

Name: M. Kamran

ID No: 7888

PRCD-I

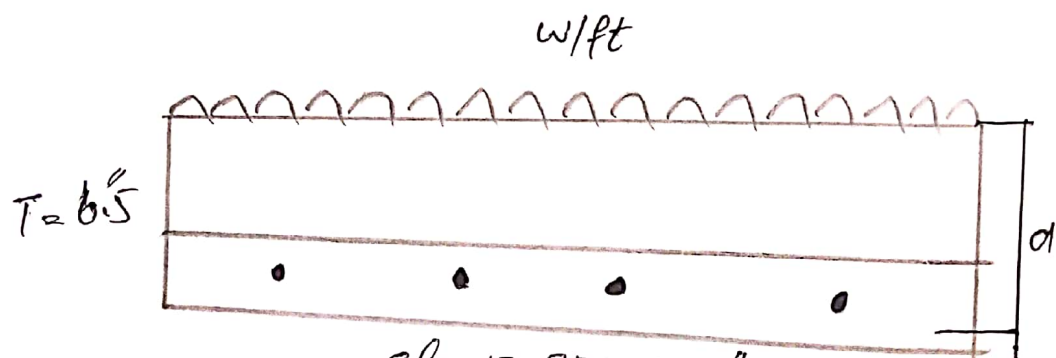
Q - No - 01 \Rightarrow Given data :-

- \rightarrow 3 equal Span concrete Slab
- \rightarrow clear Span b/w Supports = 15 ft
- \rightarrow factored live load = 160 lb/ft²
- \rightarrow Service floor finish load = 20 lb/ft²
- \rightarrow $f'_c = 4000$ psi
- \rightarrow $f_y = 40$ ksi

Solution :-

Step # 01 :- $t_{min} = \frac{L}{28} = \frac{15}{28} \times 12 = 6.5''$

Step # 02 :- Effective depth.



$$\begin{aligned} d &= T - (\text{clear cover} - \frac{1}{2} (d \cdot M \cdot B)) \\ &= 6.5 - (0.75 - \frac{1}{2} (4/8)) \\ &= 6'' \end{aligned}$$

Step # 03 :- Self Weight of Slab

$$= \frac{t}{12} \times \gamma_{\text{concrete}}$$

$$= \frac{6.5}{12} \times 150 = 81.25 \text{ PSF}$$

Step # 04 :- Total factored load

$$W_u = 1.2(81.25 \times 20) + 160$$

$$= 281.5 = 0.281 \text{ KSF}$$

Step # 05 :-

Ultimate Moment

$$M_u = \frac{W_u \times L^2}{8} = \frac{0.281 \times 15^2 \times 12}{8} = 94.8 \text{ K''}$$

Step # 06 :-

Area of Steel for main bars by trial and Repeat methods.

Trial # 01 :-

$$\text{let } d = 0.2 \times T \Rightarrow 0.2 \times 6.5 = 1.3$$

$$A_s = \frac{M_u}{\phi \times f_y \times (d - \frac{a}{2})} = \frac{94.8}{0.9 \times 60 \times (6 - \frac{1.3}{2})} = 0.32 \text{ in}^2/\text{ft}$$

Trial # 02 :- $a = \frac{M_u \times f_y}{0.85 \times f'_c \times b} = \frac{0.32 \times 60}{0.85 \times 4 \times 15} = 0.37$

$AS = \frac{M_u}{\phi \times f_y \times (d - \frac{a}{2})} = \frac{94.8}{0.90 \times 60 \left(6 - \frac{0.37}{2}\right)}$
 $= 0.30 \text{ in}^2/\text{ft}$

$a = 0.35$ $AS = 0.30 \text{ in}^2/\text{ft}$

Step # 07 :- Area of the steel for distribution bar

$AS_{min} = 0.0018 \times b \times t = 0.0018 \times 15 \times 6.5$
 $= 0.17 \text{ in}^2/\text{ft}$

Step # 08 :- Spacing for ~~distribution~~ ^{main} bar

$S = \frac{Ab}{AS} \times 12 = \frac{0.20}{0.30} \times 12 = 8 \approx 8 \frac{1}{2} \text{ c/c}$

Step # - 09 :- Spacing for distribution bar
 let try # 4 bar

$S = \frac{Ab}{AS} \times 12$

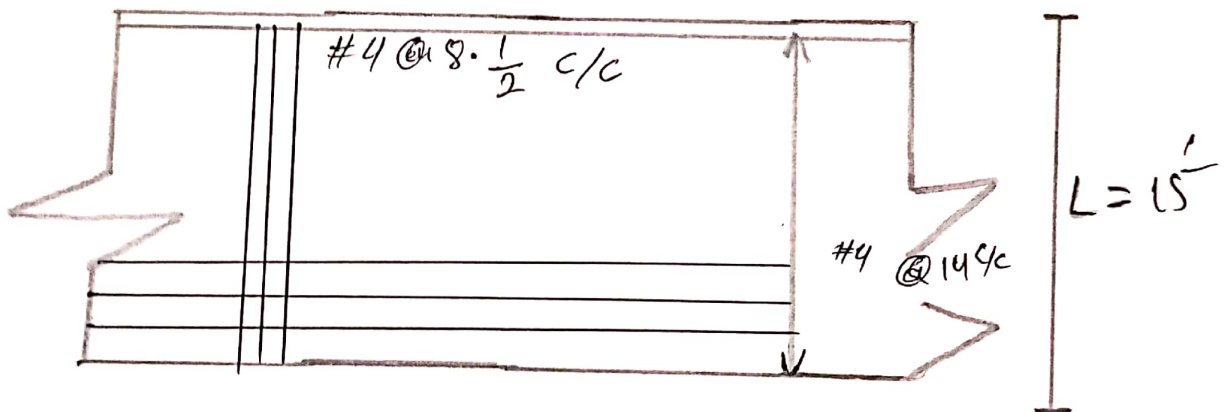
$= \frac{0.20}{0.175} \times 12 = 13.71 \approx 14$

Step # 10 = final Summary:-

$$f'c = 4 \text{ ksi} \quad f_y = 40 \text{ ksi} \quad \tau = 6.5$$

Main Steel bar # 4 = at $8 \cdot \frac{1}{2}$ c/c

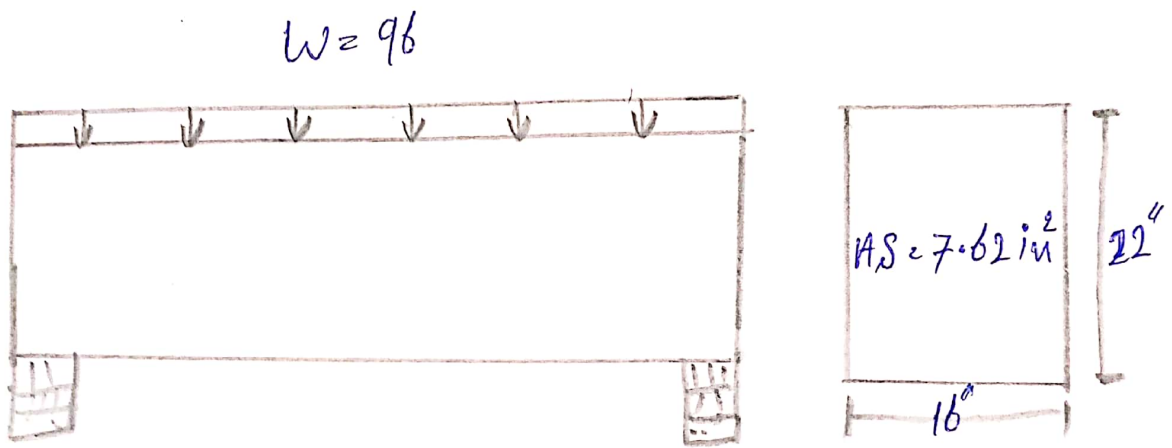
Distribution Steel bar # 4 at 14 c/c



Q No. 02.

A Simple rectangular beam:

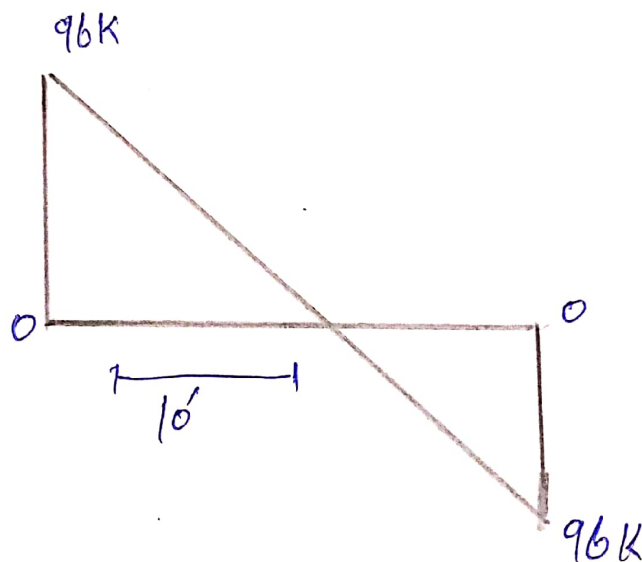
Given data:- width = 16"
 $d = 22''$ factored load = 9.6 k/ft
clear span = 20' Tensile steel Area = 7.62 in²



Step # 01 :- find the R_1 and R_2

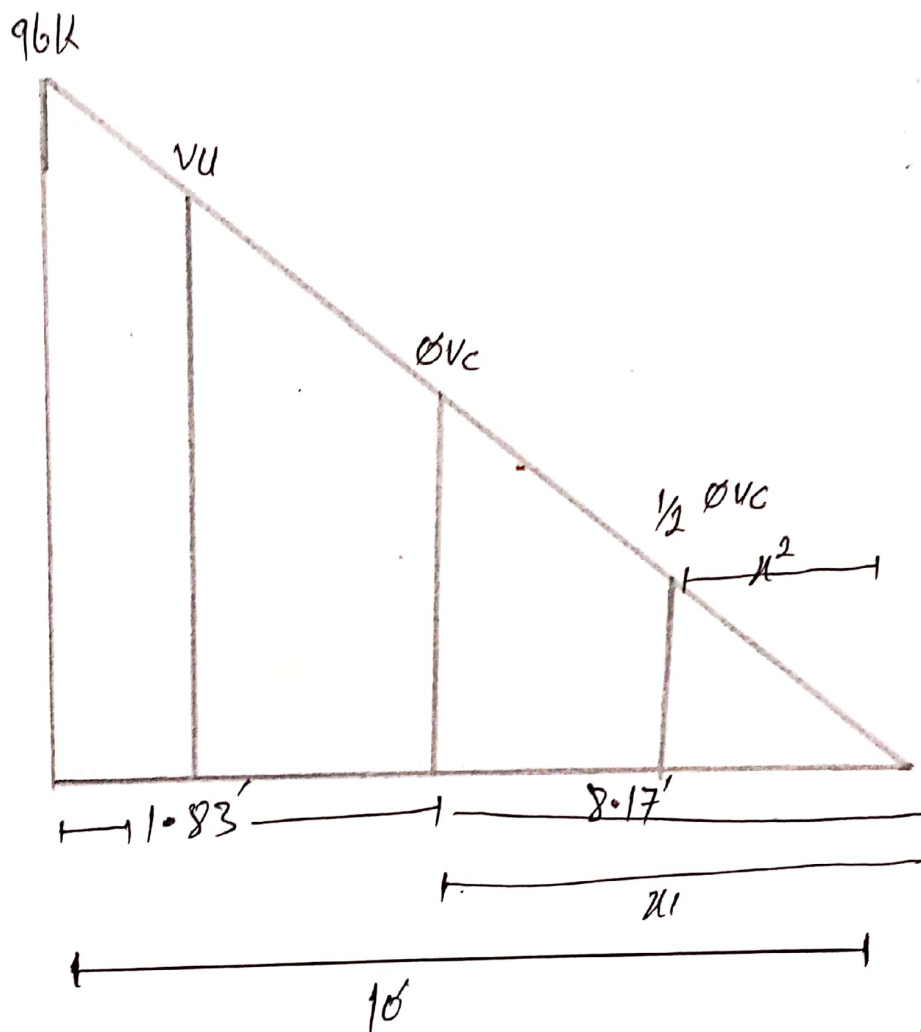
$$= 9.6 \times \frac{20}{2} = 96 \text{ k}$$

Step # 02 :-



Step # 03 :- find the value of critical stress v_u and its location.

As we know that critical section is located at distance "d" from face of support = 1.83
value of critical shear at distance "d" by
similarity of Δs



Step # 04 :- find the value of ϕv_c and $\frac{1}{2} \phi v_c$
and also its distance from zero
shear to right side.

$$\phi_{vc} = \phi \times 2 \times \frac{\sqrt{f_c'} \times b_w \times d}{1000}$$

$$= \frac{0.75 \times 2 \times \sqrt{4000} \times 16 \times 22}{1000} = 33.40 \text{ k}$$

location of ϕ_{vc} by Similar Δ, S

$$\frac{96}{10} = \frac{33.40}{x_1} \Rightarrow x_1 = 3.47$$

$$\text{Now } \frac{1}{2} \phi_{vc} = \frac{33.40}{2} = 16.70 \text{ k}$$

$$\text{location of } \frac{1}{2} \phi_{vc} \Rightarrow \frac{96}{10} = \frac{16.70}{x_2}$$

$$x_2 = 1.73$$

Step # 05 :- values of ϕ_{vs}

$$V_u = \phi_{vs} + \phi_{vc}$$

$$\phi_{vs} = V_u - \phi_{vc} \Rightarrow 78.43 - 33.40$$

$$= 45.03 \text{ k}$$

Step # 06 :- check on section adequacy

$$\phi_{vs} \times \sqrt{f_c'} \times b_w \times d = \frac{0.75 \times 8 \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$= 133.57 \text{ k} \text{ ---}$$

i.e

AS $\phi_{US} < \phi_{8 \sqrt{f_c} b_w d}$ Section is allow.

Step # 07 :-

check on maximum Spacing for stirrups -

$$\phi_{4 \sqrt{f_c} x b_w d} = \frac{0.75 \times 4 \sqrt{4000} \times 16 \times 22}{1000}$$

$$= 66.79 \text{ Ksp}$$

$$AS \phi_{4 \sqrt{f_c} b_w d} > \phi_{US} = 45.03 \text{ K}$$

So mini spacing will be selected from the following four condition.

$$\textcircled{1} S_{max} = 24''$$

$$\textcircled{2} \frac{d}{2} = \frac{22}{2} = 11''$$

$$\textcircled{3} S_{max} = \frac{A_u \times f_y}{0.75 \times \sqrt{f_c} \times b_w} = 17.40''$$

$$\textcircled{4} \frac{A_u \times f_y}{50 \times b_w} = \frac{0.22 \times 60000}{50 \times 16} = 16.50''$$

from above four condition least value of spacing for #3, 2 legged stirrup will

Selected

$$So S_{max} = 11'' \text{ c/c}$$

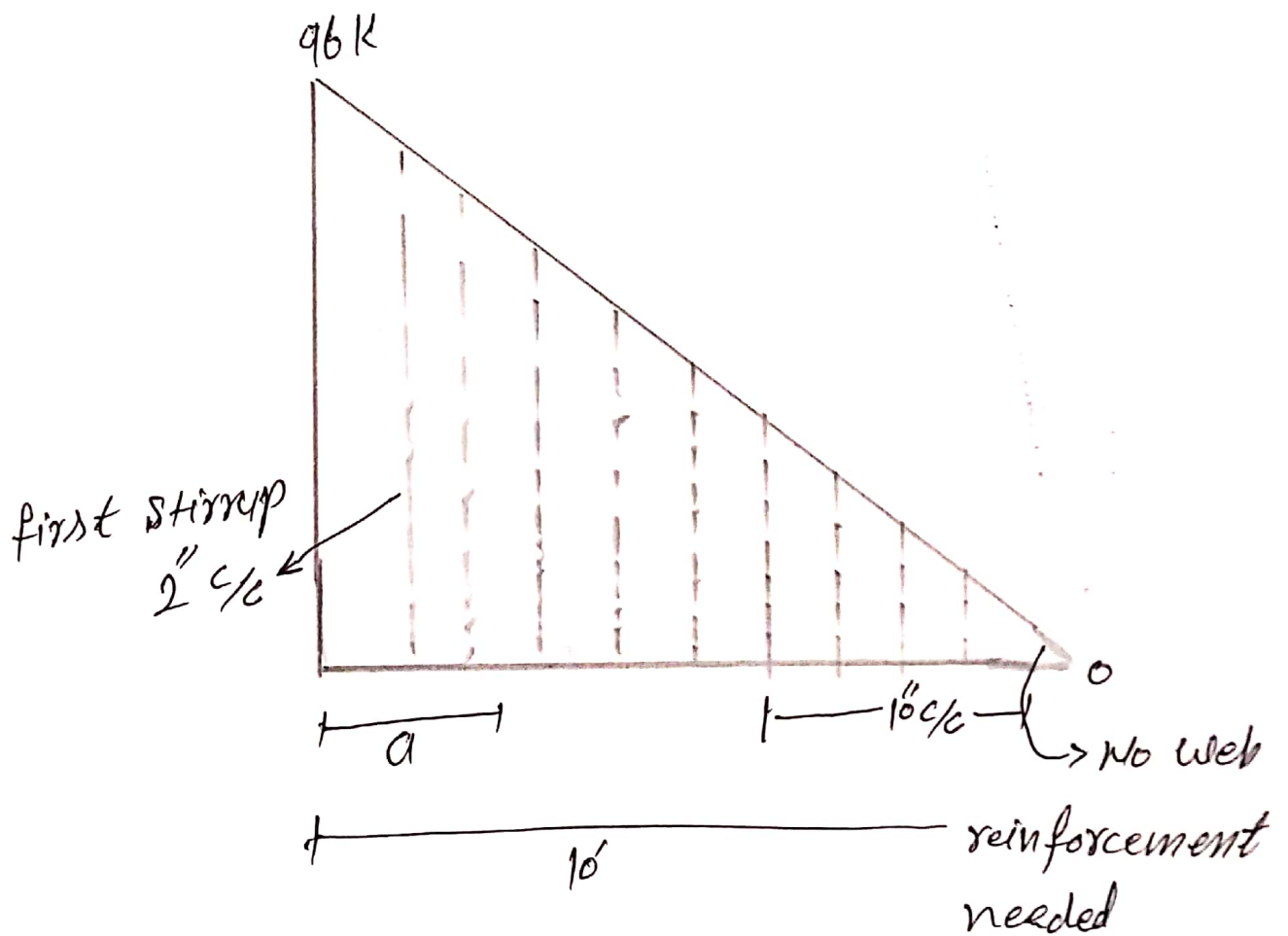
Step # 08 :-

$$S = \frac{\phi RAV \times f_y \times d}{VU - \phi VC} = \frac{0.75 \times 0.22 \times 60 \times 22}{78.43 - 33.40}$$

$$S = 5\%$$

first stirrup from start = $\frac{S}{2} = \frac{5}{2} = 2.5 \approx 2$

Step # 09 :-



QUESTION - No - 03 :-

Calculate the axial ultimate
design necessary spirals -

Step # 01 :- find gross area of
concrete,

$$A_g = b \times b \text{ (since it is square tied column)}$$

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

Step # 02 :- find the Area of Steel

$$\text{Since } A_s = 5\% \text{ of } A_g$$

$$= 0.05 \times 144 = 7.2 \text{ in}^2$$

Step # 03 :- ultimate load Bearing capacity.

$$\begin{aligned} P_u &= \phi \times 0.8 [0.85 \times f'_c \times (A_g - A_s) + A_s \times f_y] \\ &= 0.65 \times 0.8 [0.85 \times 4 (144 - 7.2 \times 60)] \end{aligned}$$

$$P_u = 466.5 \text{ k}$$

Step # 04 :-

Sketch and design of Ties

(c/c to distance)

From the below value we always take the least value of all thus-

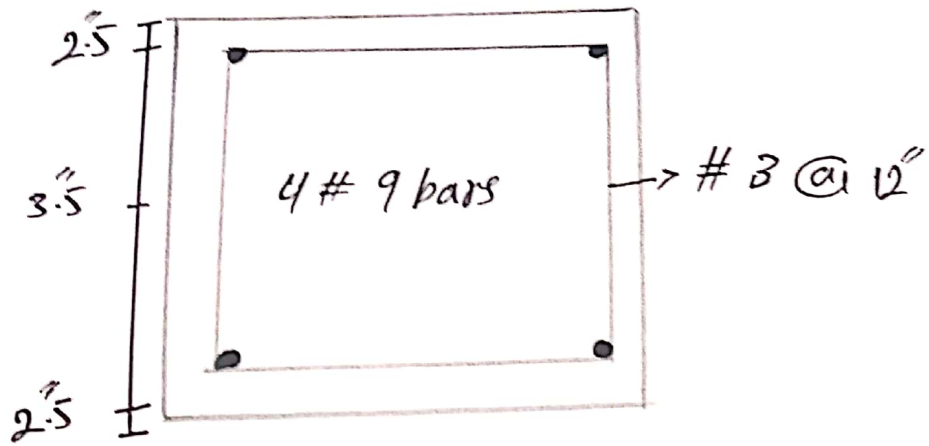
$$\textcircled{1} 16 \times \text{dia of long bar} = 16 \times \frac{9}{8} = 18''$$

$$\textcircled{2} 48 \times \text{dia of tie bar} = 48 \times \frac{3}{8} = 18''$$

$$\textcircled{3} \text{least column dimension} = 12''$$

So c/c distance b/w ties = ~~18~~ 12''

P - T - O



⊗ Since it is a tied square column so there no spiral stirrup used the stirrup used is of recta shape due to the specification of the structure this we will use Tie stirrups instead -

QUESTION - No - 04 =

Design a Square footing ——— Sketch of your final design -

Step # 01:- Let $h = 24''$

Step # 02:- Total Weight = Wt of Soil + Wt of RL

$$= 3 \times 120 + 2 \times 150$$

$$= 660 \text{ PSF} = 0.660 \text{ KSF}$$

Step # 03:- Effective Bearing capacity

$$q_e = q_a - u$$

$$q_e = 2.5 - 0.660$$

$$q_e = 1.84 \text{ KSF}$$

Step # 04:- Required Area for foundation,

$$\text{Area} = \frac{\text{Service load}}{q_e} = \frac{100 + 120}{1.84}$$

$$= 119.57 \text{ ft}^2$$

Step - #05 :-

Since foundation is square

$$\text{Area} = b \times b = 119.57 \Rightarrow B = 11$$

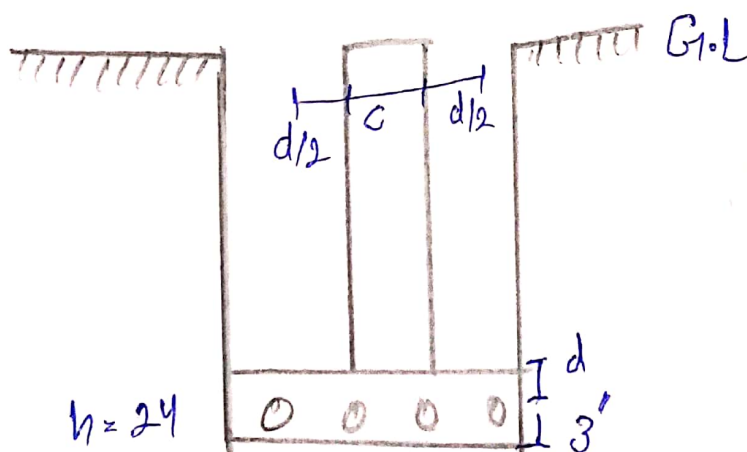
Step - 06 :- upward bearing capacity of soils-

$$q_{up} = \frac{\text{factored load}}{(B)^2} = \frac{1.2 \times 100 + 1.6 \times 120}{11^2}$$

$$q_{up} = 2.58 \text{ K/ft}^2$$

Step - # 07 :- punching shear

$$b_o = 4 \times (c + d)$$



P-T-O

$$d = 11 - c - \text{dia of bar} - \frac{1}{2} db$$

$$= 24 - 3 - 1 - \frac{1}{2} (1) = 19.5''$$

$$b' = 4 \times (16 + 19.5) = 142''$$

Table # 8 bar
dia = $\frac{18''}{8} = 1$

Step # 8 :-

$$V_{u2} = v_{up} \times [B^2 - (c+d)^2]$$

$$= 2.58 \times \frac{[11^2 - (16 \times 19.5)^2]}{12}$$

$$V_{u2} = 289.60 \text{ K}$$

Step # 9 :-

$$Q_{up} = \frac{0.75 \times 4 \times \sqrt{f'c} \times b \times d}{1000}$$

$$= \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5}{1000}$$

$$= 525.38 \text{ K}$$

Step # 10:- Beam shear/one way
Shear check.

$$V_{u1} = v_{up} \times B \left[\frac{B}{2} - \frac{e}{2} - d \right]$$

$$= 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{2} - \frac{19.5}{12} \right]$$

$$V_{u1} = 90.95 \text{ K}$$

Step # 11:- Self Shear capacity

$$\phi V_c = \phi \times 2 \times \sqrt{f_c} \times b \times d$$

$$= 0.75 \times 2 \times \sqrt{4000} \times (11 \times 12 - 16)$$

1000

$$= 110.04 \text{ K} > V_{u1} \Rightarrow \text{OK}$$

Step # 12:-

Ultimate Moment

$$M_u = \frac{v_{up} \times B}{8} \times (B - L)^2 = \frac{2.58 \times 11}{8} \times \left(11 - \frac{16}{12} \right)^2$$

$$M_u = 331.49 \text{ K} = 3977.93 \text{ K}^m$$

Step # 13 :- Area of Steel for Mainbars by Trial and Repeat Method

$$A_{smin} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24 \\ = 5.70 \text{ in}^2$$

$$A_{smin} = \frac{200}{f_y} \times B \times d = \frac{200}{60000} \times (11 \times 12) \times 19.5$$

Step # 14 :- check the main

Reinforcement by the following as method.

$$A_{smin} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24$$

$$A_{smin} = 5.7 \text{ in}^2$$



Step #: 15 :-

using # 8 bars

$$A_b = 1 \text{ m}^2$$

$$\text{No of bars} = \frac{8.85}{1 \text{ m}^2} = 9$$

= 9 bars in bars in each direction.