

Name

Fatmatullah Khan

ID

7883

Subject

PRC'D

Semester

6th

Section

B

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Eng Fowad Khan

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02

Q1

ANSWERS :

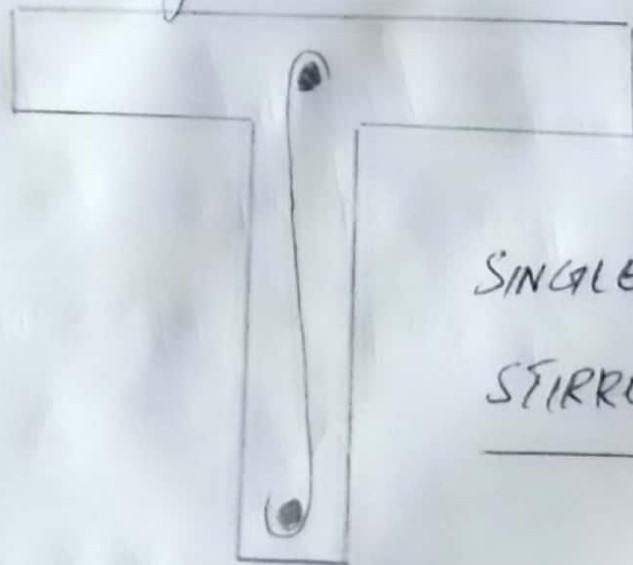
Following are the types of stirrups

- ① Single legged stirrups
- ② Two legged or Double legged stirrups
- ③ Four legged stirrups.
- ④ Six legged stirrups.

1)

SINGLE LEGGED STIRRUPS :

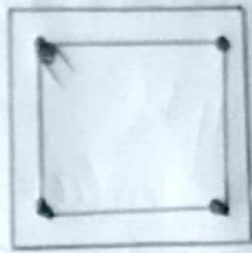
These type of stirrups are used to hold the longitudinal bars in position and prevent buckling.



SINGLE LEGGED STIRRUP.

## DOUBLE LEGGED STIRRUP:

We use a single stirrup to tie a beam or a column at a time. We say it is two legged stirrup. Double legged stirrups are adequate for typical beams with relatively short width.

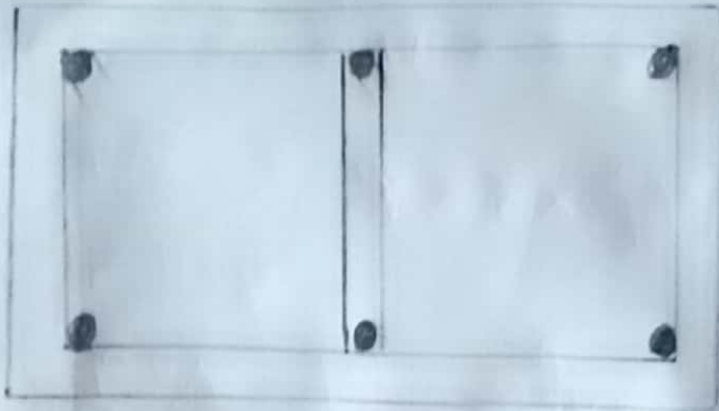


Two - legged stirrups.

## FOUR LEGGED STIRRUPS:

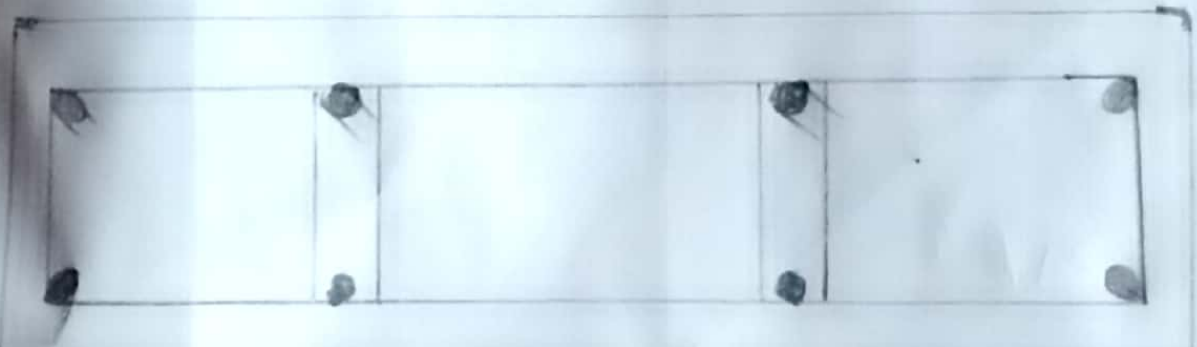
We use double stirrups to tie a beam or column at a time. We say it is four legged stirrups. For beam having longer width multiple legged or four legged stirrups are required.

(3)



## SIX LEGGED STIRRUP:

These six legged stirrups are generally used for a continuous beam structure, it consists of regular upholding of structure at each junction while joints at the joining of beam and column.



(2) Compute shear strength capacity of concrete,  $V_c = 2 \times \sqrt{f_c} \times b_w \times d$

(3) Compute Minimum Web Reinforcement.

If  $V_u \leq \phi \times V_c$  so no web reinforcement needed. If it is not applicable then min area of web reinforcement equal to:

$$i) A_{v_{min}} = 0.75 \times \sqrt{f_c} \times \frac{b_w \times s}{f_y} \quad \text{OR} \quad A_{v_{min}} = \frac{50 \times b_w \times s}{f_y}$$

→ Max spacings can be found by these formulas.

$$s_{max} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c} \times b_w} \quad \text{OR} \quad s_{max} = \frac{A_v \times f_y}{50 \times b_w}$$

(4) If  $V_u \leq \frac{\phi V_c}{2}$ , if it is true no stirrups are required.

(5) First stirrup is provided at a distance  $s/2$  " " spacing  $b_w$  between " $V_u$ " and " $\phi V_c$ " web reinforcement is found by formulas

$$S = \frac{\phi \times A_v \times f_y \times d}{V_u - \phi V_c}$$

If  $V_s \leq 4 \times \sqrt{f_c} \times b_w \times d$ ; Then  
 max spacing of stirrups will be  
 smallest of the following four conditions.

- 1-  $\geq 4"$
- 2-  $\frac{d}{2}$
- 3-  $S_{max} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c} \times b_w}$
- 4-  $S_{max} = \frac{A_v \times f_y}{50 \times b_w}$

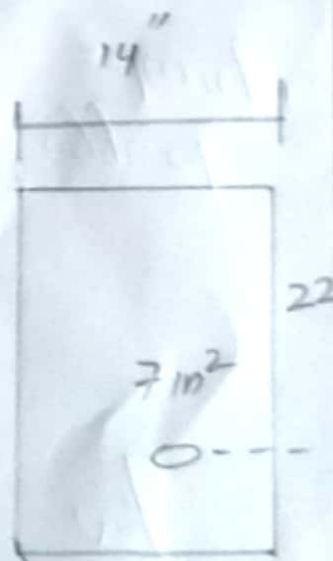
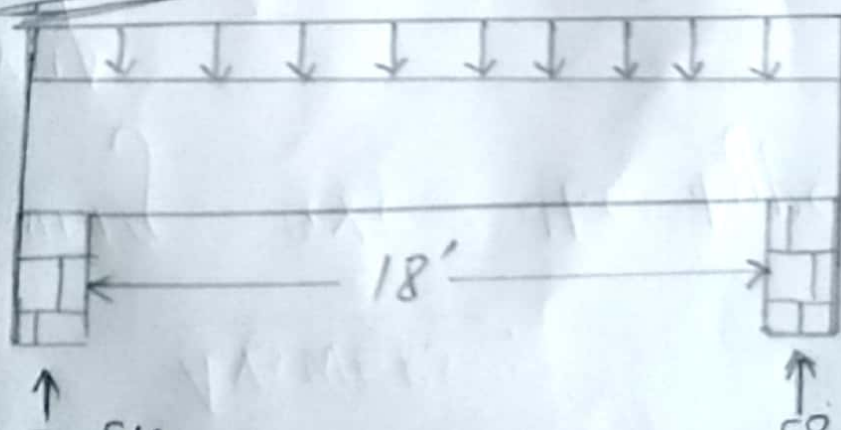
If  $V_s > 4 \times \sqrt{f_c} \times b_w \times d \rightarrow$  Then max  
 spacing will be halved.

If  $V_s > 8 \times \sqrt{f_c} \times b_w \times d$

Then either increase cross-sectional  
 dimensions or increase  $f_c$ .

Solutions:

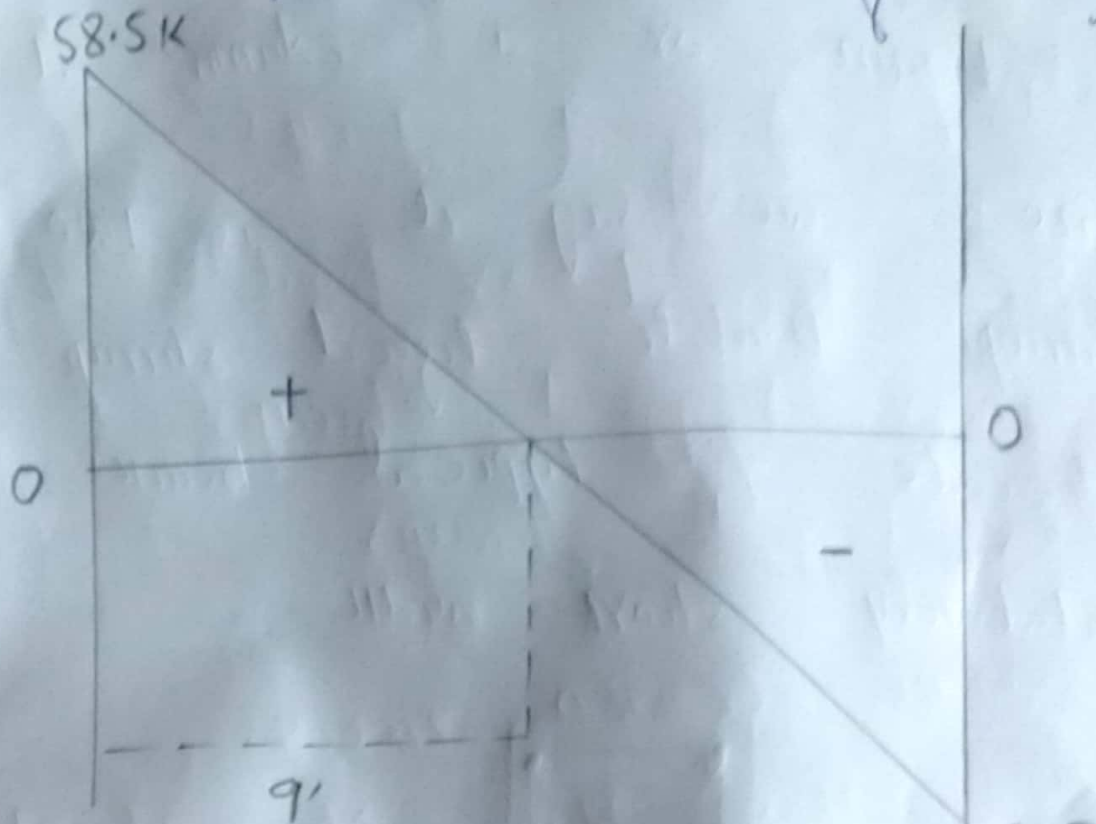
$$W_u = 6.5 \text{ K/ft}$$



Step-01: Find the Reaction on support

$$\text{Total load} = \frac{6.5 \times 18}{2} = 58.5 \text{ K}$$

Steps-02: Draw its shear force diagram



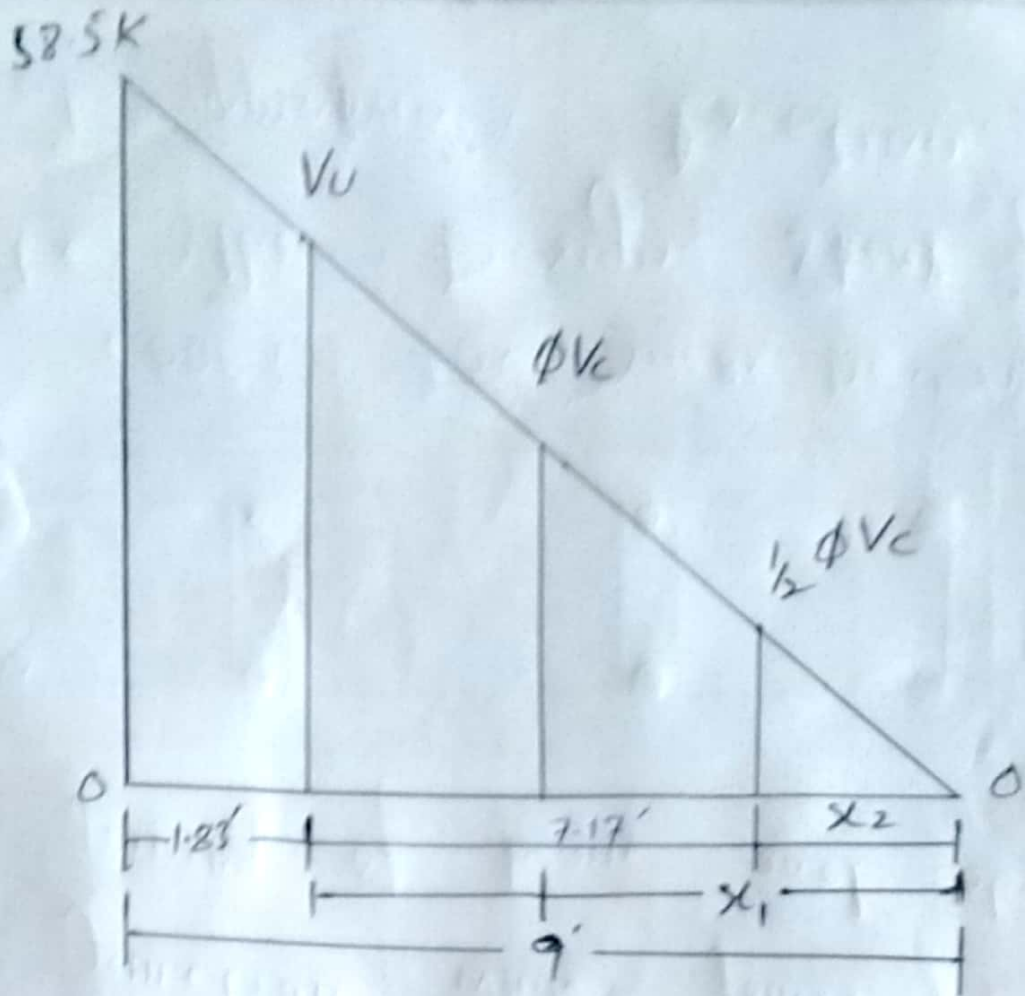
Step:3 Finding the value of critical stress " $V_u$ " and its location.

As we know that critical shear is located at a distance (d) from the face of supports  $d = 22'' = 1.8$ .

Using Similarity of Triangles.

P.T.O

(7)



$$\frac{58.5}{9} = \frac{V_u}{7.17}$$

$$V_u = \frac{58.5 \times 7.17}{9} = 46.605 \text{ K}$$

Step # 4 Finding the value of " $\phi V_c$ " and " $\frac{1}{2} \phi V_c$ " and also its distance from zero shear to right side.

By formula,

$$\begin{aligned} \Rightarrow \phi V_c &= \phi \times 2 \times \sqrt{f_c} \times b_w \times d \\ &= 0.75 \times 2 \times \sqrt{4000} \times 14 \times 22 \\ &= 129.21 \text{ K} \end{aligned}$$



(8)

⊕ Location of  $\phi V_c$  by similar triangles

$$\frac{52.5}{9} = \frac{\phi V_c}{x_1} \Rightarrow \frac{52.5}{9} = \frac{29.21}{x_1}$$

$$\Rightarrow \boxed{x_1 = 4.49'}$$

Now  $\rightarrow \frac{1}{2} \phi V_c = \frac{29.21}{2} = 14.60K$

$\rightarrow$  location of  $\frac{1}{2} \phi V_c$  will be

$$\frac{58.5}{9} = \frac{14.60}{x_2}$$

$$\boxed{x_2 = 2.24'}$$

Step 05: Finding the value of  $\phi V_s$

$$\begin{aligned} \phi V_s &= V_u - \phi V_c \\ &= 46.605 - 29.21 \end{aligned}$$

$$\boxed{\phi V_s = 17.395}$$

Step 06: Check on section adequacy  
By formulae.

$$= \phi \times 8 \times \sqrt{f_c} \times b_w \times d$$

$$= 0.75 \times 8 \times \sqrt{4000} \times 14 \times 22$$

(9)

$$= 116.87K$$

As  $\phi \times 8 \times \sqrt{f_c'} \times b_w \times d > \phi V_s$  Thus section is adequate.

Step 07: Check on Max spacing for

Stirrups

By Formula:

$$= \phi \times 4 \times \sqrt{f_c'} \times b_w \times d = 0.75 \times 4 \times \sqrt{4000} \times 14$$
$$= 58.43K$$

As  $\phi \times 4 \times \sqrt{f_c'} \times b_w \times d > \phi V_s$

So, Max spacing will be selected from

The following condition.

1 - 24"      2 -  $\frac{d}{2} = \frac{22}{2} = 11"$       3 -  $s_{max} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c'}}$

Let suppose we use #3 stirrup,

$$\underline{dia} = \frac{3}{8} = 0.375$$

$$\text{Area} = \frac{\pi}{4} (0.375)^2 = 0.11 \text{ in}^2$$

(10)

For 2-legged stirrup Area  $\times 2$

$$= 0.11 \times 2 = 0.22 \text{ in}^2$$

$$3- \delta_{\max} = \frac{0.22 \times 60000}{50 \times b_w} = 18.25''$$

$$4- \delta_{\max} = \frac{0.22 \times 60000}{50 \times b_w} = 18.25''$$

$$(5) \delta_{\max} = \frac{40 \times f_y}{50 \times b_w} = \frac{0.22 \times 60000}{50 \times 14} = 19.87''$$

So we choose the least value from

the above values  $\delta_{\max} = 11''$

Step # 08: Stirrups spacing from/cr

critical section.

By formula.

$$\delta = \frac{\phi \times A_v \times f_y \times d}{V_u - \phi V_c}$$

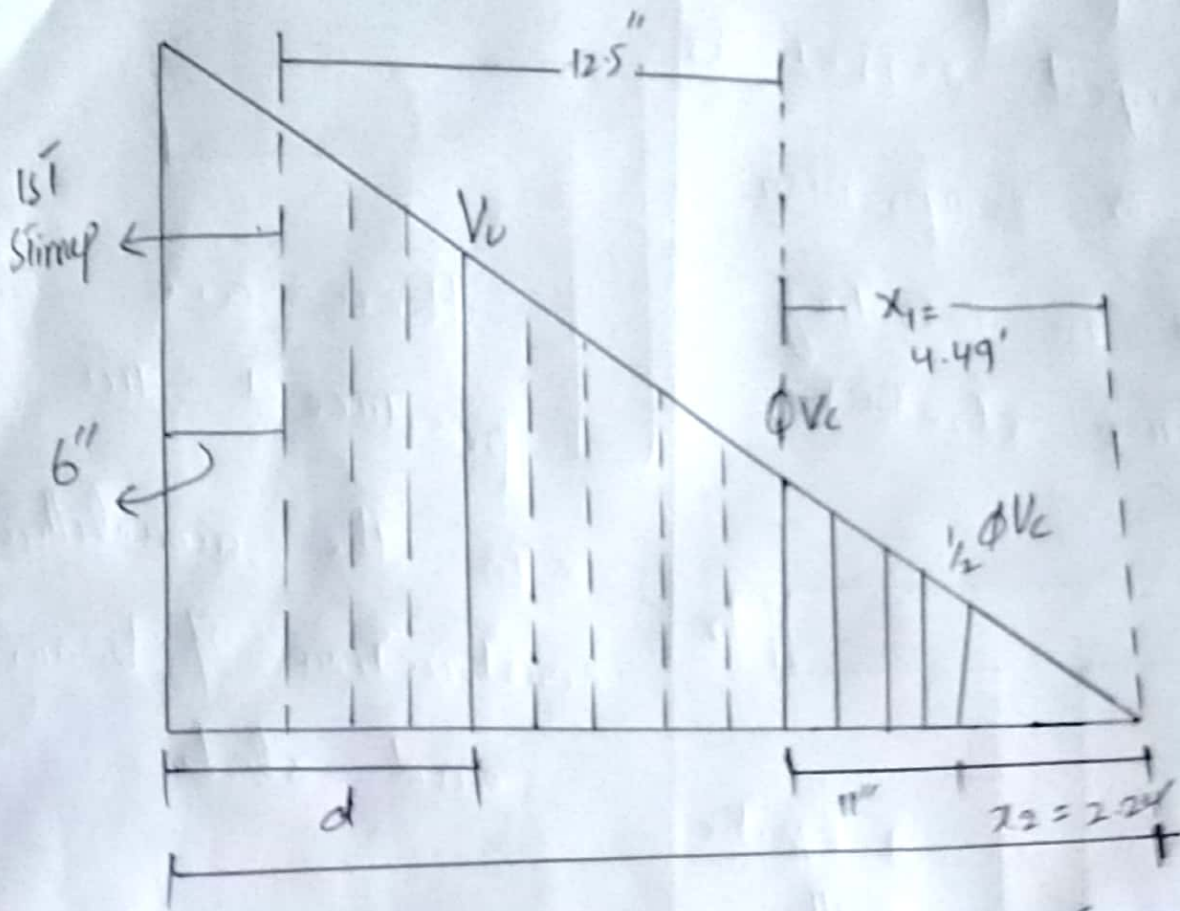
$$= \frac{0.75 \times 0.22 \times 60 \times 22}{46.605 - 29.21}$$

$$\delta = 12.52 \approx 12.5''$$

So 12.5 c/c

Step 09 Final Sketch will be.

58.5K



First stirrup from face of support

$$s/2 = \frac{12.5}{2} = 6.25 \approx 6''$$

1) Definition:

T-Beam:

It is load bearing structure of reinforced concrete, wood or metal, with

L-Beam

A beam whose has the form of inverted L; used placed so that top flange forms

a T-shaped cross-section  
① The Top of the  
T-shaped serves as  
Flange or compression  
member in resisting  
compressive stresses.

