Effective bearing capacity

$$q_e = q_u - w$$

$$= 2.50 - 0.660$$

$$q_e = 1.84 \text{ ksf}$$

STEP No# 4 ∴

Area of foundation

$$A_{req} = \frac{\text{service load}}{q_e} = \frac{100 + 120}{1.84} = \boxed{1.84 \text{ ksf}}$$

STEP NO# 5

(30)
7809

Since foundation is square

$$\text{Area} = b \times b = 119.57 \Rightarrow B \approx 11'$$

STEP NO# 6

upward bearing capacity
of soil:

$$q_{up} = \frac{\text{Factored load}}{(B)^2}$$

$$q_{up} = \frac{1.2 \times 100 + 5.6 \times 120}{11^2}$$

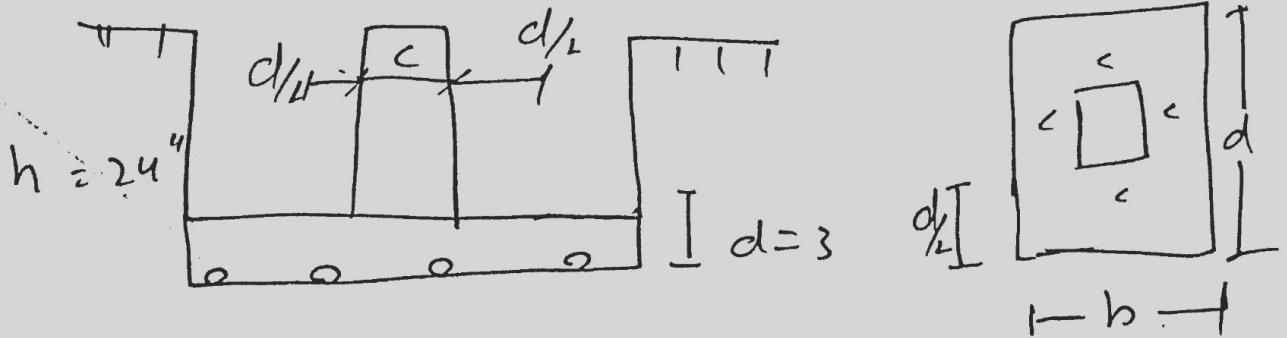
$$q_{up} = 2.58 \text{ k/ft}^2$$

STEP No # 7

31
7809

Punching Shear.

$$b_o = 4 \times (c + d)$$



Take #8 bar
Bar

$$d = h' - c.c - d_o \text{ of bar} - \frac{1}{2} db$$
$$= 24 - 3.1 - \frac{1}{2} (1) = 19.5''$$

$$b_o = 4 \times (16 + 9.5)$$

$$b_o = 142''$$

STEP No # 8

$$V_{u2} = q_{up} \times [l^2 - (c+d)^2]$$

$$V_{u2} = 2.58 \times \left[\frac{11^2 (16 + 19.5)^2}{12} \right]$$

$$V_{u2} = 289.601$$

STEP No# 9

32
7809

$$Q_{Up} = Q \times 4 \sqrt{f_c'} \times b \times d$$

$$Q_{Up} = \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 193}{1000}$$

$$Q_{Up} = 525.39 \text{ k}$$

STEP No# 10

Beam Shear one way
Shear check

$$V_u = q_{up} \times B \times \left(\frac{B}{2} - \frac{C}{2} - d \right)$$

$$V_u = 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{12} - \frac{193}{2} \right]$$

$$V_u = 90.95 \text{ k}$$

33
7009

STEP NO# 11

Self shear Capacity

$$Q V_c = \frac{Q \times L \times \sqrt{f_{ck}} \times [11 \times 12 \times 1.6]}{1000}$$

$$= 110.04 \text{ k} > V_u$$

$$= \text{OK} \quad \text{OK!}$$

STEP # 12

ultimate moment

$$M_u = \frac{q_{up} \times B}{8} \times (B - c)^2$$

$$= \frac{2.58 \times 11}{8}$$

$$M_u = \left(11 - \frac{16}{12}\right)^2$$

(34) 7809

$$M_u = 331.49 \text{ k}' \approx 3977.93 \text{ k}$$

STEP No # 13

Area of steel for
main bar by
trial and repeat
method.

Trial # 1

$$\text{let } a = 0.2 \times h = 0.2 \times 24 = 4.8''$$

$$A_s = \frac{M_u}{\phi \times f_y \times \left(d - \frac{a}{2}\right)}$$

$$A_s = \frac{3977.93}{0.90 \times 60 \times \left(11 - \frac{4.8}{2}\right)}$$

$$A_s = 8.56 \text{ in}^2$$

35
7809

Trail N2#2

$$a = \frac{A_s \times f_y}{0.85 \times f'_c \times b}$$

$$a = \frac{8.56 \times 60}{0.85 \times 3 \times 11 \times 12}$$

$$a = 1.53''$$

$$A_s = \frac{3977.93}{0.90 \times 60 \times \left(11 - \frac{1.53}{2}\right)}$$

$$A_{st} = 7.197 \text{ in}^2$$

(36) 7809

Trial #3

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$A_{st} = \frac{3977.93}{0.90 \times 60 \left(11 - \frac{1.28}{2}\right)}$$

$$A_{st} = 7.1 \text{ in}^2$$

So that area = 7.1 in²

STEP No # 14

Check minimum reinforcement
by the following method.

reinforcement
3

37

78.9

a)

$$\begin{aligned}
 A_{smin} &= 0.0018 \times B \times h \\
 &= 0.0018 \times (11 \times 12) \times 24 \\
 A_{smin} &= 5.76 \text{ m}^2
 \end{aligned}$$

b)

$$\begin{aligned}
 A_{smin} &= \frac{200}{f_y} \times B \times d \\
 A_{sim} &= \frac{200}{68000} \times (11 \times 12) \times 19.5 \\
 &= 8.58 \text{ in}^2
 \end{aligned}$$

c)

$$\begin{aligned}
 A_{sim} &= \frac{3 \times \sqrt{f'c}}{f_y} \times B \times d \\
 &= \frac{3 \times \sqrt{3000}}{68000} \times (11 \times 12) \times 19.5 \\
 A_{smin} &= 7.05 \text{ m}^2
 \end{aligned}$$

From the above value $\textcircled{58}$ 7809
will be select greater
in all

$$A_{smin} = 8.58 \text{ in}^2$$

STEP NO # 15

$$A_b = 0.785 \text{ in}^2$$

$$\text{No of bars} = \frac{A_s}{A_b} = \frac{8.58}{0.783}$$

$$= 10.92 \approx 11 \text{ bars}$$

in each direction.

NAME → Asad ullah

SECTION → A

ID → 7809

SUBJECT → PRCOI

SUBMITTED
To → Engr FAWAD Khan

Exam → Final Term

Date → 26/June/2020