

Day: M T W T F S

Date: \_\_\_/\_\_\_/\_\_\_

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Section

NO # B

Paper

MDS EE

Date

26/09/2020

University

Iqra

National

University

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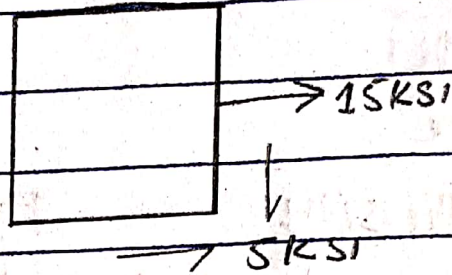
QNO (02) :

Given Data :

$$\sigma_x = 15 \text{ ksi}$$

$$\sigma_y = 0$$

$$\tau_{xy} = -5 \text{ ksi}$$



Required Data :

- Principal stress
- Max-plan shear stress
- average normal stress

Solution :

a- principal stress :

$$\sigma_{1,2} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\sigma_{1,2} = \frac{15 + 0}{2} \pm \sqrt{\left(\frac{15 - 0}{2}\right)^2 + (-5)^2}$$

$$\sigma_{1,2} = 7.5 \pm 9.01$$

$$\Rightarrow \sigma_1 = 16.51 \text{ ksi}$$

$$\sigma_2 = 7.5 - 9.01$$

$$\sigma_2 = -1.51 \text{ KSI.}$$

Now we find orientation  
we know that.

$$2\theta_2 = \frac{\tau_{xy}}{(\sigma_x - \sigma_y) / 2}$$

$$2\theta_2 = \frac{-5}{(15 - 0) / 2}$$

$$\theta_2 = -0.33$$

Now we check which  
angles goes with which  
principal stress.  
we know that:

$$\sigma_{x_1} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$= \frac{15 + 0}{2} + \frac{15 - 0}{2} \cos 2(-0.33) + (-5) \sin 2(-0.33)$$

$$= \frac{15}{2} + \frac{15}{2} (0.99) + (-5) (-0.12)$$

$$= 14.925 + 0.6$$

$$= 15.525$$

b- Max-Plan Shear Stress:  $\Rightarrow$

$$\tau_{max} = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\Rightarrow \tau_{max} = \sqrt{\left(\frac{15-0}{2}\right)^2 + (-5)^2}$$

$$\tau_{max} = 9.01 \text{ ksi}$$

Checked By:.....Parents:.....Excellent  Good

Now we find orientation.  
we know that.

$$\tan 2\theta = \frac{-(\sigma_x - \sigma_y) / 2}{\tau_{xy}}$$

$$= \frac{(15 - 0) / 2}{-5}$$

$$\tan 2\theta = +1.5.$$

$$2\theta = \tan^{-1}(+1.5).$$

$$2\theta = 56$$

$$\theta = \frac{56}{2}$$

$$\theta = 28.$$

We know that

$$\tau_{x'y'} = \frac{-\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta.$$

$$= \frac{-15 - 0}{2} \sin 2(28) + (+5) \cos 2(28).$$

$$= -7.5 (0.82) - 2.8$$

$$= -8.95$$

Ex: NO: 1 Part b

$$\sigma_x = 15 \text{ ksi}$$

$$\tau_{xy} = -5 \text{ ksi}$$

$$\sigma_y = 0$$

$$c = \frac{\sigma_x + \sigma_y}{2} = \frac{15 + 0}{2}$$

$$c = 7.5 \text{ ksi}$$

$$R = \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$R = \sqrt{\left(\frac{15 - 0}{2}\right)^2 + (-5)^2}$$

$$R = 9.01$$

Scale  $\Rightarrow$

$$1 \text{ small box} = 0.5 \text{ ksi}$$

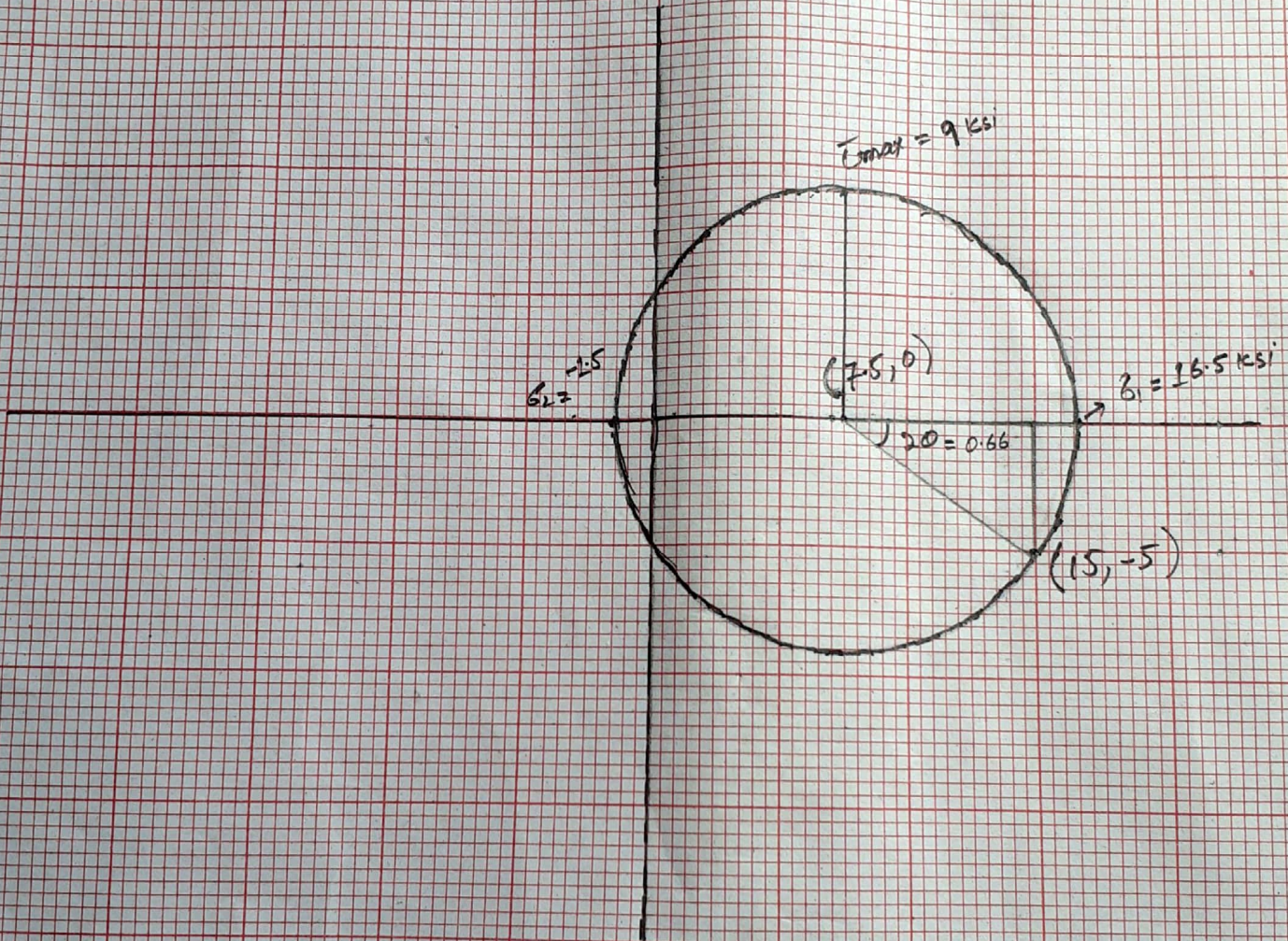
$$\sigma_x = 15 \text{ ksi}$$

$$\tau_{xy} = -5 \text{ ksi}$$

$$\sigma_y = 0$$

$$c = \frac{\sigma_x + \sigma_y}{2}$$

$$c =$$



Q: NO: 02:→

Given (Data)→

$$\sigma_1 = 32 \text{ MPa}$$

$$\sigma_2 = 16 \text{ MPa}$$

Required (Data)→

Absolute Maximum Shear stress:

Solution:→

The principal stresses are

$$\sigma_1 = 32 \text{ MPa}$$

$$\sigma_2 = 16 \text{ MPa}$$

If  $\sigma_1$  &  $\sigma_2$  are plotted along  $\sigma$  axis, the Mohar circles are obtained.

The large circle has radius of 16 MPa. & have center of 16 MPa.

The small circle has both have radius of 8 MPa &

1<sup>st</sup> small has center of 8 &  
2<sup>nd</sup> one have center of 24 on  $\sigma$  axis.



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An orientation of  $45^\circ$ , in  
Plane, show that as shown in graph.

$$\tau_{\text{abs-max}} = 16 \text{ MPa}$$

$$\sigma_{\text{ave}} = 16 \text{ MPa}$$

{ check :- }

$$\tau_{\text{abs-max}} = \frac{\sigma_1}{2}$$

$$\tau_{\text{abs-max}} = \frac{32}{2} = 16 \text{ MPa}$$

$$\sigma_{\text{ave}} = \frac{\sigma_x + \sigma_y}{2}$$

$$\sigma_{\text{ave}} = \frac{32 + 0}{2} = 16 \text{ MPa}$$

By comparison, the maximum  
in plan shear stress can be  
determined from the Mohr's  
circle shown in graph.

$$\tau_{\max-\text{in plane}} = 8 \text{ mpa}$$

$$\sigma_{\text{ave}} = 24 \text{ mpa.}$$

Check  $\Rightarrow$

$$\tau_{\max-\text{in plane}} = \frac{\sigma_1 - \sigma_2}{2}$$

$$= \frac{32 - 16}{2}$$

$$\Rightarrow 8 \text{ mpa}$$

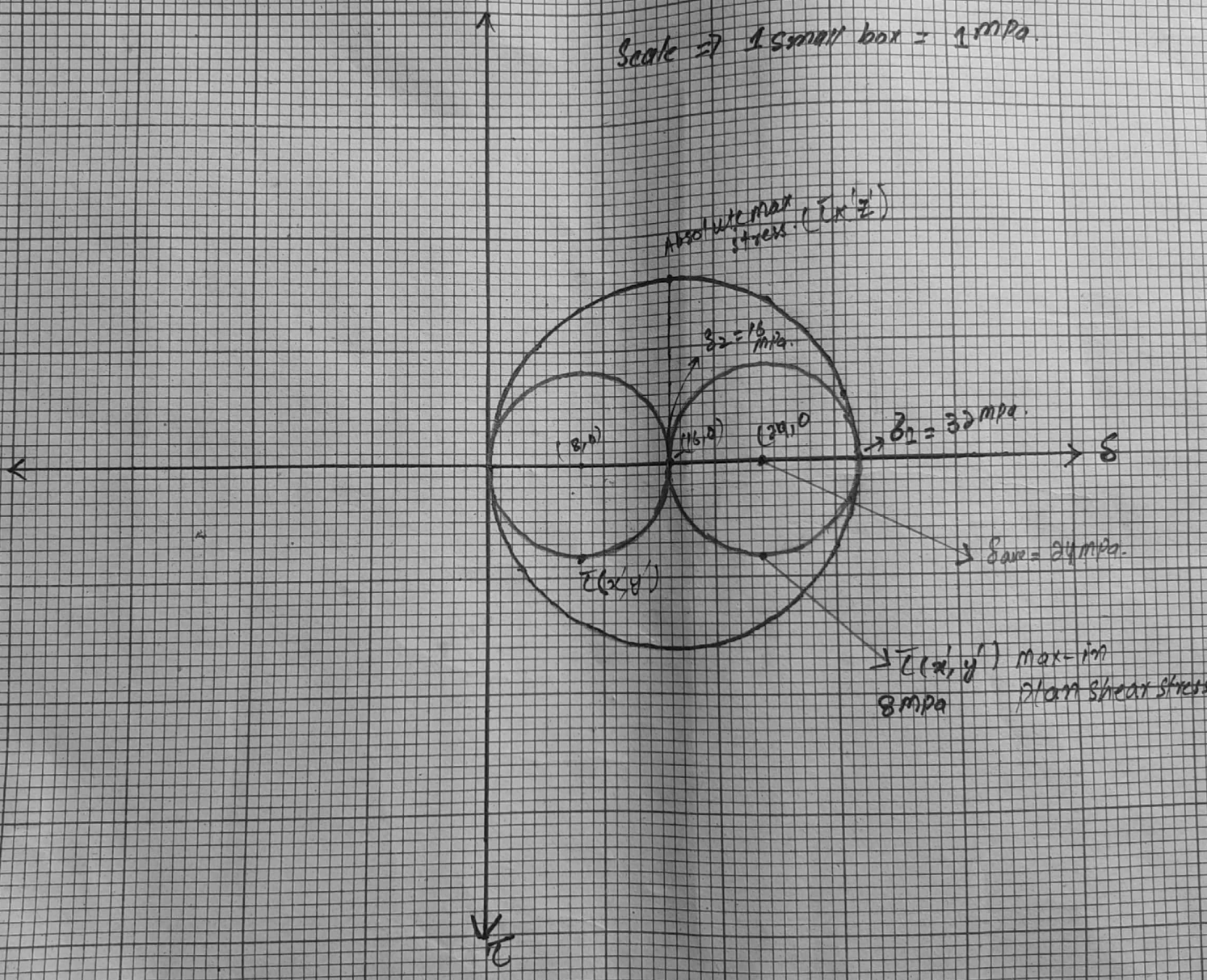
$$\sigma_{\text{avg}} = \frac{\sigma_1 + \sigma_2}{2}$$

$$\sigma_{\text{avg}} = \frac{32 + 16}{2}$$

$$\sigma_{\text{avg}} = 24 \text{ mpa.}$$

Scale  $\Rightarrow$  1 small box  $\Rightarrow$  1 MPa

Scale  $\Rightarrow$  1 small box = 1 MPa



Q No (03) :- (03)

Stresses Responsible For  
~~Parts~~ Failure of Ductile  
 and Brittle Materials.

There are two main  
 Stresses

- (1) Tensile Stresses
- (2) Shear Stresses.

Ductile Materials  $\rightarrow$  failures occurs due  
 to shear stresses. When  
 shear stresses exceed  
 the shear strength of  
 ductile materials.

Brittle Material failure  
 occurs due to tensile  
 strength. When tensile  
 stresses exceed the  
 strength of Brittle  
 materials.

Two Failure theories For  
Ductile Material.

(1) Maximum Shear Stress Theory.

(2) Maximum Distortion Energy Theory.

Two Failure theories For  
Brittle Materials.

(1) Maximum Normal Stress Theory.

(2) Mohr's Failure Criterion.

Failure Theory for  
concrete.

As a concrete is a brittle material, the fracture of brittle material is due to the maximum tensile stresses. If a brittle

material has a stress-strain diagram that is different in tension and compression than Mohr's failure criterion may be used to predict failure.

④ if the stress-strain diagram is similar in tension and compression then we used maximum normal stress theory.

⑤ Due to material property of tensile fracture of brittle material is difficult to predict, so theory of brittle failure for brittle material should be used with lot of care.

① Steel is ductile material and due to maximum shear stress the steel bend which may cause the breaking of steel. Therefore maximum Distortion theory are applicable to ductile material such as steel.