

Name:

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GD #:

7911

Section:

A

Subject:

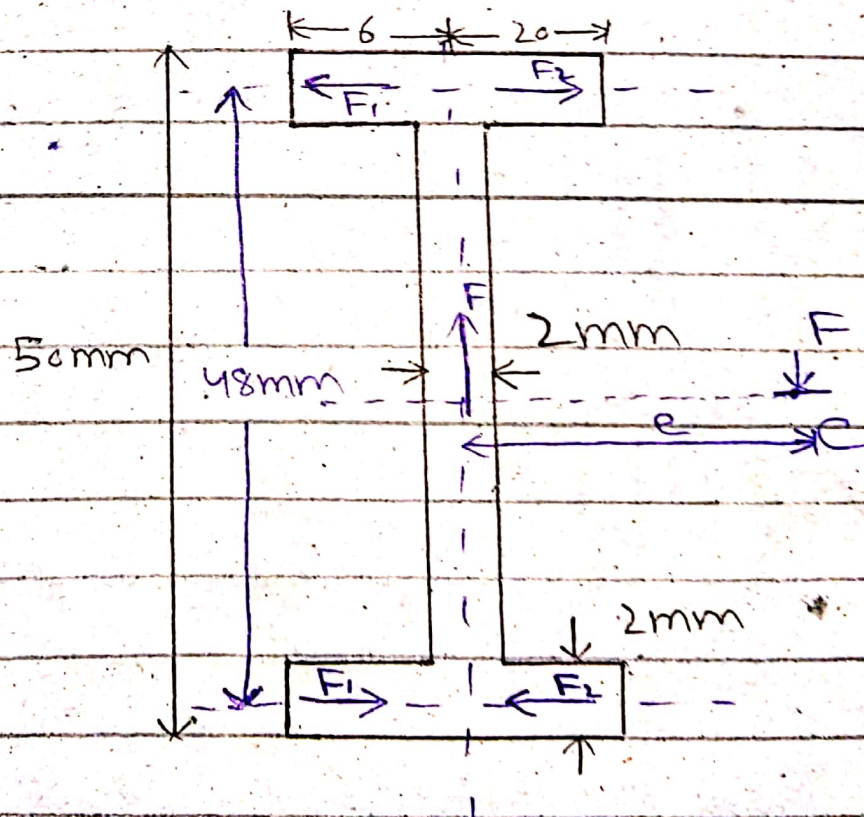
MOS (II)

Date:

23-6-2020

(1)

Q1 (a) Determine the location of shear centre for the beams having the cross-sectional dimensions shown in the figure 1. All members are to be considered thin walled and calculations should be based on the centreline dimensions.



Solution:

(2)

Solution:

As we know that

$$e = \frac{t_b h^2 b^2}{4I} \quad \text{--- (1)}$$

where

$h$  = height of section

$b$  = flange length

$t$  = thickness

Now moment of inertia is

$$I = 2 \left[ \frac{25(2)^3}{12} + (20 \times 2)(25)^2 \right] + \left[ \frac{2(50)^3}{12} \right]$$

$$I = 2 \left[ 500.66 + 20833 \right]$$

$$I = 70867.99 \text{ mm}^4$$

Now put values in eq (1)

$$e = \frac{2(50)^2(25)^2}{4(70867.99)} = 11.02 \text{ mm}$$

So shear centre  $e = 11.02 \text{ mm}$

## Answer No 1 (b)

Given:

$$H = 26 \text{ ft}$$

$$D = 22 \text{ ft}$$

$$\text{tangential stress} = 600 \text{ lb/ft}^3$$

$$\text{Specific weight of water tank} = 62.4 \text{ lb/ft}^3$$

$$\text{Thickness} = ?$$

Solution:

The pressure developed by water =  $P = \gamma h$

$$\sigma_r = \frac{PD}{2t}$$

$$\sigma_r = \frac{PD}{2t} = \frac{\gamma h D}{2t}$$

$$2t \times \sigma_r = \gamma h D$$

(4)

$$2t = \frac{\gamma h D}{G_T}$$

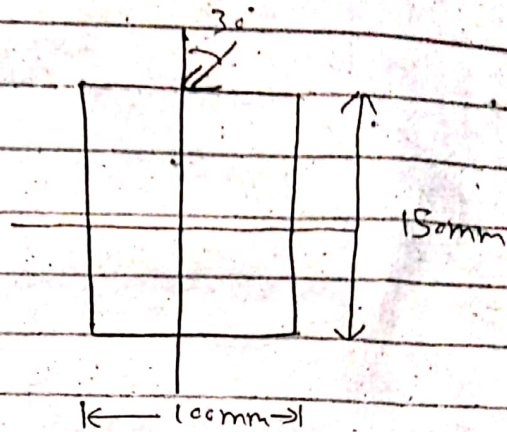
$$t = \frac{\gamma h D}{G_T \times 2}$$

$$t = \frac{(62.4) \times (26 \times 12) \times (22 \times 12)}{(12)^3 \times 6000 \times 2}$$

$$t = 0.24''$$

(5)

Answer 2 (a)



Moment of inertia

$$I_x = \frac{bh^3}{12} = \frac{0.1(0.15)^3}{12} = 2.8125 \times 10^{-5} \text{ m}^4$$

Now

$$I_y = \frac{bh^3}{12} = \frac{0.15(0.1)^3}{12} = 1.25 \times 10^{-5} \text{ m}^4$$

$$\sigma = \frac{M_z y}{I_z} + \frac{M_y z}{I_y}$$

$$\sigma = \frac{M \cos \theta}{I_z} + \frac{M \sin \theta}{I_y}$$

where

$$\begin{aligned} M &= M \cos \theta = P \cos \theta = M_z \\ &= 18 \text{ kNm} \end{aligned}$$

where

(6)

$$M = P \cos \theta = P \cos \theta = M_z$$

$$= 12 \cos 30^\circ = M_z$$

$$M_z = 1.8510 \text{ kN}$$

$$M \sin \theta = P \sin \theta = M_y$$

$$M_y = 12 \sin 30^\circ$$

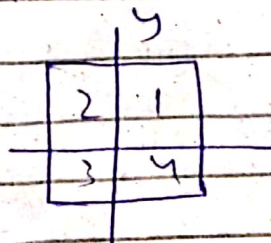
$$M_y = -11.8563 \text{ kN}$$

$$\sigma = \left( \frac{M_z}{I_z} \right) + \left( \frac{M_y}{I_y} \right)$$

$$\sigma = \frac{1.851}{2.812 \times 10^{-5}} + \frac{(-11.8563)}{1.25 \times 10^{-5}}$$

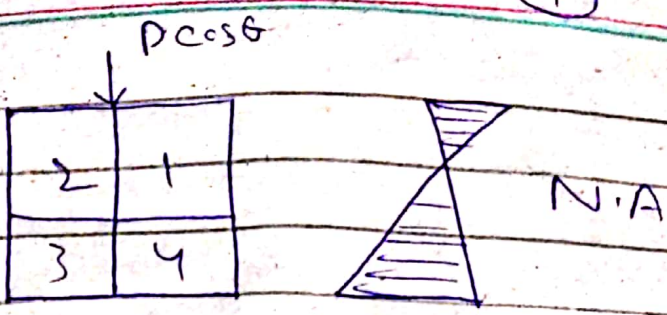
$$\sigma = -882678 \text{ Nm}^2$$

Sign Convention



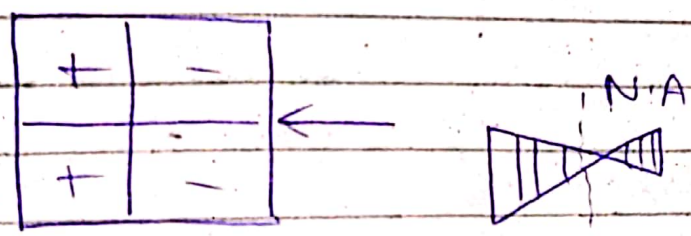
If we take compression as negative and tension as positive and the beam is simply supported

(7)



Quadrant 1, 2 (-ive)

Quadrant 3, 4 (+ive)



Quadrant 1, 4 (-ve)

Quadrant 2, 3 (+ive)

In case of unsymmetrical loading lies at an angle of " $\alpha$ " The principle axis and the algebraic sum of stress at N.A. is zero.

$$\sigma = \frac{M \cos \theta \cdot y}{I_z} + \frac{M \sin \theta \cdot z}{I_y} \quad \text{--- (1)}$$

In this case, neutral axis passes through 2, 4 So



(8)

$$\sigma = \frac{M \cos \theta}{I_z} y + \frac{M \sin \theta}{I_y} z$$

Let consider point A on neutral axis lies in quadrant 2 where

- Bending stress due to  $P \cos \theta$  is compressive
- Bending stress due to  $P \sin \theta$  is tensile

E.g. (i) becomes

$$\Rightarrow 0 = \frac{-M \cos \theta}{I_z} y_A + \frac{M \sin \theta}{I_y} z_A$$

$$\frac{y_A}{z_A} = \frac{I_z \sin \theta}{I_y \cos \theta}$$

$$\Rightarrow \tan \alpha = \frac{I_z \tan \theta}{I_y} \quad \text{--- (ii)}$$

Now putting values of  $I_z, I_y$  and  $\theta$  in e.g. (ii)

$$\tan \alpha = \frac{I_z \tan 30}{I_y}$$

(9)

$$\tan \alpha = \frac{2.8125 \times 10^{-5} (\tan 30^\circ)}{1.25 \times 10^{-5}}$$

$$\tan \alpha = -14.4129$$

$$\alpha = \tan^{-1}(-14.4129)$$

$$\alpha = 1.5^\circ$$

$$\alpha = 1^\circ 30' 5''$$

(10)

## Answer 2 (b)

Given:

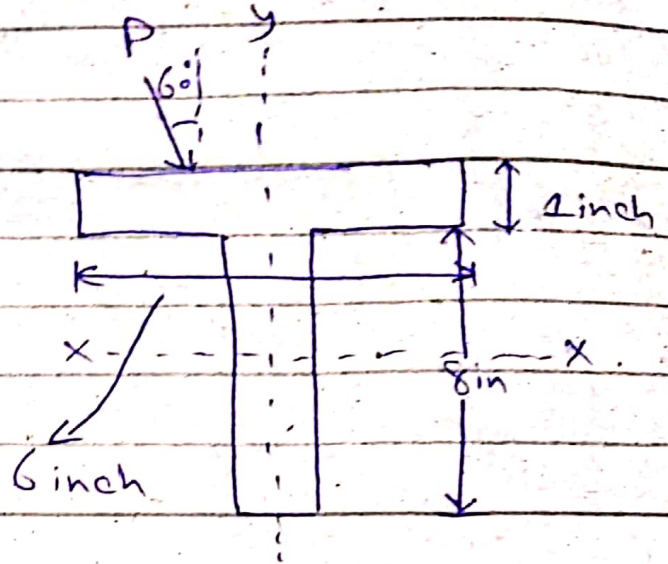
$$L = 16 \text{ ft}$$

$$I_x = 112.6 \text{ inch}^4$$

$$I_y = 18.7 \text{ inch}^4$$

$$\sigma_c = 12000 \text{ psi}$$

$$\sigma_t = 5000 \text{ psi}$$



Solution:

If we look at the figure we can judge maximum compression would that occur on an axial maximum tension C and at B. There will be tension as well as compression which will reduce that effect of each other. So we will calculate stress at A and C.

$$\sigma_A = \frac{M_x y}{I_x} + \frac{M_y x}{I_y} \text{ (Comp.)}$$

(17)

$$\delta_c = \frac{M_{xy}}{I_x} + \frac{M_{yx}}{I_y} \text{ (Tension)}$$

Now  $M_x$  and  $M_y$

$$M_x = \frac{P \cos 60^\circ (16 \times 12)}{4}$$

$$M_x = 48 P \cos 60^\circ$$

$$M_y = \frac{P \sin 60^\circ (16 \times 12)}{4}$$

$$M_y = 48 P \sin 60^\circ$$

Now

$$\delta_A = \frac{M_{xy}}{I_x} + \frac{M_{yx}}{I_y}$$

$$1200 = \frac{48 P \cos 60^\circ \times 3.07}{112.6} + \frac{48 P \sin 60^\circ \times 3}{18.7}$$

$$\Rightarrow P = 1638.6 \text{ lb}$$

(12)

Now

$$\sigma_e = \frac{M_{xy}}{I_x} + \frac{M_{yx}}{I_y}$$

$$S_{occ} = \frac{48 \rho \cos 60^\circ \times (5.93)}{112.6} + \frac{48 \rho \sin 60^\circ \times 5}{18.7}$$

$$P = 2104.9 \text{ lb}$$

Answer 3

Given:

$$\text{Length} = L = 10 \text{ ft}$$

Both sides are hinged so

$$L_e = L$$

$$E = 10.3 \times 10^6$$

Factor of safety = 2

$$b = 0.75 \text{ inch}$$

$$h = 2 \text{ inch}$$

(13)

Required:

Safe load = ?

Solution:

As

$$P_{cr} = \frac{\pi^2 EI}{L_e^2}$$

As we know that

$$I = Ay^2$$

$$y = \sqrt{\frac{I}{A}}$$

$$y = \frac{\sqrt{\frac{hb^3}{12}}}{bh} \Rightarrow \sqrt{\frac{b^2}{12}}$$

$$y = \frac{b}{2\sqrt{3}} \Rightarrow \frac{0.75}{2\sqrt{3}}$$

$$y = 0.216 \text{ inch}$$

(19)

$$P_{cr} = \frac{\pi^2 EA}{\left(\frac{L_e}{r}\right)^2}$$

$$P_{cr} = \frac{(3.14)^2 (10.3 \times 10^8) (1.5)}{\left(\frac{10}{0.216}\right)^2}$$

$$P_{cr} = 853.8343$$

Safe load =  $\frac{\text{crippling load}}{\text{factor of safety}}$

$$\text{Safe load} = \frac{853.8343}{2}$$

$$\text{Safe load} = 426.917$$

For fixed ended column

$$L_e = \frac{L}{2} = \frac{10}{2}$$

$$L_e = 5 \text{ ft}$$

$$P_{cr} = \frac{\pi^2 EA}{\left(\frac{L_e}{r}\right)^2} = \frac{(3.14)^2 \times (10.3 \times 10^8) (1.5)}{\left(\frac{10}{0.216}\right)^2}$$

(15)

$$P_{cr} = 1974.207$$

$$\text{Safe load} = \frac{P_{cr}}{\text{Factor of safety}}$$

$$= \frac{1974.207}{2}$$

$$\text{Safe load} = \boxed{987.103}$$