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Subject  $\approx$  Advance fluid 2

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Date  $\approx$  26/8/2020



Ans H 01:

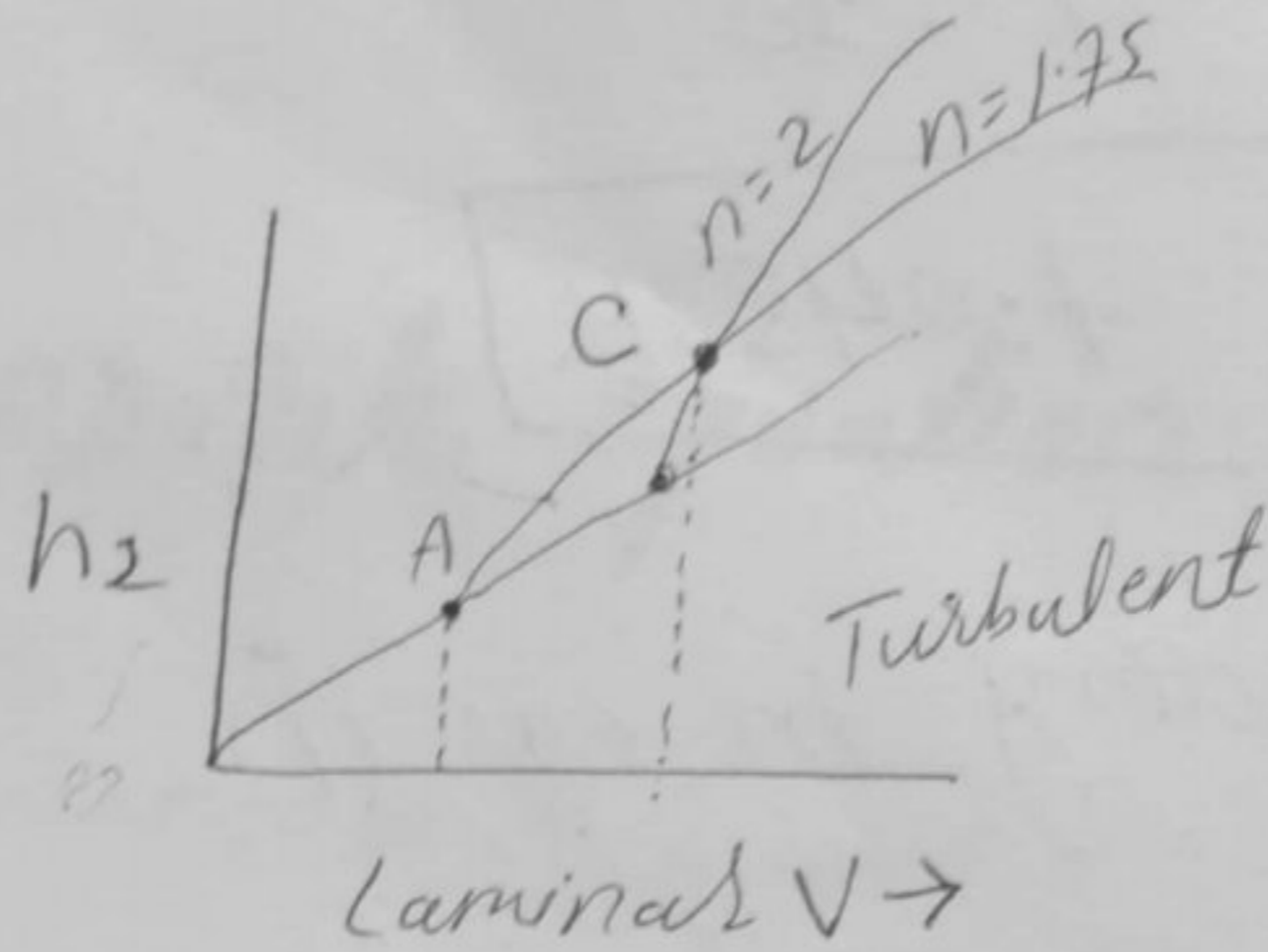
part (B):

Critical Reynolds number:-

If head loss in given length of uniform pipe is measured at different values of velocity. It is found that as long as velocity is low enough to secure laminar flow, the head loss to secure laminar flow, the head loss due to friction will be directly proportional to velocity, but increase in velocity, change from laminar to turbulent change in head loss. Thus if values are plotted, lines obtained with slope about 1.75 to 2. Thus for laminar, drop of energy varies as  $V$  and for turbulent, friction varies



as  $V^n$  where  $n$  is 1.75 to 2.



The upper critical Reynolds number corresponding to point B is indeterminate and depends upon care taken to prevent initial disturbance. Its value is 4000. But normally it is impossible for flow to be in straight one then after " $R$ " is at 2000. Thus lower value is much more definite than higher one and is dividing point. Thus lower value is true Critical Reynolds Number.

Mathematical form  $\Rightarrow$  
$$R_{cr} = \frac{DV_{cr}}{\nu}$$



Ans H 01<sup>3</sup>  
" part (A)

" Velocity profile equation::

$$\text{As } h_L = \frac{\tau 2L}{\rho g}$$

from viscosity  $\therefore \tau = \mu \frac{du}{dy}$   
where  $u$  is a value of velocity at distance  
 $y$  from boundary.

$$y = r_0 - r$$

$$dy = dr_0 - dr$$

$$dr_0 = \text{const} = 0$$

$$\therefore dy = -dr$$

$$\tau = -\mu \frac{du}{dr}$$

$$\text{Now } h_L = \frac{-\mu du 2L}{\rho g dr}$$

$$du = -\frac{h_L \rho g}{2\mu L} r dr$$

P.T.O



integrating:-

$$\int du = \frac{-h\gamma r}{2\mu L} \cdot \frac{r^2}{2} + C$$

$$u = \frac{-h\gamma r}{2\mu L} \cdot \frac{r^2}{2} + C$$

As;  $u = u_{\max}$

$\therefore C = u_{\max}$

$$u = u_{\max} - \frac{h\gamma r}{2\mu L} \cdot \frac{r^2}{2}$$

$$u = u_{\max} - k r^2$$

Now; As we know that  $u=0$

where  $r = r_0$

$$u_{\max} = k r_0^2 = \frac{h\gamma r}{4\mu L} \cdot r_0^2$$

It is also known as Ver

$$V_c = \frac{h\gamma r}{4\mu L} \cdot r_0^2 = \frac{h\gamma r \cdot D^2}{16\mu L}$$

P.T.O.



The average velocity may be taken as;

$$V_s = \frac{V_{cr} + 0}{2} = 0.5 V_{cr}$$

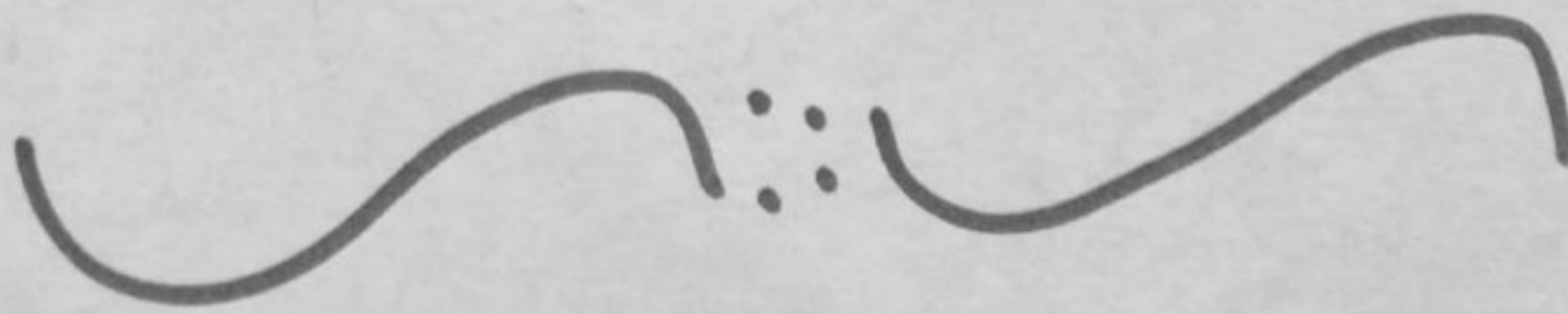
$$= \frac{hLV D^2}{32\mu L}$$

As  $R = \eta S$ ,  $\mu/\eta = \nu$

$$\lim \frac{32\mu LV}{D^2} = \frac{32\mu LV}{\eta \cdot D^2} = 32 \nu \frac{L}{D^2} \nu$$

$\int du$

$$= u = \frac{1}{2} \text{ Ans.}$$





Ans: 02;

"Given Data"

Oil;

$$S = 0.7$$

$$\text{Kinematic viscosity} = 1.8 \times 10^{-5} \text{ m}^2/\text{s}$$

Flow;

$$\text{Pipe dia} = 150 \text{ mm} = 0.15 \text{ m}$$

$$Q = 0.5 \text{ m}^3/\text{s}$$

"Required Data";

Centerline velocity,  $V_{\text{max}} = ?$

Velocity at 10mm from edges = ?

Velocity at edge of pipe = ?

Max shear stress at wall pipe = ?

"Solution";

Check the flow of oil;

$$V = \frac{Q}{A} = \frac{0.5}{\frac{\pi}{4} (0.15)^2}$$

$$V = 28.29 \text{ m/s}$$



$$* R = \frac{Dv}{\nu} = \frac{(0.15)(28.29)}{1.8 \times 10^{-5}}$$

$$\boxed{R = 235750 > 2000}$$

"Flow is turbulent"

$$* f = \frac{0.316}{R^{0.25}} = \frac{0.316}{(235750)^{0.25}}$$

$$\boxed{f = 0.0143}$$

\* Centerline velocity;

$$V_{max} = v \left( 1 + 1.33 \sqrt{f} \right)$$

$$= 28.29 \left( 1 + 1.33 \sqrt{0.0143} \right)$$

$$\boxed{V_{max} = 32.74 \text{ m/s}}$$

\* Velocity at 10mm from edges;

$$U = V_{max} - 2.5 \sqrt{\frac{\tau_0}{\rho}} \ln \frac{y_0}{y_0 - y} \quad \text{--- (10)}$$

First calculate shear;

$$\tau_0 = \frac{f \cdot \rho \cdot v^2}{8} = \frac{(0.0143)(0.7 \times 1000)(28.29)^2}{8}$$

$$\boxed{\tau_0 = 1001.40 \text{ N/m}^2}$$

"Shear stress at wall"



\* (1) ⇒

$$V_{10\text{mm}} = V_{\text{max}} - 2.5 \sqrt{\frac{1001.4}{0.7 \times 1000}} \cdot \ln \frac{0.075}{0.075 - 0.01}$$

$$V_{10\text{mm}} = 32.31 \text{ m/s}$$

\* Velocity at edge;

$$U_{\text{max}} = V (1 + 1.32 \sqrt{f})$$

$$V = \frac{V_{\text{max}}}{1 + 1.32 \sqrt{f}}$$

$$V = \frac{32.74}{1 + 1.32 \sqrt{0.0143}}$$

$$V = 28.24 \text{ m/s}$$

