

M. Abdullah Khan

Section B

7758

Submitted to: Engr. Adeed Khan

Hydraulic Structures

Assignment 1

Ans "Stage discharge relationship for a contracted rectangular box weir?"

Given Data:

Width = 1.4m

Height = 0.9m

Length = 26m

Slope = 1:1000

Manning's $n = 0.013$

Square edged entrance, $K_e = 0.5$

Range = 0-3m

Solution

$H/D \leq 1.4m$

$H \leq 0.9m$

Discharge is given by,

$$Q = 2.92 Y_0 \left[1.2 Y_0 / 1.2 + 2 Y_0 \right]^{2/3} A$$

Y_0 (m)	Q (m^3/s)	Y_c (m)
0.3	0.299	0.166
0.6	0.785	0.317
0.9	1.330	0.451

By putting values of " Y_0 " we will get the corresponding discharge.

$$\bullet Q_1 = 2.92(0.3) \left[\frac{1.2(0.3)}{1.2 + 2(0.3)} \right]^{2/3}$$

$$= 0.299 \text{ m}^3/\text{s}$$

$$\bullet Q_2 = 2.92(0.6) \left[\frac{1.2(0.6)}{1.2 + 2(0.6)} \right]^{2/3}$$

$$= 0.785 \text{ m}^3/\text{s}$$

$$\bullet Q_3 = 2.92(0.9) \left[\frac{1.2(0.9)}{1.2 + 2(0.9)} \right]^{2/3}$$

$$= 1.330 \text{ m}^3/\text{s}$$

"Critical depth"

Q. (3)

$$x_c = \left(\frac{q^2}{g} \right)^{1/3} \quad \text{--- } \overset{A}{B}$$

$$q = \frac{Q}{B}$$

By putting values in eq B°

$$q_1 = \frac{Q_1}{B} = \frac{0.299}{1.4} = 0.213$$

$$q_2 = \frac{Q_2}{B} = \frac{0.785}{1.4} = 0.561$$

$$q_3 = \frac{Q_3}{B} = \frac{1.336}{1.4} = 0.95$$

Now by putting values in eq A°

$$x_{c1} = \left(\frac{q_1^2}{g} \right)^{1/3} = \left(\frac{(0.213)^2}{9.81} \right)^{1/3} = 0.166m$$

$$x_{c2} = \left(\frac{q_2^2}{g} \right)^{1/3} = \left(\frac{(0.561)^2}{9.81} \right)^{1/3} = 0.317m$$

$$x_{c3} = \left(\frac{q_3^2}{g} \right)^{1/3} = \left(\frac{(0.95)^2}{9.81} \right)^{1/3} = 0.451$$

At the inlet every a short reach

$$H = Y_0 + \frac{V^2}{2g} + K_2 \cdot \frac{V^2}{2g}$$

$$V_1 = 1.1428 \text{ m/s}$$

So,

$$H_1 = Y_{01} + \frac{V^2}{2g} + K_e \frac{V^2}{2g}$$

$$= 0.3 + \frac{(1.142)^2}{2(9.81)} + 0.5 \left(\frac{(1.142)^2}{2(9.81)} \right)$$

$$= \boxed{0.399 \text{ m}}$$

$$H_2 = 0.06 + \frac{(1.142)^2}{2(9.81)} + 0.5 \left(\frac{(1.142)^2}{2(9.81)} \right)$$

$$= \boxed{0.699 \text{ m}}$$

$$H_3 = 0.9 + \frac{(1.142)^2}{2(9.81)} + 0.5 \left(\frac{(1.142)^2}{2(9.81)} \right)$$

$$= \boxed{0.999 \text{ m}}$$

X_0 (m)	H (m)	Q (m^3/s)
0.03	0.399	0.288
0.6	0.699	0.785
0.9	0.999	1.330
orifice 1.2 D"	1.08 →	1.477 by interpolation

2" $H/D \geq 1.4$

"a", for orifice flow,

$$Q = cd (1.4 \times 0.9) [(2g(H - D/2))]^{1/2}$$

$$Q = 0.62 (1.4 \times 0.9) [(2(9.81)(1.08 - \frac{0.9}{2}))^{1/2}]$$

$$Q = 2.746 \text{ m}^3/\text{s}$$

The following result are obtained

H(m)	Q (m^3/s)	X (m)
1.08	2.746	20.9

no cavitation
flow exists

"B" For Pipe Flow the energy equation gives,

$$H + S_0L = D + H_c$$

where e_{eff}

$$h_f = K_e \frac{V^2}{2g} + (V_n)^2 \frac{L}{R^{4/3}} + \frac{V^2}{2g}$$

Thus =

$$Q = 2.08 (H - 0.57)^{1/2}$$

During rising stages the barrel flows full from $H = 1.08$ m and during falling stages the flow becomes free-surface flow when $H = 0.999$ m.

The following table summarizes the result?

H(m)	Q (m ³ /s)	Types of flow
Rising stages		
0.399	0.299	open channel
0.699	0.785	open channel
0.999	1.330	open channel
1.080	1.477	Pipe flow
2.000	2.487	Pipe flow
3.000	3.242	Pipe flow
Falling stages		
2.000	2.487	Pipe flow
1.080	1.477	pipe flow
0.999	1.330	pipe flow
0.699	0.785	open channel
0.399	0.299	open channel

LOADS ON BRIDGE FOUNDATION DUE SCORING:-

Maximum amount of load to cause failure in foundation. The failure can not be expected due to inadequate bearing capacity but by scoring and leading of mortar joints of wall foundation. The increased moments due to MBCG leading would create more bending shear in the string especially in the lap and setting in the junction. In the event of failure of wall foundation the wall is made of stone masonry would be joint in bending.

MECHANISM AND WORKING

A significant amount of work has been conducted on bridge span. Such thought can be classified into two major categories:

- (1) Science
- (2) Engineering

Engineering Mechanism:-

The engineering mechanism of bridge foundation is based on its construction technology.

The 6 No of bars are driven to the well and cemented to the well cap and pier by doveled bars would the become flush some have opined that even in the event of failure of well the dumb bars amount to well cap upto height of 1.70m above the well top would give rise to a lot of friction and prevent the pier from lateral friction would generate when there is normal reaction perpendicular to the moment of pier.