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Section :-

A

Subject :-

Advanced Fluid Mechanics

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Question No. 1.

Part (a):
Define Drag with its components. Write down the equations for friction Drag coefficient both in laminar and turbulent boundary layer.

Answer:

FORCES ON IMMERSED BODIES:

A body which is wholly immersed in a homogenous fluid may be subjected to two kind of forces arising from relative motion between body & fluid. These forces are termed as drag & lift. depending on forces either parallel or right angle to motion.

Drag force on submerged body can have 2 components.

(2) Pressure Drag (F_p):-

It is equal to the integration of component in the direction of motion of all forces exerted on surface of body.

$$F_p = C_p \cdot \frac{\rho v^2}{2} \cdot A$$

where C_p depend on shape

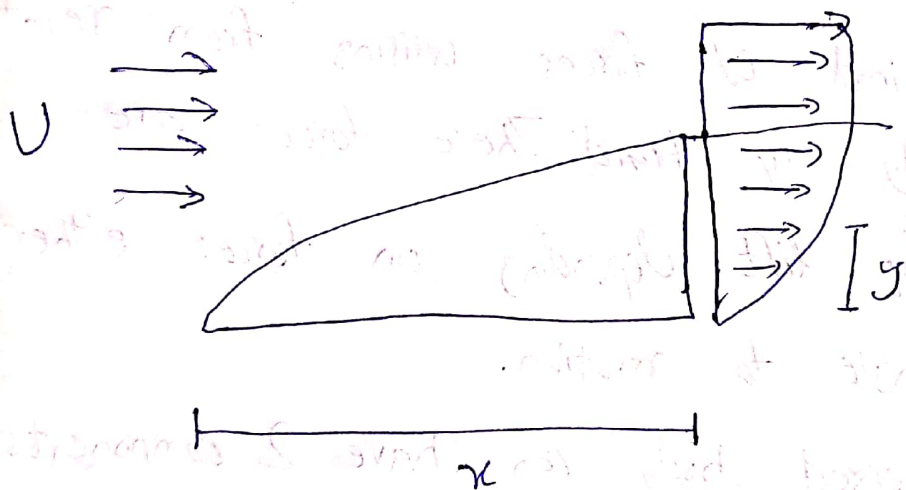
(2) Friction Drag:

It is equal to the integration of component of all shear stresses along the surface in the direction of motion.

$$F_p = C_f \cdot \rho \cdot \frac{V^2}{2} (BL)$$

" C_f " depends on velocity & viscosity

Friction Drag on Boundary layer



$$\bar{Z}_0 = \frac{\mu U \int_0^L f(x) dx}{\rho U^2 L}$$

$$\bar{Z}_0 = \frac{\mu U B}{\rho U^2 L} \quad \text{--- (2)}$$

As we have $Z_0 = \int_0^L v^2 \times \frac{ds}{du}$

Compare with

$$\rho v^2 \propto \frac{d\delta}{dx} = \frac{\mu v B}{\delta}$$

$$\delta d\delta = \frac{\mu B dx}{\rho v \alpha}$$

Integrating on b.s

$$\frac{\delta^2}{2} = \frac{\mu B}{\rho v \alpha} \cdot x + C$$

at $x=0, \delta=0 \Rightarrow C=0$

$$\delta = \sqrt{\frac{2B}{d}} \cdot \sqrt{\frac{\mu x}{\rho v}}$$

$$B = 1.63, \quad d = 0.135$$

$$\delta = \frac{4.91 x}{\sqrt{R_x}} \quad \text{--- (6)}$$

where (R_x) is local Reynold number.

As we have,

$$\tau_0 = \frac{\mu v B}{\delta}$$

$$F_x = \int B v^2 \rho d$$

where d is a function of boundary layer velocity distribution.

Now to find shear stresses.

$$\tau = \frac{F_x}{A} = \frac{dF_x}{B dx} = \frac{dF_x}{B dx}$$

$$\bar{\tau}_0 = \frac{\int \rho u^2 dy}{\rho dy} = \frac{\int u^2 \alpha dy}{dx}$$

LAMINAR BOUNDARY LAYER:

In case of laminar flow,

$$\tau_0 = \mu \left(\frac{dy}{dy} \right)_{y=0} = \frac{\mu}{\delta} \left(\frac{du}{dx} \right)$$

$$= \frac{\mu U}{\delta} \left[\frac{df(\eta)}{d\eta} \right]$$

By solving,

$$\tau_0 = \frac{\mu U B}{\delta}$$

Equating $\Rightarrow \tau_0 = \rho \nu^2 \alpha \frac{df}{dx}$

$$\delta dx = \frac{\mu B}{\rho \nu \alpha}$$

Solving it

$$\frac{f^2}{2} = \frac{\mu B}{\rho U \alpha} x + C$$

At $x=0, f=0, C=0$

$$f = \sqrt{\frac{2 \mu B x}{\rho U \alpha}} = \sqrt{\frac{2 B}{\alpha}} \cdot \frac{x}{\sqrt{R_x}}$$

Experimentally $B = 1.63, \alpha = 0.135$

Putting values in \hookrightarrow

$$\frac{f}{x} = \frac{\sqrt{2 \times 1.63}}{0.135} \times \frac{1}{\sqrt{R_x}} = \frac{4.91}{\sqrt{R_x}}$$

Where R_x may be called the local Reynold number.
It should be noted that R_x increases linearly in
down stream direction.

Now, $F_f = B \int_0^x Z_0 dx \Rightarrow$

$$Z_0 = 0.332 \frac{\mu U}{\rho} \sqrt{R_x}$$

$$R_x = \frac{\rho U f}{\mu}$$

Thus, $F_f = 0.664 B \sqrt{\rho U L U^3}$

where, $F_f = C_f \rho \frac{U^2}{2} BL$

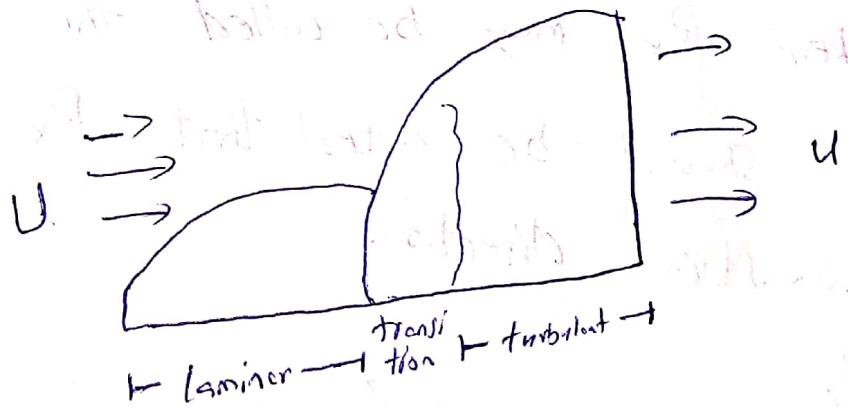
equating both

$$C_f = 1.328 \sqrt{\frac{\mu}{\rho L U}} = \frac{1.328}{\sqrt{R}}$$

For laminar $R \leq 500,000$.

Turbulent Boundary layer:

This fig. shows the velocity distribution of boundary layer which is steeper near walls & flatter through out layer.



The shear stress is greater in turbulent than in laminar.

Thus, $Z_0 = \rho f \frac{U^2}{g}$

where U is the average velocity.

To obtain relation b/w average & max. we have.

$$\frac{V}{U_{\max}} = \frac{1}{1 + 1.33\sqrt{f}}$$

$$\therefore f = 0.028$$

$$\frac{V}{U_{\max}} = \frac{1}{1 + 1.33\sqrt{0.028}}$$

$$U = 1.235 V$$

$$V = \frac{U}{1.235}$$

C_f

$$f = \frac{0.316}{(R_h)^{3/4}}$$

$$Z_0 = f \frac{V^2}{8}$$

$$Z_0 = \frac{0.316}{\left(\left(\frac{P}{2}\right) \left(\frac{V}{1.235}\right)\right)^{3/4}} \cdot \frac{1}{8} \left(\frac{V}{1.235}\right)^2$$

$$Z_0 = \frac{0.23 f V^2}{\left(\frac{2f}{V}\right)^{3/4}}$$

As we have general C_f .

$$Z_0 = \int V^2 \propto \frac{df}{dx}$$

Equation (1) & (2)

$$x=0, \delta=0$$

$$\delta = \left(\frac{0.0287}{\alpha} \right)^{4/5} \left(\frac{V}{\nu x} \right)^{1/5} \cdot x$$

$$d = 0.0972$$

$$\delta = \frac{0.377}{(R_n)^{1/5}} \cdot x \quad \text{--- (3)}$$

$$Z_0 = 0.0597 \frac{V^2}{2} \left(\frac{V}{\nu x} \right)^{1/5}$$

Now

$$F_f = \int_0^L Z_0 dx$$

$$F_f = 0.0735 \frac{V^2}{2} \left(\frac{V}{\nu} \right)^{1/5} \cdot B L$$

$$F_f = C_f \cdot \int \frac{V^2}{2} B \cdot L$$

$$C_f = \frac{0.0735}{(R)^{1/5}}$$

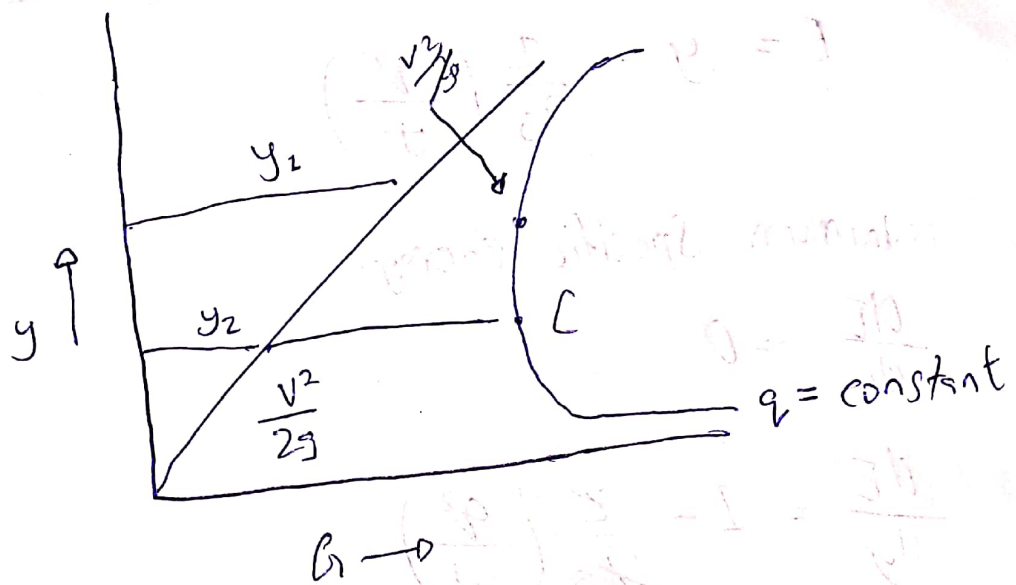
For $R > 10^7$

$$C_f = \frac{0.455}{(\log R)^{2.57}}$$

Question No. 2

Part (b): Derive equation for critical depth, critical velocity of rectangular section of a channel.

Answer:



This is specific energy equation.

For particular q , there will be two kind of possible value of y for given E . The eqn is cubic with three roots with third being negative giving no values. This two alternative depths represents two totally different flow regimes - slow & deep, an upper portion & fast & shallow on lower

Portion.

Point represent dividing point between two regions of flow. Thus for given " q ", value of E is minimum q flow at this point is critical flow. Depth of flow at this point is critical depth y_c q velocity at this point is critical velocity.

Thus relation of critical depth can be found as

$$E = y + \frac{1}{2g} \left(\frac{q^2}{y^2} \right)$$

For minimum Specific energy.

$$\frac{dE}{dy} = 0$$

$$\frac{dE}{dy} = 1 - \frac{2}{2g} \left(\frac{q^2}{y^3} \right)$$

$$\frac{dE}{dy} = 1 - \frac{q^2}{gy^3}$$

$$1 = \frac{q^2}{gy^3} \Rightarrow q^2 = gy^3$$

$$y_{cr} = \left(\frac{q^2}{g} \right)^{1/3} \text{ critical depth}$$

$$\text{As } q = vy, \quad ve^2 = gy^3$$

$$\text{OR } \boxed{ve = \sqrt{gy_c}} \text{ critical velocity}$$

$$y_c = \frac{V_c^2}{g}$$

Now,

$$\frac{y_c}{2} = \frac{V_c^2}{2g}$$

$$E_{min} \Rightarrow y_c + \frac{V_c^2}{2g} = y_c + \frac{y_c}{2}$$

$$\frac{3}{2} y_c \quad \text{OR} \quad y_{cr} = \frac{2}{3}$$

	Subcritical	critical	supercritical
Depth of flow	$y > y_c$	$y = y_c$	$y < y_c$
Velocity	$V < V_c$	$V = V_c$	$V > V_c$
Slope	mild slope $S_1 < S_c$	critical slope	

Question No. 2Given:Depth of Rectangular channel (d) = ?Flow rate (Q) = $3.5 \text{ m}^3/\text{sec}$ Slope of bed (S_0) = 0.0008 $n = 0.0219$ width of Bed = 7820 mm $= 7.820$

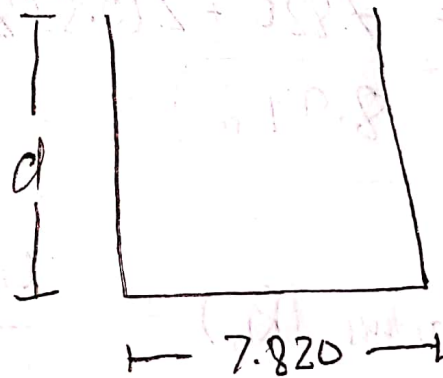
Critical depth = ?

Flow Subcritical or Supercritical = ?

Solution:

$$\begin{aligned} \text{Area} &= 7.820 \times d \\ &= 7.820d \end{aligned}$$

$$\begin{aligned} \text{Perimeter} &= d + 7.820 + d \\ &= 7.820 + 2d \end{aligned}$$



$$\text{Hydraulic Radius } (R_h) = \frac{A}{P}$$
$$= \frac{7.820 d}{7.820 + 2d}$$

By using Manning Equation.

$$Q = \frac{1}{n} A R_h^{2/3} \cdot S_0^{1/2}$$

Putting values.

$$3.5 = \frac{1}{0.0129} \times 7.820 d \times \left(\frac{7.820 d}{2d + 7.820} \right)^{2/3} + (0.0008)^{1/2}$$

$$d = \cancel{0.558} \text{ } 0.558 \text{ m}$$

$$\text{Area} = 7.820 (0.558)$$

$$= 4.36 \text{ m}^2$$

$$\text{Perimeter} = 7.820 + 2(0.558)$$

$$= 8.94 \text{ m}$$

$$\text{Hydraulic Radius } (R_h) = \frac{4.36}{8.94}$$

$$= 0.487 \text{ m}$$

Finding critical depth:-

$$y_{cr} = \left(\frac{q^2}{g} \right)^{1/3}$$

$$\text{As, } q = \frac{Q}{B}$$

$$= \frac{3.5}{7.820}$$

$$= 0.447 \text{ m}^2/\text{sec}$$

$$\Rightarrow y_{cr} = \left(\frac{(0.447)^2}{9.81} \right)^{1/3}$$

$$=$$

$$= 0.281$$

As $y > y_{cr}$

$$0.558 > 0.281$$

So Flow is sub-critical.

Question No. 3

Data:

Friction Drag (F_D) = ?

width (B) = 200 mm = 0.2 m

Length (L) = 800 mm = 0.8 m

Specific Gravity (d) = 0.89

Undisturbed velocity (U) = 5 m/sec

kinematic viscosity (ν) = $0.93 \times 10^{-4} \text{ m}^2/\text{sec}$

Solution:

Checking whether flow is laminar or not

By Reynold Number,

$$R = \frac{DU}{\nu}$$

For smooth flat plate.

$$D = L, \quad U = U$$

$$\text{So } R = \frac{LU}{\nu}$$

$$= \frac{0.8 \times 5}{0.93 \times 10^{-4}} = 43010$$

43010 < 500,000 → Laminar

By using formula:

$$F_f = C_f \cdot J \cdot \frac{V^2}{2} \cdot BL$$

where $C_f = \frac{1.328}{\sqrt{R}} = \frac{1.328}{\sqrt{43010}} = 0.0064$

$$J = \frac{\rho_{oil}}{\rho_{water}} \Rightarrow 0.89 = \frac{\rho_{oil}}{1000}$$

$$\rho_{oil} = 0.89 \times 1000$$

$$\rho_{oil} = 890 \text{ kg/m}^3$$

$$\Rightarrow F_f = C_f \cdot J \cdot \frac{V^2}{2} \cdot BL$$

$$= 0.0064 \times 890 \times \frac{(5)^2}{2} \times 0.2 \times 0.8$$

$$F_f = 11.39 \text{ N}$$