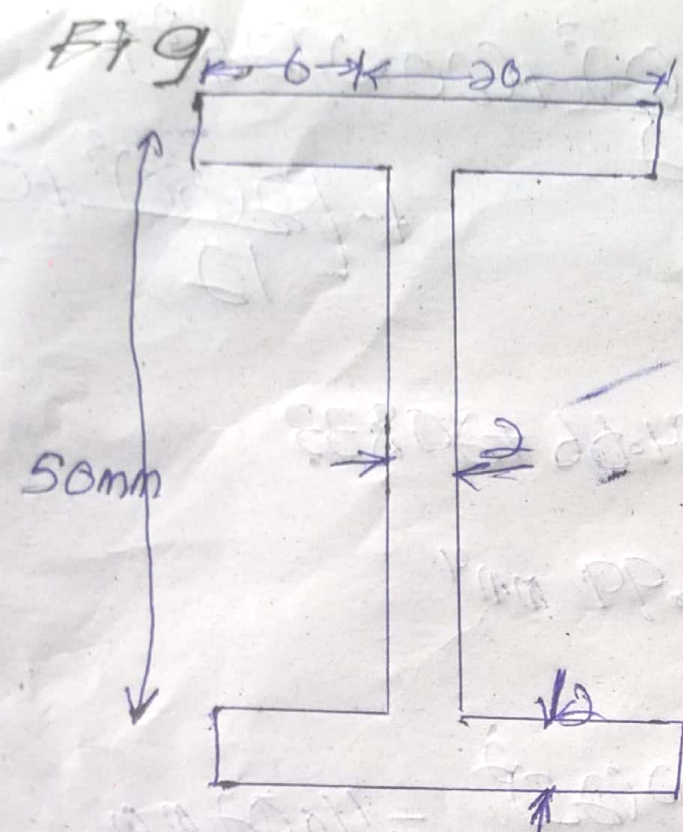


Q1

(9)



Required:-

location of shear centre

Sol:-

As we know that

$$e = \frac{t_f h^2 b^2}{4I}$$

and

$$I = 2 \left(\frac{bh^3}{12} + Ah^2 \right) + \left[\frac{bh^3}{12} + Ah^2 \right]$$

$$= 2 \left[\frac{(200)^3}{12} + (200 \times 2)(25)^2 \right]$$

$$+ \left[\frac{2(50)^3}{12} + 0 \right]$$

$$I = 50034.66 + 20833$$

$$I = 70867.99 \text{ mm}^4$$

$$e = \frac{2(50)^2(25)^2}{4(70867.99)} = 110.07 \text{ mm}$$

So,

shear centre $e = 110.07 \text{ mm}$

Q QUESTION NO 1 :-

part (b) :-

Given Data :-

$$\text{Height} = h = 26 \text{ ft}$$

$$D = 22 \text{ ft}$$

$$\text{tangential stress} = 600 \text{ lb/ft}$$

specific weight of water

$$\text{tank} = 62.4 \text{ lb/ft}^3$$

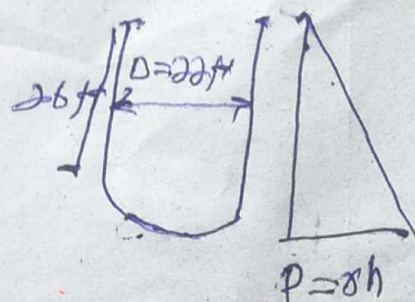
Required :-

To find the thickness = ?

Solution :-

The pressure developed
by water = $P = \gamma h$

$$\sigma_t = \frac{PD}{2t}$$



(i)

$$6t = \frac{PD}{\rho} \Rightarrow \frac{\rho h D}{\rho t}$$

$$\rho t \times 6t = \rho h D$$

$$\rho t = \frac{\rho h D}{6t}$$

$$t = \frac{\rho h D}{6t}$$

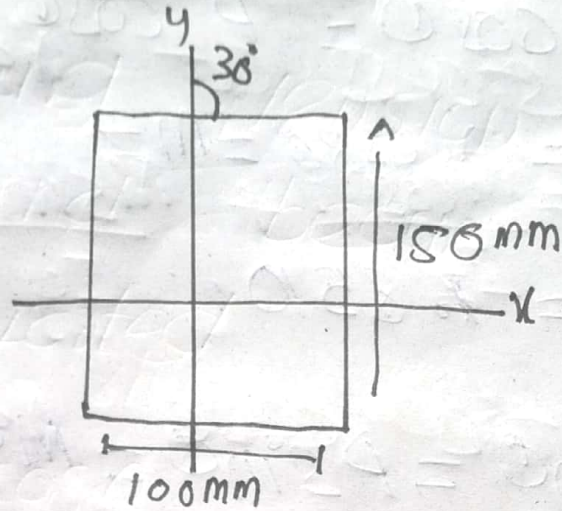
$$t = \frac{(60 \times 4) \times (26 \times 12) \times (22 \times 12)}{(12)^3}$$

$$6000 \times 2$$

$$t = 0.24''$$

Question NO 2

(a)



Moment of Inertia

$$I_x = \frac{bh^3}{12} = 0.1 \frac{(0.15)^3}{12}$$

$$I_x = 2.8125 \times 10^{-5}$$

Now,

$$I_y = \frac{bh^3}{12} = 0.15 \frac{(0.1)^3}{12}$$

$$I_y = 1.25 \times 10^{-5}$$

$$\sigma = \frac{M_z y}{I_z} + \frac{M_y z}{I_y}$$

$$\sigma = \frac{M \cos \theta}{I_z} + \frac{M \sin \theta}{I_y}$$

where

$$M = G \cos \theta = P \cos \theta = M_z$$
$$= 12 \cos 30^\circ = M_z$$

$$M_z = 10.8510$$

$$M \sin \theta = P \sin \theta = M_y$$

$$M_y = 12 \sin 30^\circ$$

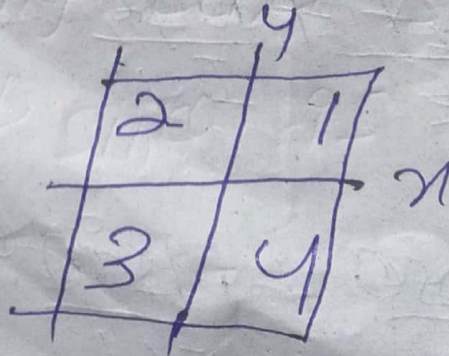
$$M_y = -11.08563$$

$$\sigma = \left(\frac{M_z}{I_z} \right) + \left(\frac{M_y}{I_y} \right)$$

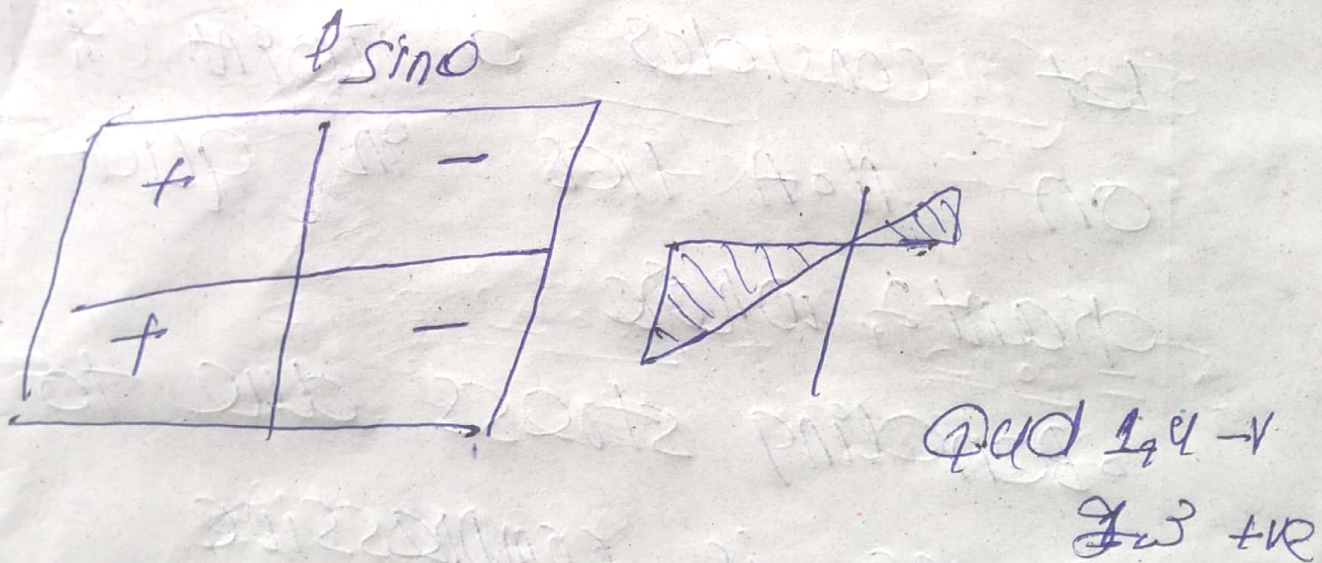
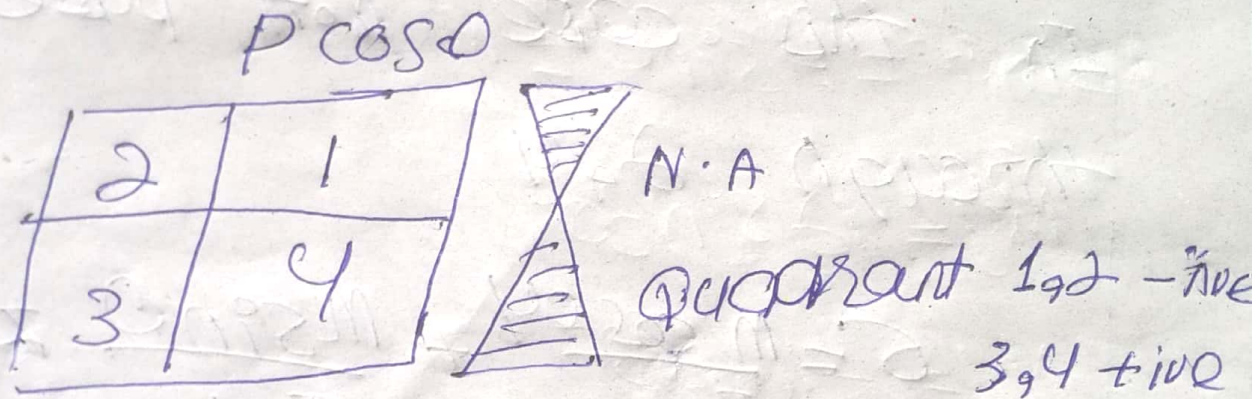
$$\sigma = \left(\frac{10.851}{2.812 \times 10^5} + \frac{(-11.08563)}{1.25 \times 10^5} \right) =$$

$$882678 \text{ Nm}^3$$

sign convention



If we take compression as negative and tension as positive and beam is simply supported



In case of unsymmetrical roofing in neutral axis lies at an angle of (α) the principal axis

and the algebraic sum of stress at NoA is 0.

$$\sigma = \frac{M \cos \theta y}{I_z} + \frac{M \sin \theta z}{I_y} \quad \rightarrow (i)$$

In this case NoA passes through z, y

$$\sigma = \frac{M \cos \theta y}{I_z} + \frac{M \sin \theta z}{I_y}$$

Let consider \circ point (A) on NoA lies in quadrant 2, where

- Bending stress due to $P \cos \theta$ is compressive
- Bending and stress due to $P \sin \theta$ is tensile.

$$\text{CQCD} \Rightarrow 0 = -\frac{m \cos \theta}{I_z} y_A + \frac{m \sin \theta}{I_y} z_A$$

$$\Rightarrow 0 = -\frac{m \cos \theta}{I_z} y_A + \frac{m \sin \theta}{I_y} z_A$$

$$\Rightarrow \frac{m \cos \theta}{I_z} y_A + \frac{m \sin \theta}{I_y} z_A$$

$$\frac{y_A}{z_A} = \frac{I_z \sin \theta}{I_y \cos \theta} \Rightarrow \tan \alpha = \frac{I_z}{I_y} \tan \theta \quad \text{Eq (ii)}$$

Now put values in eq (ii)

$$\tan \alpha = \frac{2.8125 \times 10^{-5}}{1.25 \times 10^{-5}} (\tan 30^\circ)$$

$$\tan \alpha = -14.0424$$

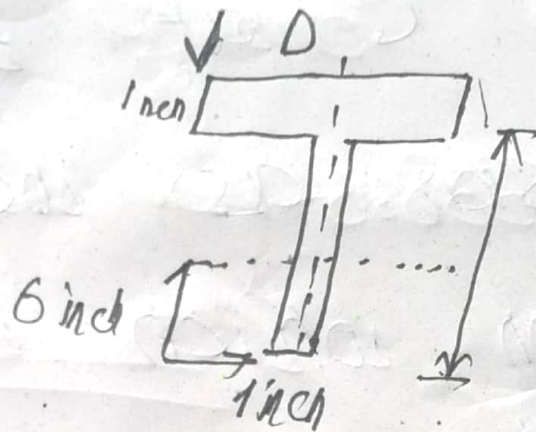
$$\alpha = \tan^{-1}(-14.0424)$$

$$\alpha = 105^\circ$$

$$\alpha = 130.5^\circ$$

Q2

part B



$$L = 16 \text{ ft}$$

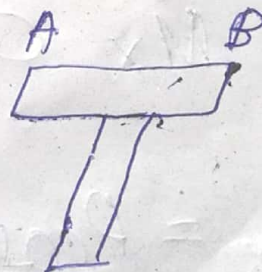
$$I_x = 112.6 \text{ inch}^4$$

$$I_y = 18.7 \text{ in}^4$$

$$S_x = 12000 \text{ PSI}$$

$$S_y = 5000 \text{ PSI}$$

Solⁿ-



By looking fig we can

Judge that max compression

occur on a maximum tension
 at B. There will
 tension as well as compres-
 sion which will reduce
 that effect of each other
 so we will calculate stress
 at A and C.

$$S_A = \frac{M_x y}{I_x} + \frac{M_y x}{I_y} \text{ compression}$$

$$S_C = \frac{M_x y}{I_x} - \frac{M_y x}{I_y} \text{ tension}$$

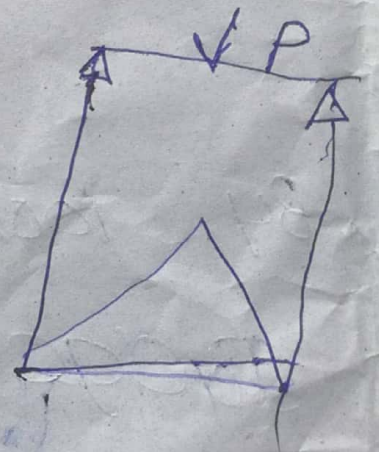
NOW

M_x and M_y .

so

$$M_x = \frac{P \cos 60 \times (10 \times 12)}{40}$$

$$M_y = M_x = 48 P \cos 60$$



$$M_y = \frac{P \sin 60 (16 \times 12)}{4}$$

$$M_y = 48P \sin 60$$

NOW

$$S_A = \frac{M_{xy}}{I_x} + \frac{M_{yx}}{I_y}$$

$$\Rightarrow 1200 = \frac{48P \cos 60 \times 3.07}{112.6}$$

$$= \frac{48P \sin 60 \times 3}{18.07}$$

Solving eq.

$$\Rightarrow P = 1638.08 \text{ lb}$$

NOW

$$S_B = \frac{M_{xy}}{I_x} + \frac{M_{yx}}{I_y}$$

$$5000 = 48P \cos 60 \times (5.93) + \frac{48P \sin 60 \times 0.5}{18.07}$$

$$P = 21011.9 \text{ lb}$$

So, the maximum load

P applied should be

163806 lb.

Q3(a)

Given:-

$$\text{length} = 10 \text{ ft}$$

$$E = 10.3 \times 10^6$$

$$b = 0.75$$

$$h = 2$$

Required: factor of safety = 2

(a) safe load at hinged = ?

(b) safe load at fixed = ?

Solⁿ

(a) safe load at hinged^s

$$L_e = L$$

$$I = I_x = \frac{(0.75)(2)^3}{12} = 0.5 \text{ in}^4$$

$$P_{cr} = \frac{\pi^2 EI \alpha}{L_e^2}$$

$$P_{cr} = \frac{\pi^2 (1.7)(18.3 \times 10^6)(0.05) \pi^2}{(10 \times 12)^2}$$

$$P_{cr} = \frac{50776940}{14400} = 3526.176 \text{ lb.}$$

$$P_{\text{safe}} = \frac{P_{cr}}{\text{factor of safety}} = \frac{3526.176}{2}$$

$$= 1763.088 \text{ lb}$$

(b) π

$$L_e = \frac{L}{2} \text{ (for fixed)}$$

$$L_e = \frac{10}{2} = 5 \text{ ft}$$

$$I = \frac{\pi y^4}{12} = \frac{\pi (0.75)^4}{12} = 0.07 \text{ in}^4$$

$$P_{cr} = \frac{\pi^2 EI \pi^2}{L_e^2} = \frac{(1.7)(18.3 \times 10^6)(0.07)(\pi^2)}{(5 \times 12)^2}$$

$$P_{cs} = \frac{\cancel{7111} 7108771.6}{(60)^2}$$

$$P_{cs} = 19746.58 \text{ lb}$$

$$P_{\text{safe load}} = \frac{19746.58}{2}$$

$$= 9873.29 \text{ lb}$$
