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Section # A

Sub MOS 2

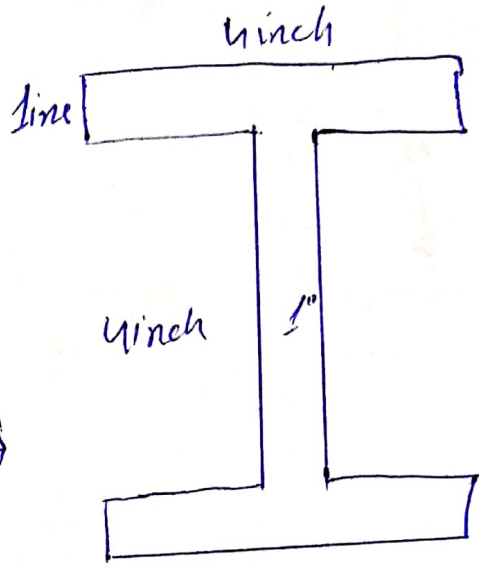
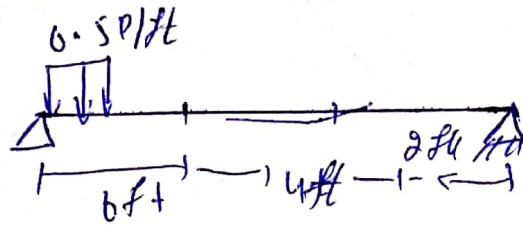
Semester 4th

Degree BE civil

Instructor: Eng Saqib Khan

Question # 1

Ans

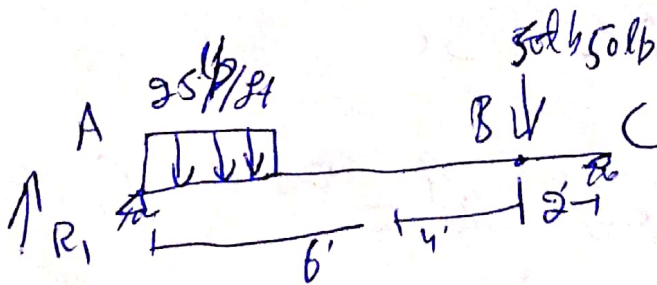
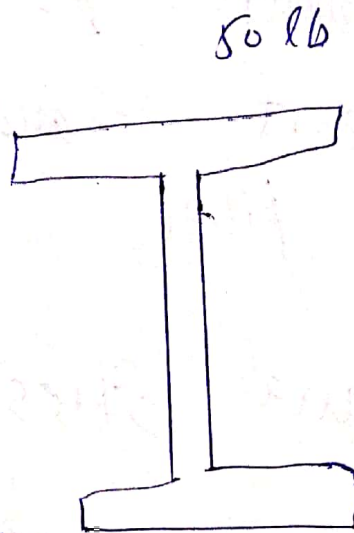


Here My class registration No

7925

So we have

$$2p = 2 \times 25 = 50$$



First we find

②

at the support applying equilibrium Equations
Unknown reaction

$$\sum F_x = 0 \quad \text{i.e.} \quad R_3 = 0$$

$$\sum F_y = 0 \quad \uparrow \downarrow$$

$$R_1 + R_2 = (25 \times 6) \text{ lb} + 50$$

$$R_1 + R_2 = 150 \text{ lb} + 50 \text{ lb}$$

$$\boxed{R_1 + R_2 = 200 \text{ lb}} \quad \text{--- } \textcircled{1}$$

$$R_2 \times 12 - 10 \times 50 - (25 \times 6) \times 3 = 0$$

$$12 R_2 - 500 - 450 = 0$$

$$12 R_2 = 500 + 450 = 950$$

Divid 12 on both side

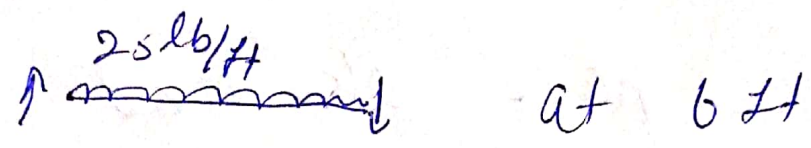
$$R_2 = \frac{950}{12} = 79.166$$

$$R_1 + R_2 = 200 \text{ lb}$$

$$R_1 = 200 - 79.166$$

$$\boxed{R_1 = 120.833}$$

Now shear force at change point of beam



Shear force at 6 ft from support

$\sum F_y = 0$, $\uparrow \downarrow$

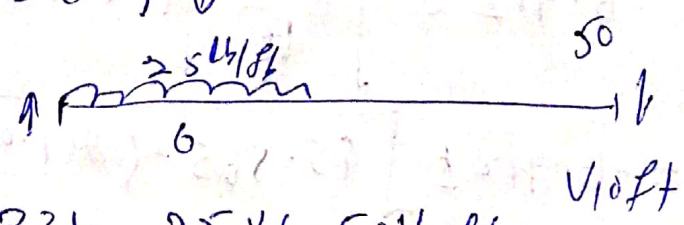
$120 \cdot 834 - 25 \times 6 - V_{6ft} = 0$

$-29 \cdot 166 - V_{6ft}$

$V_{6ft} = -29 \cdot 166$

Now shear force at 10 ft

$\sum F_y = 0$, $\uparrow \downarrow$



$120 \cdot 834 - 25 \times 6 + 50 - V_{10ft} = 0$

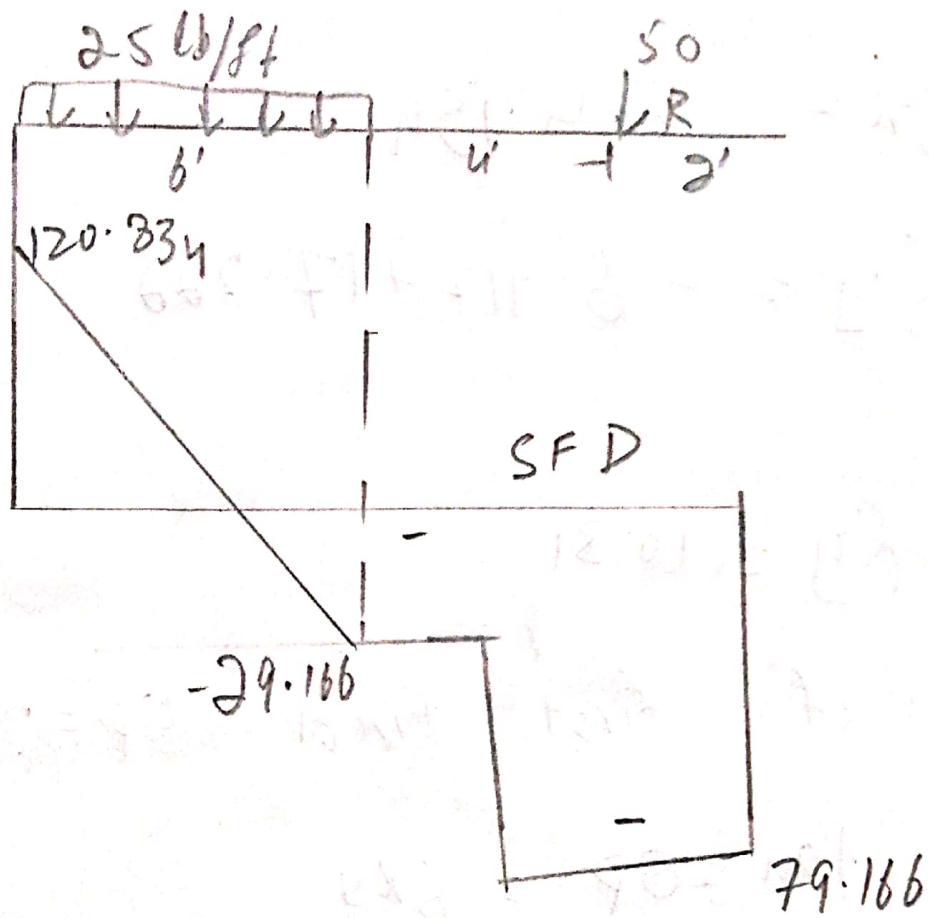
$120 \cdot 834 - 150 - 50 - V_{10ft} = 0$

$120 \cdot 834 - 200 - V_{10ft} = 0$

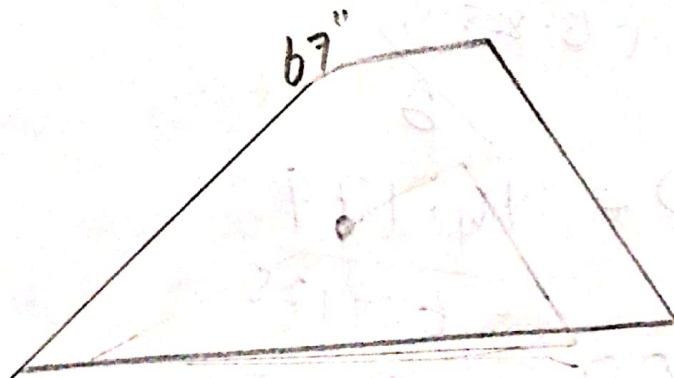
$-V_{10ft} = +79 \cdot 166$

$V_{10ft} = -79 \cdot 166$

Now draw Shear force and Bending Moment diagram we have



B.M.D



Point of Maximum Bending moment

As we know that the point where shear force is zero

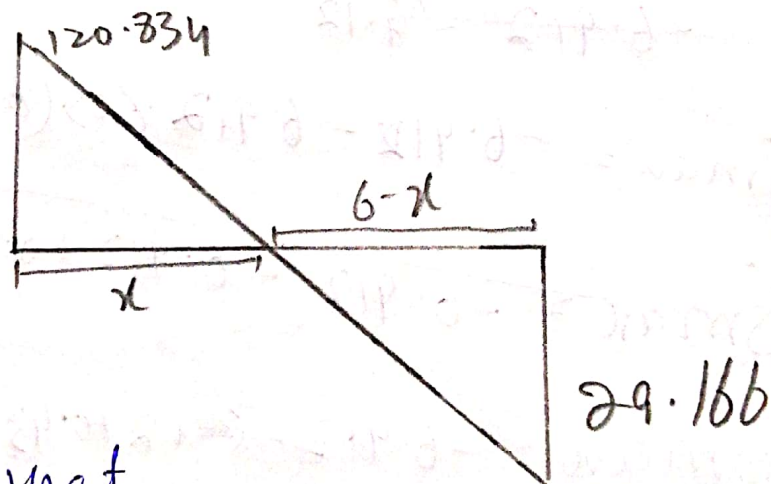
is maximum the bending

moment is maximum so from

point zero shear corresponding point

will have maximum bending moment

from shear force diagram (SFD)



We know that

$$\frac{120.834}{x} = \frac{29.166}{x-6}$$

$$6-x(120.834) = x(29.166)$$

$$725.004 - 120.834x = 29.166x$$

$$725.004 = 29.166x + 120.834x$$

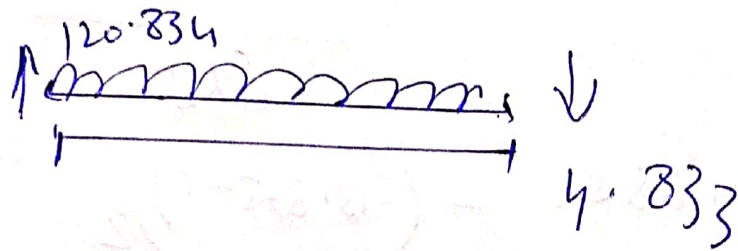
$$725.004 = 150x$$

Dividing 150 on both sides

b.

$$\frac{725.004}{150} = x \Rightarrow 4.833 \text{ ft}$$

Now Determine the value of moment at point 4.833 ft



$$M_{4.833} - 120.834 \times 4.833 + (25 \times 4.833)$$

$$M_{4.833} - 583.990 + 120.825$$

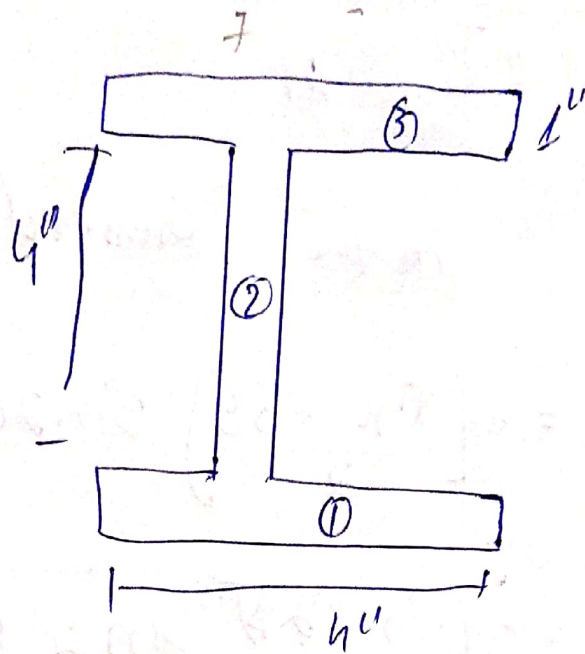
$$M_{4.833} - 463.165$$

$$M_{4.833} = 463.165$$

For shear stress we have

$$\tau = \frac{VQ}{Ib}$$

So first we have determine moment of inertia I of the given section of beam



As the give figure is symmetrical along Both the axis

So $\bar{x} = 4/2 = 2 \text{ inch}$

$\bar{y} = 4/2 = 3 \text{ inch}$

i.e $(\bar{x}, \bar{y}) = (2, 3)$

Centre of gravity

Extreme left and Bottom

Area of point (1) = $4 \times 1 = 4 \text{ inch}^2$
 " " " (2) = $4 \times 1 = 4 \text{ inch}^2$
 " " " (3) = $4 \times 1 = 4 \text{ inch}^2$

Moment of Inertia about x -axis

(Centroidal I) I_{xx}

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Determine the Distance b/w C.G
 of the whole section and corresponding
 parts

let's

G_1, G_2, G_3 be in the centre of
 gravity of point ① ② and ③

and k_1, k_2, k_3 be the distance
 b/w \bar{y} and y_1, y_2, y_3 respectively

So $k_1 = \bar{y} - y_1 = 3 - 0.5 = 2.5 \text{ inch}$

$k_2 = \bar{y} - y_2 = 3 - 3 = 0 \text{ inch}$

$k_3 = \bar{y} - y_3 = 3 - 0.5 = 2.5 \text{ inch}$

So $I_{xx} = \frac{b_1 h^3}{12} + a_1 k_1^2 + \frac{b_2 h^3}{12} + a_2 k_2^2 + \frac{b_3 h^3}{12} + a_3 k_3^2$

$I_{xx} = \frac{4(1)^3}{12} + 4(2.5)^2 + \frac{4(1)^3}{12} + a_2(0)$

+ $\frac{4(1)^3}{12} + 4(2.5)^2$

= $\frac{4}{12} + 25 + \frac{64}{12} + \frac{4}{12} (2.5)$

$I_{xx} = \frac{4 + 12(25) + 64 + 4 + 12(2.5)}{12}$

$$I_{xx} = 56 \text{ inch}^4$$

Now

$$I_{yy} = \frac{b_1^3 h_1}{12} + \frac{b_2^3 h_2}{12} + \frac{b_3^3 h_3}{12}$$

$$I_{yy} = \frac{(4)^3 (1)}{12} + \frac{(1)^3 (4)}{12} + \frac{(4)^3 (1)}{12}$$

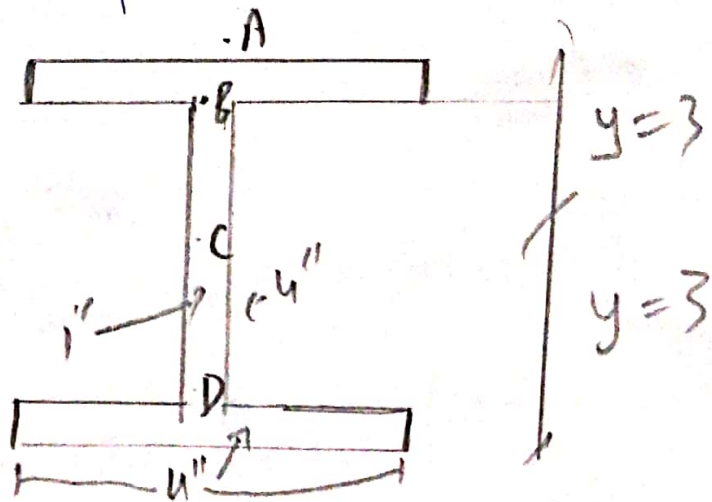
$$I_{yy} = \frac{64}{12} + \frac{4}{12} + \frac{64}{12}$$

$$I_{yy} = \frac{64 + 4 + 64}{12}$$

$$I_{yy} = \frac{132}{12} = 11 \text{ inch}^4$$

Next to find the shear stresses at various point we have

$$\tau = \frac{VQ}{Ib}$$



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Shear Stress at point A
i.e. at the top of fiber

$$\tau = VQ/Ib \quad \therefore Q = Ay$$

So

$$V_{\max} = 79.166 \text{ lb}$$

$$I_{\text{So}} = 67 \text{ inch}^4$$

$$\text{So } \tau = \frac{(79.166)(0)}{67(4)}$$

Here $A=0$ Beam no area
of section or exist about
Point "A"

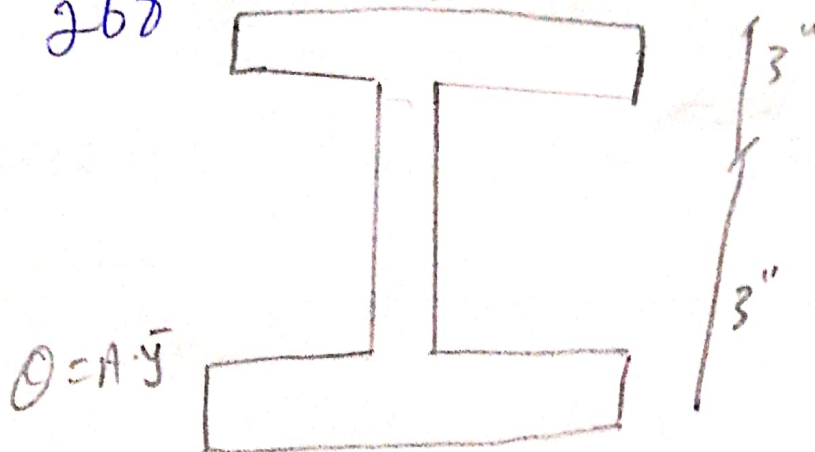
$$\text{i.e. } Q = Ay = 0(\bar{y}) = 0$$

$$\tau = 0$$

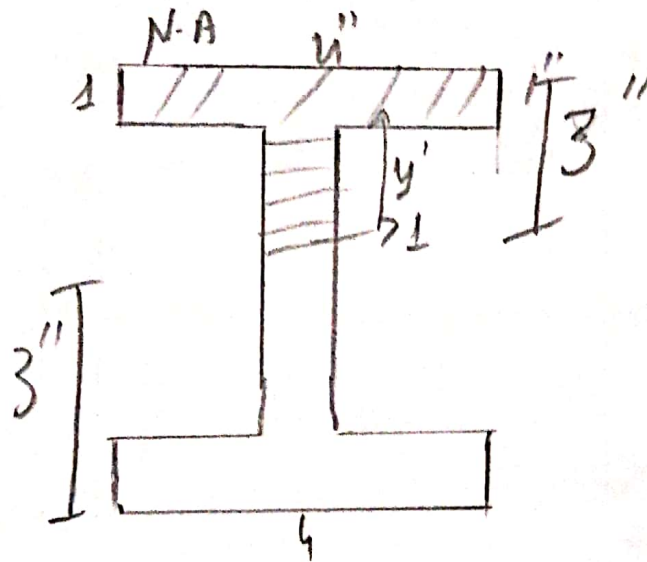
Shear stress at point "B"

$$\tau = \frac{VQ}{Ib} = \frac{(79.166) \times (4 \times 1(3-0.5))}{67 \times 4}$$

$$T = \frac{791.66}{2.68} = 2.951 \text{ (lb/in)}^2$$



iii) Shear stress at point C

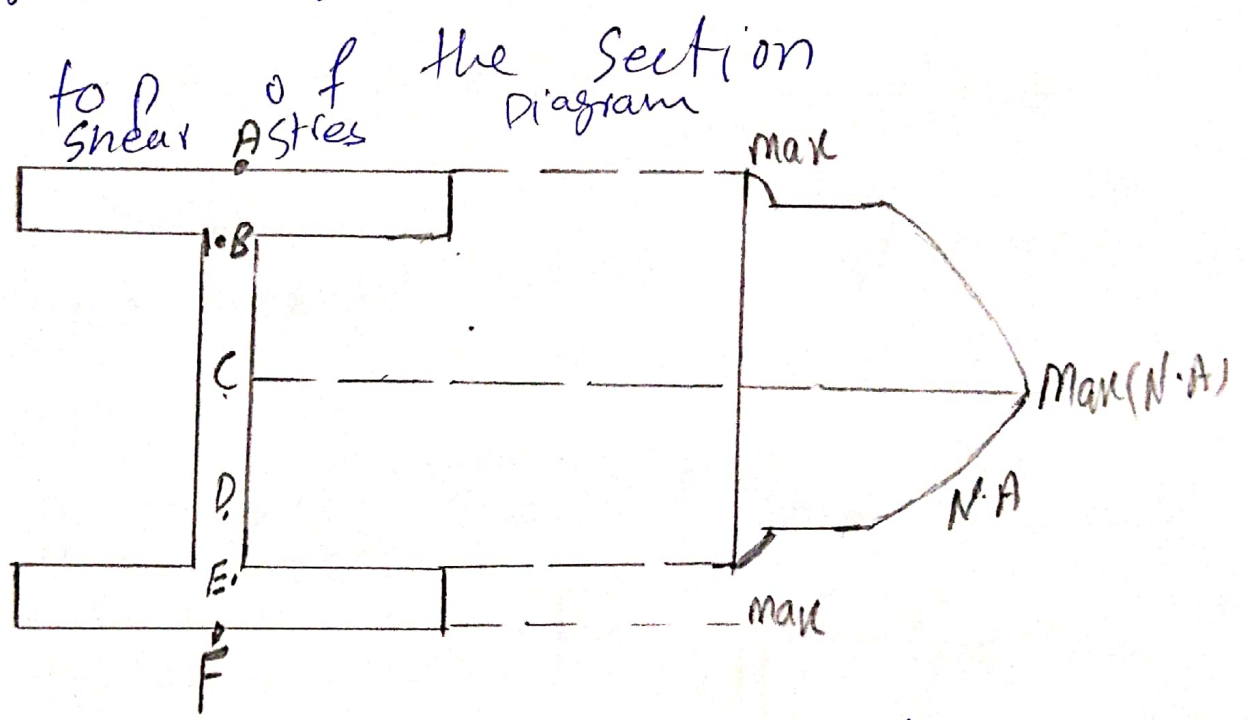


$$\tau = \frac{VQ}{Ib} = \frac{79.166 (4 \times 1 (3 - 0.5) + (1 \times 2) (2 - 1))}{67 \times 1}$$

$$= \frac{949.992}{67} = 14.1789 \text{ lb/in}^2$$

iv) Shear stress at point D and E will be the same because of the symmetry

Note: The maximum shear stress value occurs at the neutral axis and ~~the~~ minimum value at the



flexural stress determination

$$f = \frac{my}{I}$$

flexural stress at the top fiber point 'A'

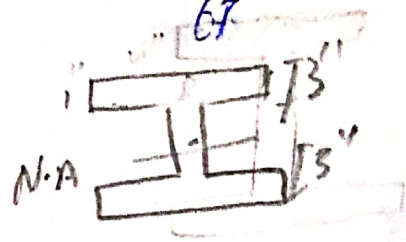
$$S =$$

$$= \frac{(463 \cdot 165)3}{67} = 1389.495 = S = 20.738 \frac{\text{lb}}{\text{in}^2}$$

ii) flexural stress at point 'B'

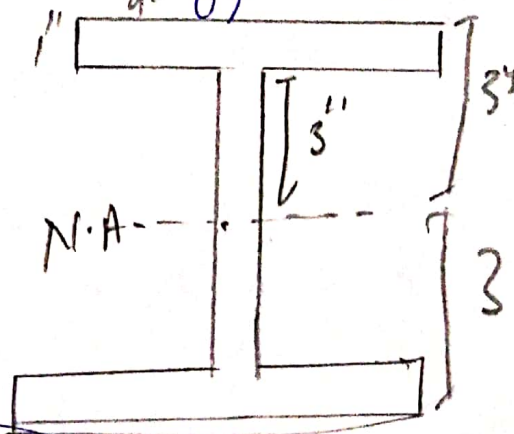
$$S = \frac{My}{I} = \frac{463 \cdot 165 \times (3 - 0.5)}{67} = \frac{11.67 \cdot 912}{67}$$

$$S = 17.43 \frac{\text{lb}}{\text{in}^2}$$



iii) flexural stress at point 'C'

$$S = \frac{463 \cdot 165 \times (3 - 1)}{67} = \frac{926.33}{67} = 13.825 \frac{\text{lb}}{\text{in}^2}$$

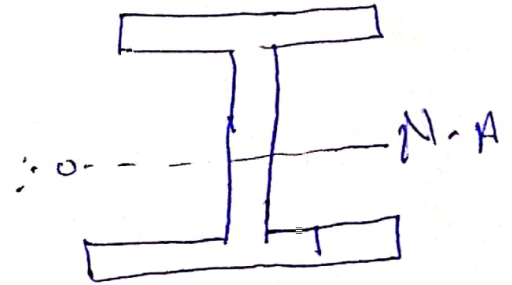


$$S = 13.825 \frac{\text{lb}}{\text{in}^2}$$

iv.) flexural stress $\neq 0$ ~~Neutral~~ Neutral axis (N.A)

$$S = \frac{my}{I}$$

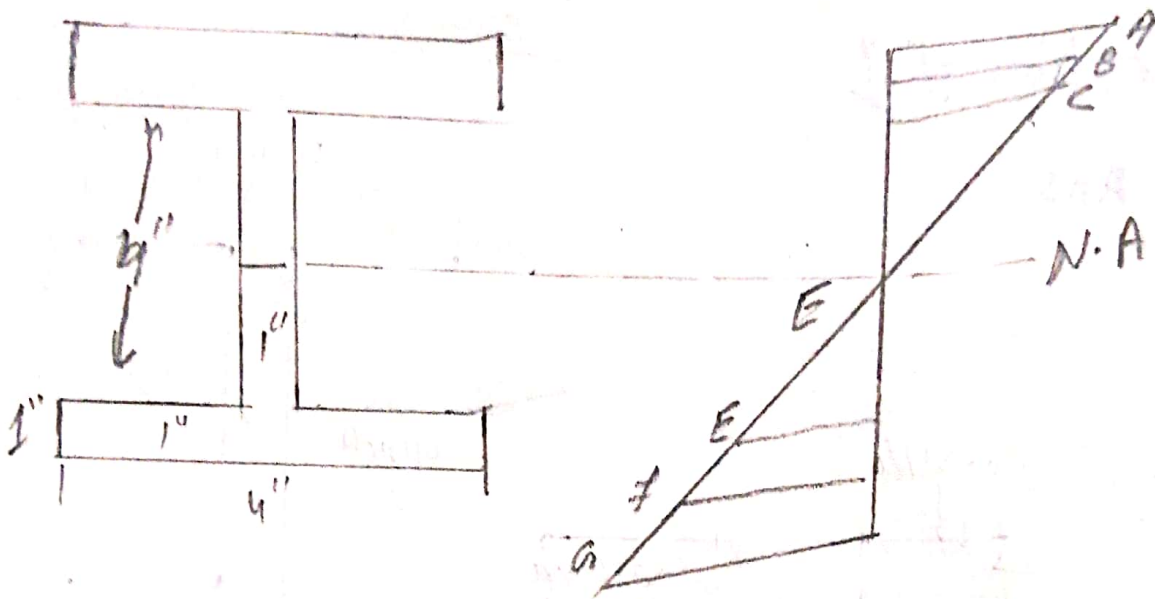
$$S = \frac{463 \cdot 165(0)}{67} = 0.16 \text{ lb/in}^2$$



flexural stress value at point E-F and G remain the same because of symmetry the upper

portion Above the N.A. Shows Tension and below the N.A. show compressive

Note: the flexural stress value is maximum at ~~centre~~ extreme top and bottom fiber at zero and N.A.



\Rightarrow Stress state =

Find stress state of a point element located 3ft from left support and 1inch below from top fiber

flexural stress at point 'C'

$$\sigma = 13.826 \text{ Psi}$$

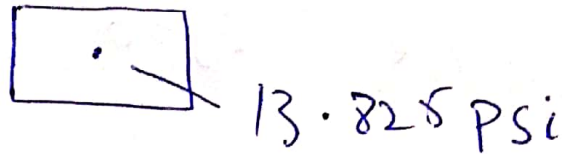
shear stress at point C

$$\tau = 14.178 \text{ Psi}$$

considered point "C" is a

planned element

$$\boxed{\sigma \rightarrow \text{sign}}$$

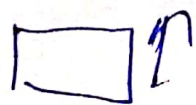


As the flexural stress σ is perpendicular to the cross section can be represented normal stress

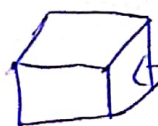
$T = 14.178$ PSI is compressive because point "C" lies in compression zone of beam cross section



If the point C lies below the centroid then stress would be tensile



$$T = 14.179 \text{ PSI}$$



$$T = 14.179 \text{ PSI}$$

$$\sigma = 13.825 \text{ PSI}$$

Combine stress on 2D element

we have also find

$$\sigma_x = 13.825$$

$$\sigma_y = 0$$

$$\tau_{xy} = 14.179$$

principle of stress eqn

$$\sigma_{x,y} = \frac{\sigma_x + \sigma_y}{2} \pm \sqrt{\left(\frac{\sigma_x - \sigma_y}{2}\right)^2 + \tau_{xy}^2}$$

$$\sigma_x = \frac{-13.825 + 0}{2} \pm \sqrt{\left(\frac{13.825 - 0}{2}\right)^2 + 14.179^2}$$

$$\sigma_{x,y} = -6.912 \pm \sqrt{\frac{191.130}{4} + (14.179)^2}$$

$$= -6.912 \pm \sqrt{47.78 + (14.179)^2}$$

$$= -6.912 \pm \sqrt{248.824}$$

$$= -6.912 \pm 15.77$$

(18)

$$\delta x = -6.912 - 15.77 = -22.682$$

$$\delta x = -6.912 + 15.77 = 8.858$$

First find $\theta p = ?$

$$\tan 2\theta p = \frac{\delta x y}{\frac{\delta x - \delta y}{2}}$$

$$\tan 2\theta p = \frac{14 \cdot 179}{\frac{-13.825}{2}}$$

$$\tan 2\theta p = \frac{14 \cdot 179}{-6.912}$$

$$\tan 2\theta p = -2.051$$

$$2\theta p = \tan^{-1}(-2.051)$$

$$2\theta p = -64.007$$

Divide of both sides

$$\theta p = \frac{-64.007}{2}$$

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$$OP = -32.003$$

put in General Equation

$$f_{max} = \frac{-13.825 + 0}{2} - \frac{13.825 + 0}{2}$$

$$\cos(-32.003) + 14.179 \sin(-32.003)$$

$$f_{max} = -6.912 = -6.912 + 0.437 \cdot 12.74$$

$$f_{max} = -26.36$$

Max in plane shear stress
in this case

$$\tan 2\theta_s = - \frac{(\sigma_x - \sigma_y)}{2\tau_{xy}}$$

$$\tan 2\theta_s = - \frac{(-13.825 - 0)}{2 \cdot 14.825}$$

$$\tan 2\theta_s = \frac{13.825}{2 \cdot 14.825}$$

$$\tan 2\theta_s = \frac{6.912}{14.82}$$

$$\tan 2\theta_s = 0.466$$

$$2\theta_s = \tan^{-1}(0.466)$$

$$2\theta_s = 24.98$$

$$\theta_s = 12.49$$

Divid 2 on both
sides

$$\theta_s = 12.49$$

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Put in the General
sol equation

$$r(x, y) = \left[\frac{\delta x - \delta y}{2} \right] \sin 2(12.49) + 14.179$$

$$r(x, y) = \left[\frac{\delta x - \delta y}{2} \right] \sin 2\theta + \delta xy \cos 2\theta$$

$$r(x, y) = \left[\frac{-13.825}{2} \right] \sin 2(12.49) + \cos 2(12.42)$$

$$r(x, y) = \left(\frac{13.825}{2} \right) \sin(24.98) + \cos(24.98)$$

$$r(x, y) = 6.912(0.422) + 14.179(0.904)$$

$$r(x, y) = 2.91 + 12.85$$

$$r(x, y) = 15.76$$

To Draw Mohr's circle

Centre Co-ordinate

$$(h, k) = \left(\frac{\delta x + \delta y}{2}, 0 \right)$$

$$\Rightarrow \left(\frac{-13.825 + 10}{2}, 0 \right)$$

$$(h, k) = \Rightarrow (-6.912, 0)$$

Radius of Mohr's circle

$$r = \sqrt{\left(\frac{\delta x - \delta y}{2} \right)^2 + (z \cdot xy)}$$

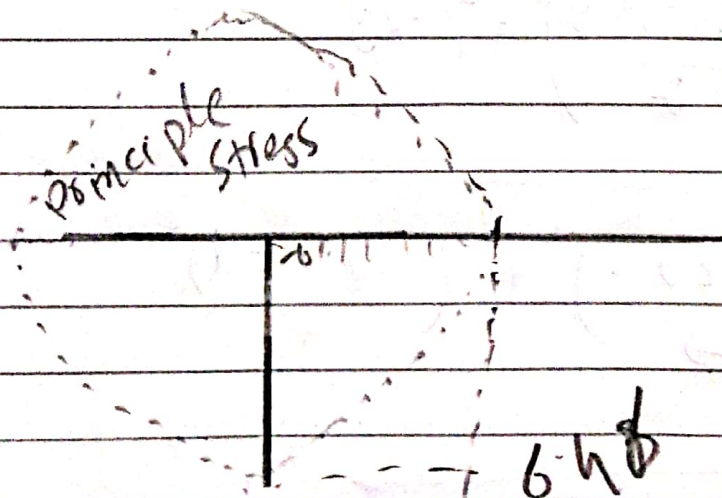
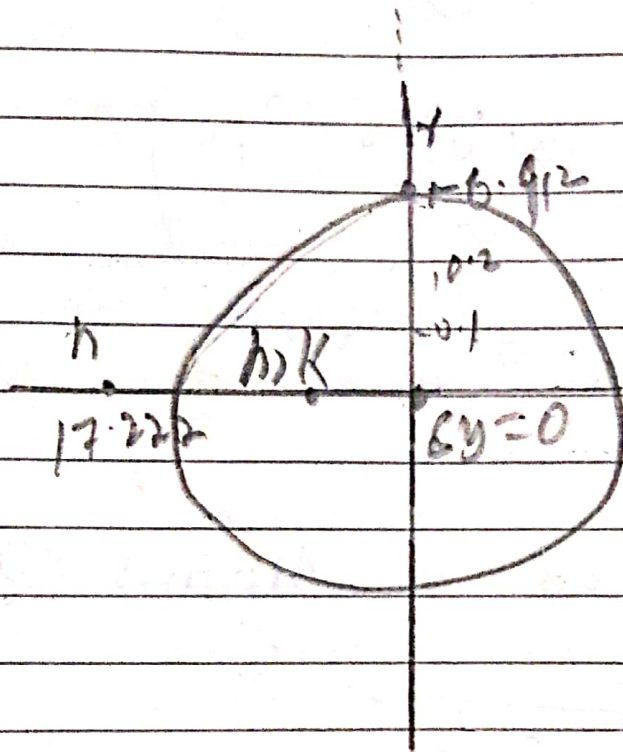
$$= \sqrt{\left(\frac{-13.825}{2} \right)^2 + (14.179)^2}$$

$$= \sqrt{\frac{191.13}{4} + 201.04}$$

$$= \sqrt{47.78 + 201}$$

$$= \sqrt{296.009}$$

$$\sigma = 17.222$$



$$\sigma = \sigma_{xy}$$