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Section B

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Subject PRCD-I

Submitted To,

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Q.1 Given Data :-

- ⊙ Live Load (L.L) = 2.47 Kips/ft
- ⊙ Dead load (D.L) = 1.05 Kips/ft
- ⊙ width of Beam (b) = 10 inch
- ⊙ Height of Beam (h) = 20 inch
- ⊙ Span of Beam (L) = 18 ft
- ⊙  $f_y = 60,000 \text{ psi} = 60 \text{ Ksi}$
- ⊙  $f'_c = 4000 \text{ psi} = 4 \text{ Ksi}$

Solution :-

⊙ Effective depth :-

$$d = h - 3$$

$$d = 20 - 3$$

$$d = 17''$$

⊙ Effective Cover ( $d'$ )  
Suppose  $d' = 2.5''$

Step ①

Reinforcement Ratio

$$f_{max} = 0.85 * \beta * \frac{f'_c}{f_y} * \left( \frac{E_u}{E_u + E_f} \right)$$

$$f_{max} = 0.85 * 0.85 * \frac{4}{60} * \left( \frac{0.003}{0.003 + 0.005} \right)$$

$$f_{max} = 0.0181$$

No unit b/c  
it is Ratio  
blw Same unit

Step ② :-

Calculate Area of Steel  
We know that,

$$f_{max} = \frac{A_{st}}{b \times d}$$

now

$$A_{st} = f_{max} (bd)$$

$$A_{st} = 0.0181 \times (10 \times 17)$$

$$A_{st} = 3.077 \text{ in}^2$$

Step ③ :-

Design Factored Moment

According to Formula

$$M_{u2} = \phi \times A_{st} \times f_y \times \left(d - \frac{a}{2}\right)$$

First we find  $a = ?$ 

As

$$a = \frac{A_{st} \times f_y}{0.85 \times f'_c \times b}$$

$$a = \frac{3.08 \times 60}{0.85 \times 4 \times 10} = 5.4''$$

now

$$M_{u2} = 0.90 \times 3.077 \times 60 \times \left(17 - \frac{5.4}{2}\right)$$

$$M_{u2} = \del{2368.98} 2368.98 \text{ K''}$$

$$M_{u2} = 2368.98 \text{ K''}$$

Now Moment due to given load:-

$$\begin{aligned} \text{Beam Self weight} &= b \times t \times \rho_c \\ &= \frac{10}{12} \times \frac{20}{12} \times 150 \\ &= 208.33 \text{ lb/ft} \end{aligned}$$

Total Factored load:-

$$\begin{aligned} W_T &= 1.2 \times D.L + 1.6 \times L.L \\ &= 1.2 \times (1050 + 208.33) + 1.6 \times (2470) \\ &= 5461.996 \text{ lb/ft} \end{aligned}$$

$$\text{or } W_T = 5.46 \text{ Kips/ft}$$

Ultimate Factored Moment:-

$$M_u = \frac{W \times L^2}{8} \times 12 \text{ b/c } L = 18''$$

$$M_u = \frac{5.46 \times (18)^2}{8} \times 12$$

$$M_u = 2653.56 \text{ K''}$$

Here

$$M_u > M_{u2}$$

$$M_u = 2653.56 > M_{u2} = 2368.98$$

So we provided extra steel in compression zone & thus it should be Doubly Reinforcement Design

Step 4 :-

$$M_{u1} = M_u - M_{u2}$$

$$M_{u1} = 2653.56 - 2368.99$$

$$M_{u1} = 284.57 \text{ kip-inch}$$

For this extra moment we provided extra steel in compression zone.

Step 5 :-

$$A'_s = \frac{M_{u1}}{\phi * f_y * (d - d')}$$

$$A'_s = \frac{284.57}{0.90 * 60 * (17 - 2.5)}$$

$A'_s = 0.36 \text{ in}^2$  thus  
Steel area for compression

Step 6 :- Total steel area  
in tensile

$$A_{s0} = A_{st} + A'_s$$

$$A_s = 3.07 + 0.36$$

$$A_s = 3.43 \text{ in}^2$$

This steel area provided  
in tensile zone.

Step 7 :-

Selection of Bars :-

(A) For Tensile Steel :-

Let we try #8 bar  
we know

Area of one #8 =  $0.785 \text{ in}^2 = A_b$   
Now

$$\text{Number of Bars} = \frac{A_s}{A_b}$$

$$\text{Number of Bars} = \frac{3.43}{0.785}$$

$$\text{Number of Bars} = 4.369 \approx 5$$

So we provided 5 #8 bars  
in tensile zone.

(B) For Compression Steel :-

Let we try #6 bar

Area of one #6 bar =  $0.44 \text{ in}^2$

$$\text{Number of Bars} = \frac{A_s}{A_b}$$

$$= \frac{0.36}{0.44}$$

$$\text{Number of bars} = 0.8181 \approx 1$$

So we provided 1 #6 in  
Compression zone.

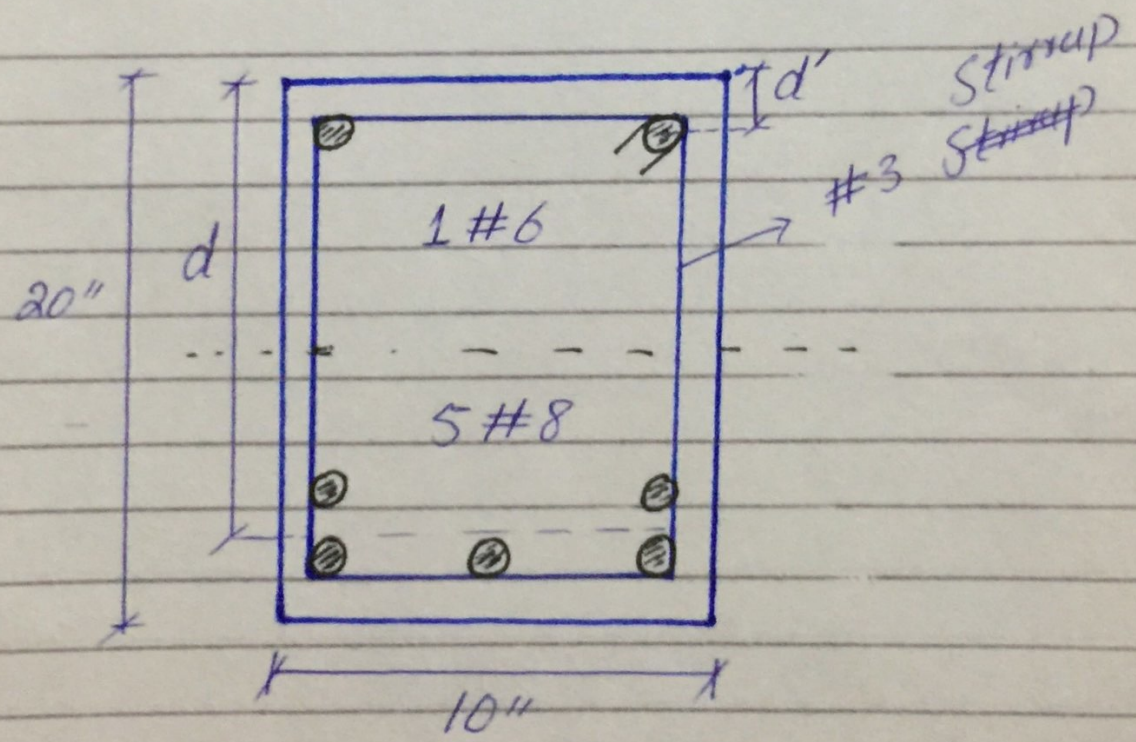
Step 8 :-

"Beam Minimum Width"

$$b_{min} = 2(1.5) + 2\left(\frac{3}{8}\right) + 5\left(\frac{8}{8}\right) + 4\left(\frac{8}{8}\right)$$

$$b_{min} = 12.75'' > 10''$$

Not good on one layer  
to provide main bar  
Thus it should be provided  
into two layer.



⊙ effective depth =  $d = 16.62''$

⊙ effective cover  $d' = 2.25''$

Step 9 :-

"Final Step Design moment"

According TO Formula

$$M_d = \phi \left[ A_s' f_y (d - d') + (A_{st} - A_s') \times f_y \left( d - \frac{a}{2} \right) \right] \quad (*)$$

$$a = ?$$

$$a = \frac{(A_{st} - A_s') \times f_y}{0.85 \times f_c' \times b}$$

$$a = \frac{(5 \times 0.785 - 1 \times 0.44) \times 60}{0.85 \times 4 \times 10}$$

$$a = 6.15 \text{ in}$$

Now put values in eq (\*)

$$M_d = 0.90 \left[ 1 \times 0.44 \times 60 (16.62 - 2.25) + (5 \times 0.785 - 1 \times 0.44) \times 60 \right.$$

$$\left. \times \left( 16.62 - \frac{6.15}{2} \right) \right]$$

Solve it we get;

$$M_d = 2890.42 > 2653.56$$

Thus the Design is Okay

1/4



Q.2

(a)

Bond Stress :-

These stress which is acting on the outer inter face of the steel to the surrounding concrete is known as bond stress.

⊙ The resulting stress of bond is called bond stress.

⊙ These stresses help in keeping bond b/w reinforced and concrete.

⊙ Due to the Bond stress result any force that tries to pull out the rods from the concrete.

⊙ When we try to pull out the reinforcement bar from hardened concrete then bond stress resists the bar to come out.

## Development Length :- (L<sub>d</sub>)

It can be define as;

The length of steel bar needed to be embedded into the column to establish the desired bond strength b/w concrete and steel is called development length.

© It hold two concrete members together such as; Beam, Column, Footing etc

## Reason For Providing Development length :-

© To creates a safe bond b/w Bar surface and concrete.

© Reinforcement bars should not slip through the concrete.

© To transfer stresses or load from beam to column smoothly.

What happen if we dont provide Development length :-

⊙ If we dont provide or less provide development length then the structure will Occure Slipage of Joints in such a case the bars will not break first but the failure will happen First on joint and then the Reinforcement bar will split from concrete.

Formula For Development length :-

$$L_d = \frac{\phi \sigma_s}{4 \tau_{bd}}$$

- ⊙  $L_d$  = Development length
- ⊙  $\phi$  = Nominal dia of Reinf.
- ⊙  $\sigma_s$  = Stress in bar at Section considered at design load.
- ⊙  $\tau$  = Design bond Stress.

(b)

We provided Doubly reinforced beam due to following Reason.

- ⊙ When depth are Restrictions.
- ⊙ In Continuous Beam Flood System.
- ⊙ Where it is Required to increase Stiffness of the beam.
- ⊙ Compression steel increase the ductility and structure with High ductility Respond better to Seismic Forces.
- ⊙ When the Restrictions Occure in the Size (cross-<sup>Section</sup>) of beam.

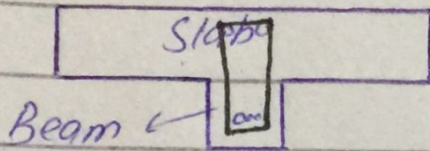
For Example :-

If the depth of beam should not be greater than 20" and the external load on beam is very much in which can not resist a singly reinf. Such a condition we provided Doubly Reinforced beam.

(C)

## T-Beam

⊙ Shape of T-Beam look like as;



⊙ Slab and Beam are monolithically connected.

⊙ It is used mostly in heavy duty

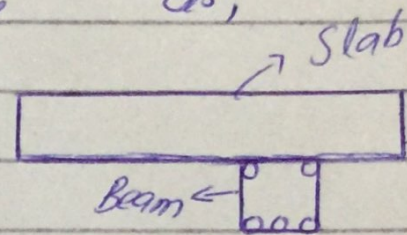
⊙ It act as a single member.

⊙ Here Reinforced <sup>Beam</sup> emerged in Slab

⊙ It is more economical than Rectangular Beam

## Rectangular Beam

⊙ Shape of Rectangular beam look like as;



⊙ No joint between Slab and Beam

⊙ It is used in Commercial building.

⊙ Here beam support the Slab

⊙ Here Reinforced <sup>Beam</sup> not emerged in Slab.

⊙ It is less economical than T-Beam.

(d)

Effect of Strength Reduction factor on flexural strength:-

If we design flexural strength. The strength reduction factor decrease from tension Control Section to Compression Controlled Section to increase safety with decreasing ductility. This show to determine the reduction factor Flexural strength of reinforcement concrete.

(e)

### Design Methods:-

Mostly there are two method used for Designing different Structure.

- (1) Allowable Stress Design (ASD) method.
- (2) Ultimate Stress Design Method (USD)

#### (1) ASD Method :-

⊙ It is also known as working stress design method.

⊙ It is based on the principle that stresses developed in the structural member should not exceed a certain limit Friction of elastic limit.

⊙ In this type method all load are taken as a service load.

⊙ No Factor is applied to increase those service load.

⊙ To evaluate Forces and Stresses using linear material.

⊙ In this method allowable material stress must be greater than maximum material stress which caused by load.

## (2) USD Method :-

⊙ USD method also know as Load factor method.

⊙ When a structure subjected to large external load the ultimate strength is determine by the elastic analysis.

⊙ It is Apply ultimate factored load.

⊙ Evaluate Sectional demand using linear or yielded materials.

⇒ ⊙ "USD is better due to Following ~~Atto~~ Reason"

⊙ As the ultimate strength of materials is to be considered we will get mach stander as compare to "ASD" method.

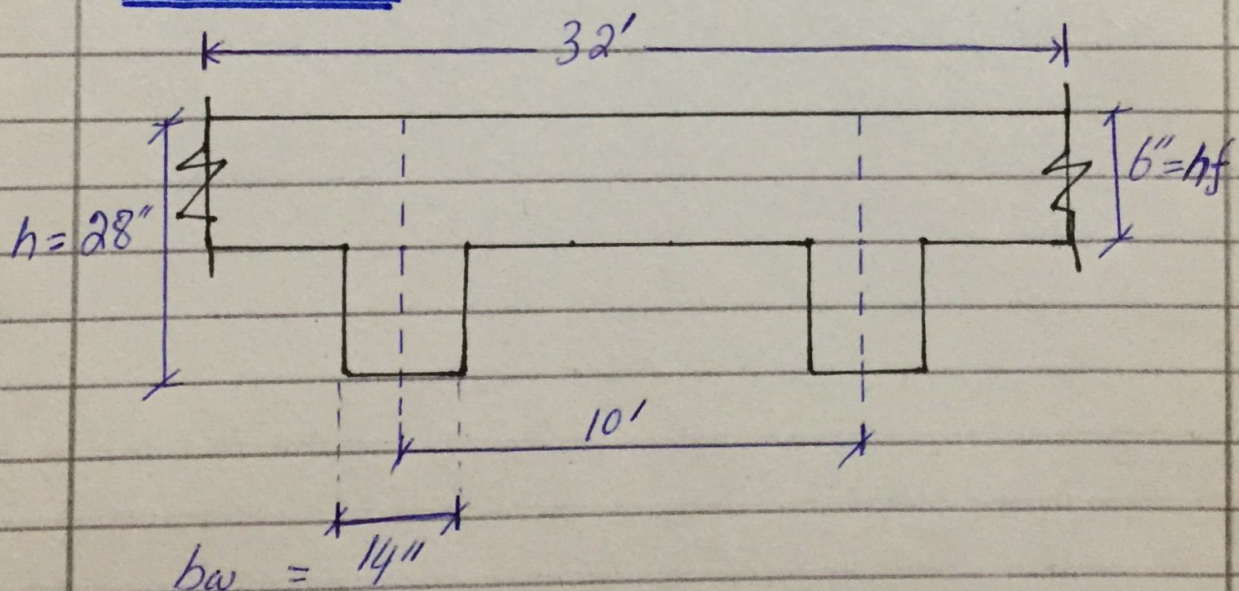
⊙ It is more economical design for a building with fewer special need for customized area and requirement.

⊙ "These design method Utilizes a more realistic Factor of Safety."



Q.3 Given Data :-

- ⊙ Span of Beam ( $L$ ) = 32'
- ⊙ C/c distance = 10'
- ⊙ Thickness of Slab ( $h_f$ ) = 6"
- ⊙ width of web ( $b_w$ ) = 14"
- ⊙ Total depth ( $h$ ) = 28"
- ⊙ effective depth ( $d$ ) =  $h - 3 = 28 - 3$   
 $d = 25"$
- ⊙ Dead load (D.L) = 50 lb/ft<sup>2</sup>
- ⊙ Live load (L.L) = 225 lb/ft<sup>2</sup>
- ⊙  $f_y = 60,000 \text{ psi} = 60 \text{ ksi}$
- ⊙  $f'_c = 4000 \text{ psi} = 4 \text{ ksi}$

Solution :-Step ① :-

Ultimate Factored moment

$$M_u = \frac{wL^2}{8}$$

i - Find Self weight per feet :-

$$wt = b \times t \times \rho_c$$

$$wt = \frac{14}{12} \times \frac{28}{12} \times 150$$

$$wt = 408.33 \text{ lb/ft} \quad \therefore \rho_c \text{ RCL} = 150 \text{ lb/ft}$$

ii - Find Total Factored Load :-

$$wt = 1.2 \times D \cdot L + 1.6 \times L \cdot L$$

$$wt = 1.2(50 + 408.33) + 1.6(225)$$

$$wt = 0.909 \text{ Kips/ft}$$

AS Moment :-

$$M_u = \frac{0.909(32) \times 12}{8}$$

$$M_u = 1396.22 \text{ Kips/ft}$$

Step (2) :-

Find effective width "b<sub>e</sub>"

$$(1) 16 \times h_f + b_w = 16 \times 6 + 14 = 110''$$

$$(2) \text{ c/c distance} = 10 \times 12 = 120''$$

$$(3) \text{ Span/4} = \frac{32}{4} \times 12 = 96''$$

Here 96'' is smallest value

So

$$b_e = 96''$$

Step ③ :-

To checked whether Rectangular or T-Beam Analysis is needed.

Trail # 01 :-

$$\text{let } a = hf = 6''$$

$$A_{st} = \frac{M_u}{\phi * f_y * (d - \frac{a}{2})}$$

$$A_{st} = \frac{1396.22}{0.90 * 60 * (25 - \frac{6}{2})}$$

$$A_{st} = 1.175 \text{ in}^2 \text{ --- (i)}$$

Trail # 02 :-

$$a = \frac{A_s * f_y}{0.85 * f'_c * b_e}$$

$$a = \frac{1.175 * 60}{0.85 * 4 * 96}$$

$$a = 0.21'' < 6''$$

"Thus Rectangular Beam Design"

$$A_{st} = \frac{1396.22}{0.90 * 60 * (25 - \frac{0.21}{2})}$$

$$A_{st} = 1.03 \text{ in}^2 \text{ --- (ii)}$$

Trial #03 :-

$$a = \frac{A_s \times f_y}{0.85 \times f'_c \times b_e}$$

$$a = \frac{1.03 \times 60}{0.85 \times 4 \times 96} = 0.18''$$

Now

$$A_{st} = \frac{1396.22}{0.90 \times 60 \left(25 - \frac{0.18}{2}\right)}$$

$$A_{st} = 1.03 \text{ in}^2 \text{ --- (iii)}$$

$$ev \text{ (ii)} = ev \text{ (iii)}$$

Step 4 :-Checked  $f_{\max}$  and  $f_{\min}$ 

$$\textcircled{1} f_{\max} = 0.85 \times \beta \times \frac{f'_c}{f_y} \times \left( \frac{\epsilon_u}{\epsilon_u + \epsilon_t} \right)$$

$$f_{\max} = 0.85 \times 0.85 \times \frac{4}{60} \times \left( \frac{0.003}{0.003 + 0.005} \right)$$

$$\therefore f_{\max} = 0.018$$

$$\textcircled{2} f_{\min} = \frac{200}{f_y} = \frac{200}{60,000} = 0.003$$

$$\textcircled{3} f = \frac{A_{st}}{bd} = \frac{1.03}{14 \times 25}$$

$$f = 0.00294$$

Here  $f_{min} > f < f_{max}$   
 $0.003 > 0.00294 < 0.018$

As  $f'$  is less than  $f_{min}$   
 then we have:

$$f = \frac{A_{st}}{bd} \Rightarrow A_{st} = f * bd$$

$$f = 0.003 * (14 * 25) = 1.05 \text{ in}^2$$

Step 5 :- Selection and No. of Bar :-

let try ~~#10~~ #10 main bar  
 Area of 1 #10 = 1.27 in<sup>2</sup>

$$\text{No. of Bar} = \frac{A_{st}}{A_b} = \frac{1.05}{1.27}$$

$$\text{No. of Bar} = 1.3 \approx 2$$

So take 2 #10 Main Bars

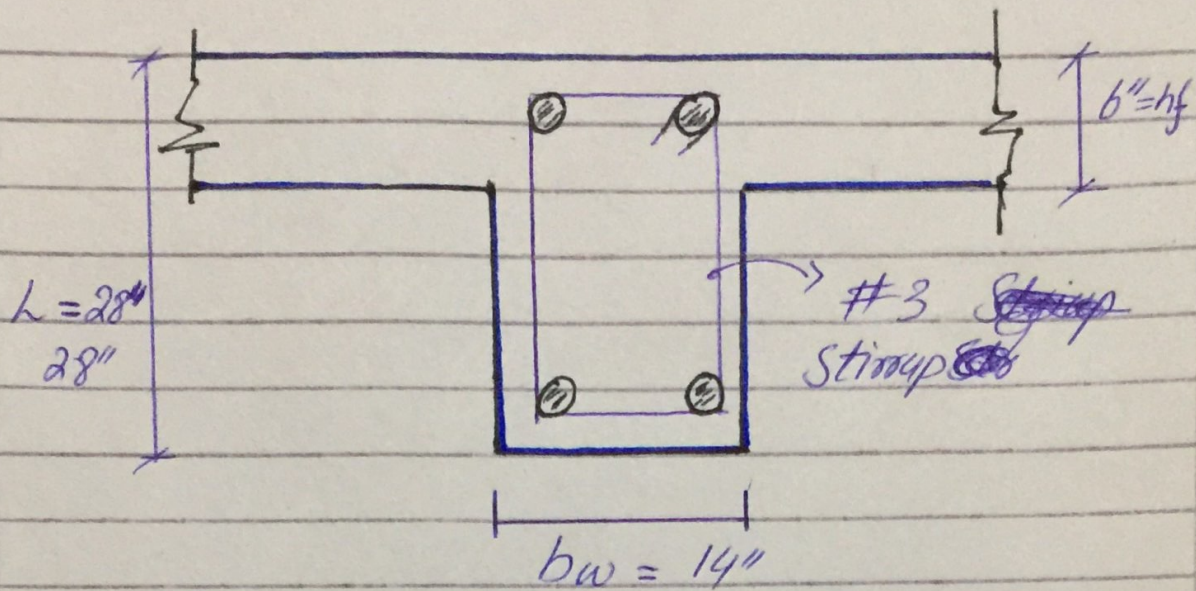
Step 6 :-

"Checked On Minimum  
 width"

$$b_{min} = 2 * 1.5 + 2 * \left(\frac{3}{8}\right) + 2 \left(\frac{10}{8}\right) + \left(\frac{10}{8}\right)$$

$$b_{min} = 7.5" < 14"$$

"So it is good in one layer"



Step 7 :- "Design Moment"

$$M_d = \phi * f_y * A_{st} * \left( d - \frac{a}{2} \right) \quad \text{--- (*)}$$

First  $a = ?$

$A_{st} = \text{area of 1 bar} * \text{No. of Bar}$

$$A_{st} = 1.27 * 2 \quad \text{--- Area of 1 \#10} = 1.27 \text{ in}^2$$

$$A_{st} = 2.54 \text{ in}^2$$

Now

$$a = \frac{A_{st} * f_y}{0.85 * f'_c * b_e} = \frac{2.54 * 60}{0.85 * 4 * 96}$$

$$a = 0.46 \text{''}$$

Put value in eq (\*) we got ( $M_d$ )

$$M_d = 0.90 * 60 * 2.54 * \left( 25 - \frac{0.46}{2} \right)$$

$$M_d = 3396.9$$

$$\text{Here } 3396.9 \text{ k''} > 1396.22 \text{ k''}$$

"Thus Design is Okay"