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SECTION "C"

ASSIGNMENT Sessional Assignment. 1

SEMESTER 8th

SUBJECT HYDRAULIC STRUCTURE

SUBMITTED TO ENGR. ADDED KHAN

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QUESTION :-

Establish the stage (head water level) - discharge relationship for a concrete rectangular box culvert using the following data:

$$\text{width} = 1.2 \text{ m}$$

$$\text{Height} = 0.6 \text{ m}$$

$$\text{Length} = 30 \text{ m}$$

$$\text{slope} = 1 \text{ in } 1000$$

$$\text{Manning's } n = 0.013$$

Square-edged entrance condition

Free jet outlet flow

Range of head water level for investigation = 0-3 m

Neglect the velocity of approach.

SOLUTION :

① $H/D \leq 1.2$. For $H < 0.6 \text{ m}$, free flow open-channel conditions prevail.

Referring to fig 10.6 and assuming that the steep slope entry gives entrance control i.e.

the depth at the inlet is critical, For $H = 0.2 \text{ m}$

$$\text{For } H = 0.2 \text{ m}$$

$$\text{ignoring entry loss } y_c = \left(\frac{2}{3}\right) \times 0.2$$

$$= 0.133 \text{ m}$$

$$\text{and } V_c = 1.142 \text{ m/s}$$

This gives the critical slope $(V/n) = 0.00424$.

Therefore the slope of culvert is mild and hence subcritical flow analysis gives

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The following results:

$$Q = 1.2 y_0 \left[\frac{k_2 y_0}{(1.2 + 2y_0)} \right]^{2/3} (0.001^{1/2} / 0.013)^{1/3}$$

$$= 2.92 y_0 \left[\frac{1.2 y_0}{(1.2 + 2y_0)} \right]^{2/3}$$

y_0 (m)	Q ($m^3 s^{-1}$) (equation (i))	y_c (m)
0.2	0.165	0.124
0.4	0.451	0.243
0.6 (=D)	0.725	0.352

At the inlet over a short reach

$$H = y_0 + V^2/2g + kV^2/2g$$

Cross-Drainage And Drop Structure

The entrance loss coefficient, $k_a =$ is as follows

for a square-edged entry 0.5

for a flared entry 0.25

for a rounded 0.05

y_0 (m)	H (m) (equation ii)	Q ($m^3 s^{-1}$)
0.2	0.236	0.165
0.4	0.467	0.451
0.6	0.691	0.725
unif. c. \leftarrow 0.6 \leftarrow (1.2D)	0.72 \rightarrow	0.817 (by interpolation)

$$(2) \quad H/D \geq 1.2$$

(a) For orifice flow

$$Q = C_d (1.2 \times 0.6) [2g(H - D/2)]^{1/2}$$

with $C_d = 0.62$ the following results are obtained.

H (m)	Q (m ³ s ⁻¹)	y ₀ (m) equation i
0.72	1.29	> 0.6 → no orifice flow exists

$$H + S_{0L} = D + h_L$$

Where,

$$h_L = K_e V^2 / 2g + (V_n)^4 / R^{4/3} + V^2 / 2g$$

Thus,

$$Q = 2.08 [H - 0.57]^{3/2}$$

H (m)	Q (m ³ s ⁻¹) equation iv
y ₀ = 0.6 (equation i) ← 0.691 ←	0.723
0.72	0.805
1.00	1.364
2.00	2.487
3.00	3.242

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During rising stages the barrel flows full from $H = 0.72$ and during falling stages the flow becomes free-surface flow when $H = 0.691$ m.

The following table summarizes results.

H (m)	Q (m^3/s)	Type of flow
<u>Rising stages</u>		
0.236	0.163	Open channel
0.467	0.451	open channel
0.691	0.785	open channel
0.720	0.803	pipe flow
1.00	1.364	pipe flow
2.00	2.487	pipe flow
3.00	3.242	pipe flow
<u>Falling stages</u>		
2.00	2.487	pipe flow
1.00	1.364	pipe flow
0.72	0.803	pipe flow
0.691	0.723	pipe flow
0.691	0.751	open channel
0.467	0.451	open channel
0.236	0.165	open channel

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BRIDGE SCOUR :-

BRIDGE SCOUR is the removal of sediment such as sand and rocks from around bridge abutments or piers. Scour by swiftly moving water, can scoop out scour holes, compromising the integrity of a structure.

Effect Of Scour :-

- Lowering the river bed level around pier,
- Destabilize the foundation (pier)

Mechanisms :- of Scour.

⇒ DEVELOPMENT OF SCOUR :-

Vortex system formed in front of the obstruction, and has the form of horseshoe. River flow and the energy of the vortex increased shear stress commence local sediment transport.

⇒ LOCAL SCOUR AT PIERS :-

Occurs due to the acceleration of flow around the pier the formation of flow vortices.

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PROTECTION:-

GRAVEL BAGS:-

Put around pier use for filter function to reduce flow but disadvantages handling cost and potential damage to bags during installation and after a time loose rock due to flow.