

NAME:

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I.D.:

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SUB:

STRUCTURE II

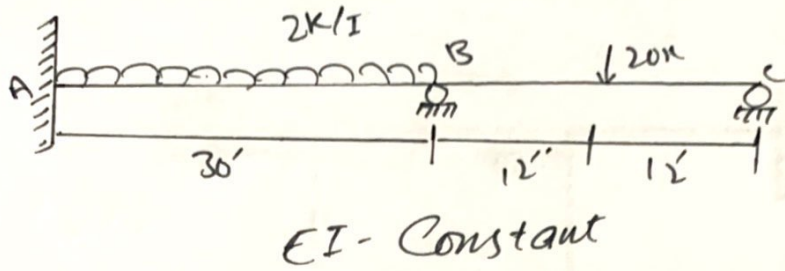
INST:

SIR ADEED

DPTT:-

CIVIL

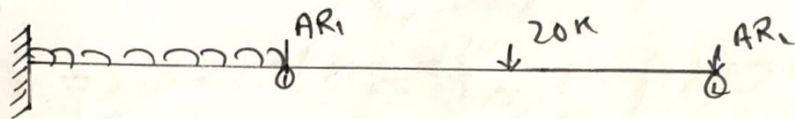
Q NO 18



Soln

$$S.I = 2^{\circ}$$

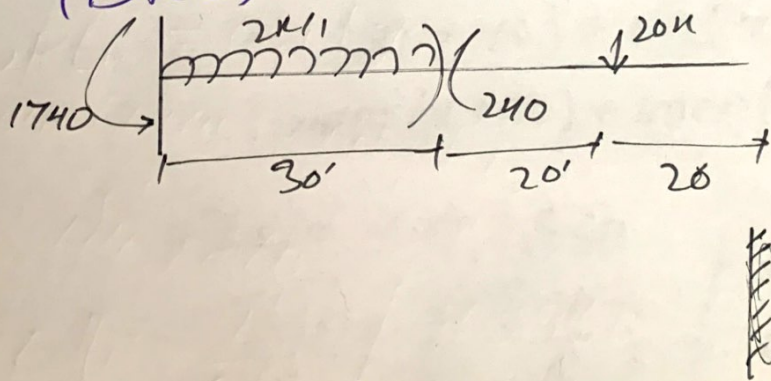
STEP 01:- Select redundant actions



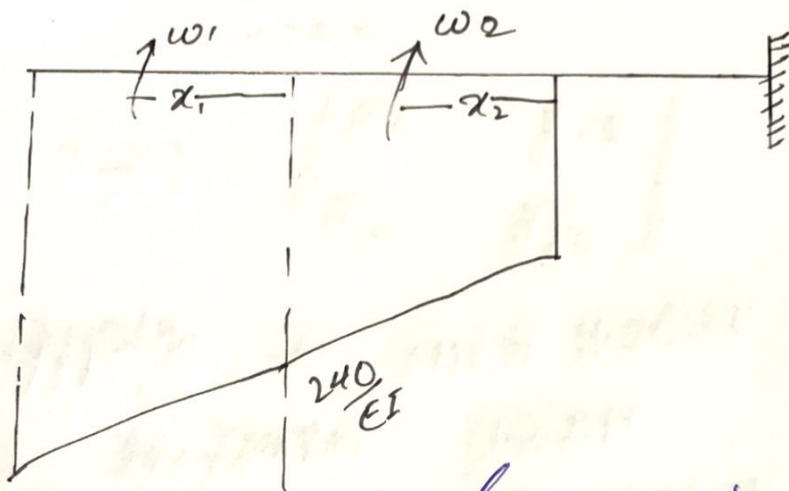
$$\begin{bmatrix} DRS_1 \\ DRS_2 \end{bmatrix} = \begin{bmatrix} ? \\ ? \end{bmatrix} \quad \begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} ? \\ ? \end{bmatrix}$$

$$[DRS] = [DRL] + F \times AR$$

STEP# 02 Compute the value of [DRL]



$$\begin{aligned} 20 \times 12 &= 240 \\ (20 \times 42) \times 2 &+ 30 \times 15 \\ &= 1740 \end{aligned}$$



$$1740/EI \quad \omega_1 = \left(\frac{240+0}{2EI} \right) \times 12 = 1440/EI$$

$$\omega_2 = \frac{1}{n+1} \times (b \times h) = \frac{1}{2+1} \left(\frac{1100}{EI} \right) \times 30$$

$$= 11000/EI$$

$$x_1 = \frac{1}{3} \left(\frac{a+2b}{a+b} \right) = 4'$$

$$x_2 = \frac{3}{n+2} \times b = \frac{3}{2+2} (30) = 22.5'$$

$$DRL_1 = \omega_1 (x_1 + 30) = 48940$$

$$DRL_2 = \omega_1 (x_1 + 40) + \omega_2 (x_2 + 12)$$

$$= 1440 (4 + 40) + 11000 (22.5 + 12)$$

$$DRL_2 = 442860$$

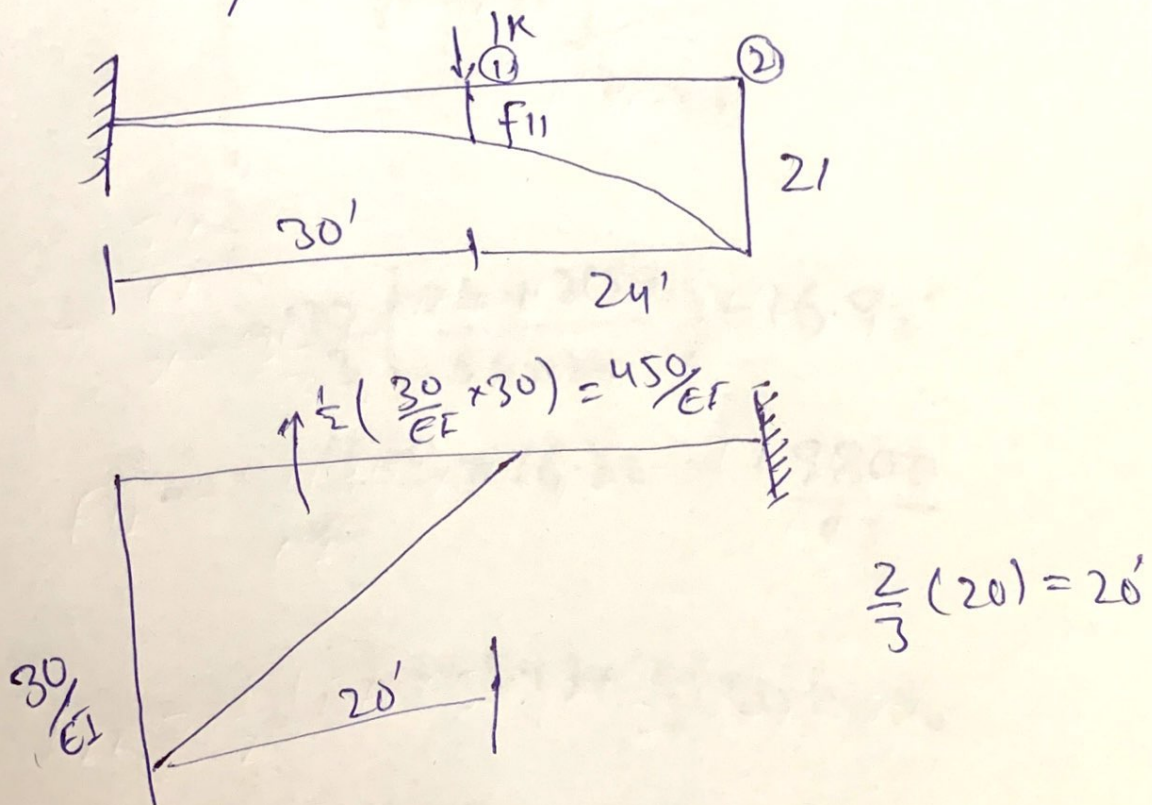
$$[DRL] = \frac{1}{EI} \begin{bmatrix} 48960 \\ 442860 \end{bmatrix}$$

Step # 03: Constant Flexibility Co-efficient matrix

$$F_{2 \times 2} = \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix}$$

a) Apply a unit value of AR_1 at reference point

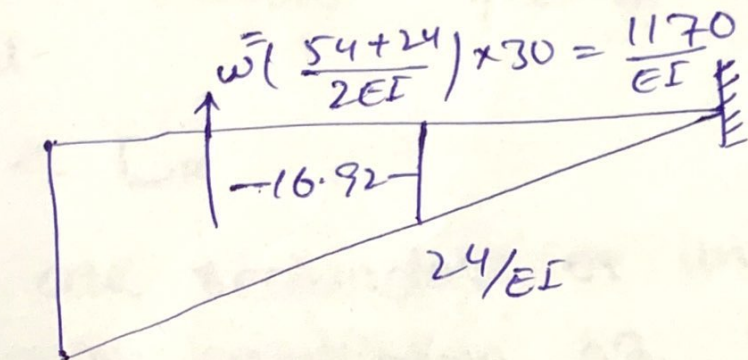
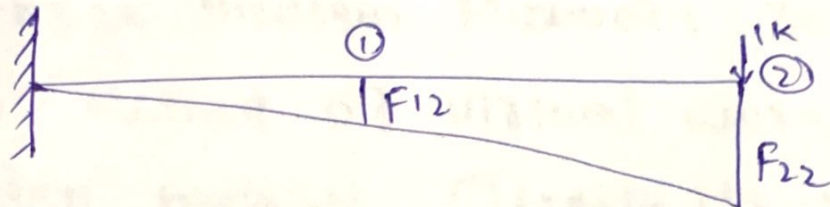
(i) Compute the value F_{11} & F_{21}



$$F_{11} = \frac{450}{EI} (20) = \frac{9000}{EI}$$

$$F_{21} = \frac{450}{EI} (20 \times 24) = \frac{19800}{EI}$$

(b) Apply a unit of AR_L at
 reference point ② (ii) Compute the value
 of F_{12} and F_{22}



$$\frac{54}{EI}$$

$$x = \frac{30}{3} \left[\frac{24 + 2(54)}{54 + 24} \right] = 16.92'$$

$$F_{12} = \frac{1170}{EI} \times 16.92 = \frac{19800}{EI}$$

$$F_{22} = \frac{1}{2} (54 \times 54) \times \frac{1}{3} (30) + 24$$

$$= \frac{49572}{EI}$$

QNO 28-

ANS:- Force Methods:- Strain energy Method
Castigliano's theorem Maxwell's reciprocal
theorem, Method of virtual work Consistent
deformation method - Flexibility matrix
method-

→ $D_S < D_R$

→ force are redundant or unknowns

→ Starts with equilibrium of force

→ forces found by compatibility eqns
of displacements

→ no of redundants = D_S

→ not suitable for = Computed

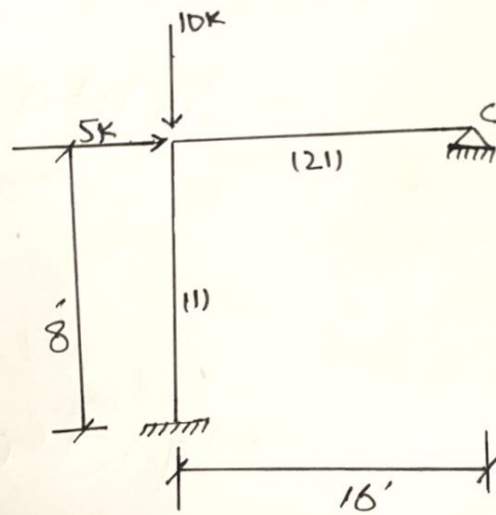
⇒ Displacement methods:- Moment
distribution method Slope deflection
method Kan's method, Stiffness
matrix method-

- $D_s > D_k$
- Displacements are redundant and unknown-
- Starts with Compatible deformation
- Displacements found by equilibrium equation of forces-
- no of redundants = D_k
- not suitable for Truss-

⇒ SUGGESTO

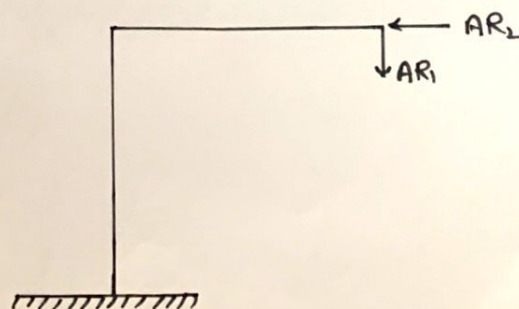
Displacement method is better and suitable because it is used globally and easy too-

QND3:- Analyze the rigid joint frame
 Shown in fig by flexibility
 Method Assume EI is constant
 for all members.



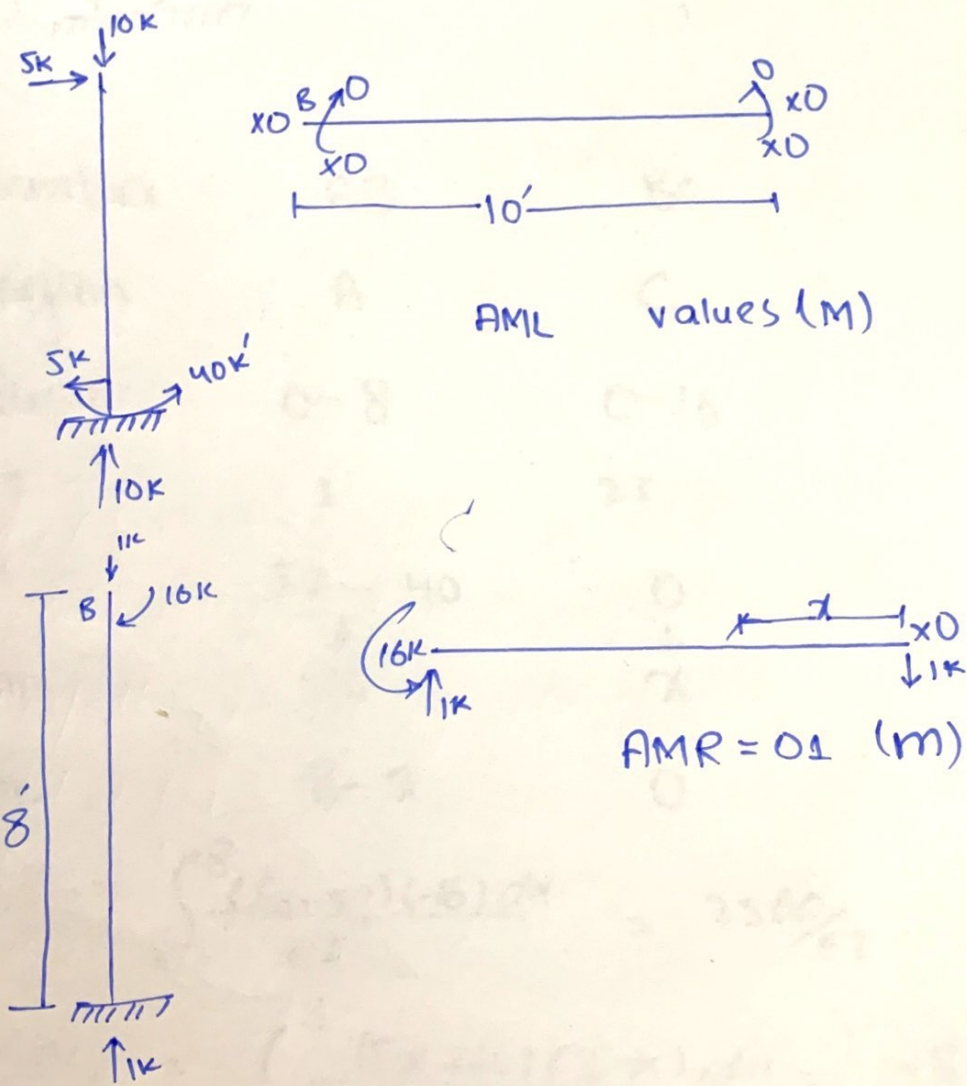
Solution:- $S.I = R - 3 \Rightarrow 5 - 3$
 $= 2$

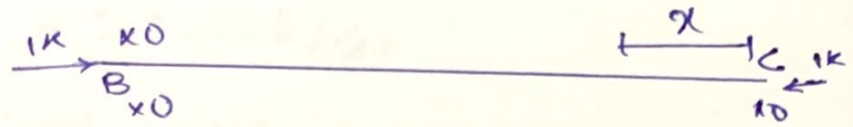
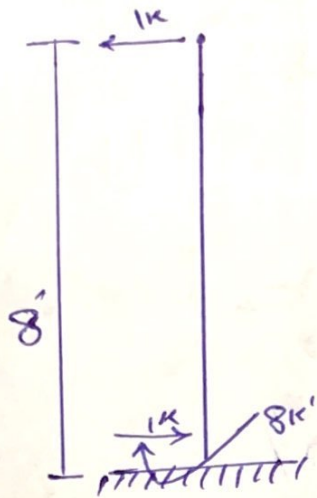
Step # 01:- identify the redundant
 Action.



$$\begin{bmatrix} DRS_1 \\ DRS_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix} \quad \begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} ? \\ ? \end{bmatrix}$$

Step#02:- Compute the value of DRL and f





AM_L(02)

Member	AB	BC
Origin	A	C
Limit	0-8	0-16
I	I	2I
M	$5x - 40$	0
m_1	\downarrow -16	\downarrow x
m_2	$8 - x$	0

$$DRL_1 = \int_0^8 \frac{(5x-40)(-16) dx}{EI} = \frac{2560}{EI}$$

$$DRL_2 = \int_0^8 \frac{(5x-40)(8-x) dx}{EI} = \frac{-853.33}{EI}$$

$$F_{11} = \int_0^8 \frac{(-16)^2 dx}{EI} + \int_0^{16} \frac{x^2}{2EI} dx$$

$$= 2730.67/EI$$

$$F_{12} = \int_0^8 \frac{-16(8-x)}{EI} dx = -512/EI$$

$$F_{22} = \int_0^8 \frac{(8-x)^2}{EI} dx = 170.67/EI$$

$$\begin{bmatrix} AR_1 \\ AR_2 \end{bmatrix} = \begin{bmatrix} F_{11} & F_{12} \\ F_{21} & F_{22} \end{bmatrix}^{-1} \times \begin{bmatrix} DRS_1 - DRL_1 \\ DRS_2 - DRL_2 \end{bmatrix}$$

$$= \begin{bmatrix} 2730.31 & -512 \\ -512 & 170.0 \end{bmatrix} \begin{bmatrix} 0 & -2560 \\ 0 & -853.33 \end{bmatrix}$$