

7722 Mid term Examination Summer 2020 (1)

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Subject : Steel Structure.

QNO# 01?

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General Statement of Design Philosophies:

A general Statement assuming Safety in Engineering design.

Resistance (of material & X-section) \geq

Effect of applied load $\text{---} 1$

In eq (1) it is Essential that both design sides are evaluated for same condition (e.g.) if effect of load is to produce compressive stress on soil,

then it should be compared with bearing capacity of soil.

* When particular loading reaches its limit, failure is the assumed result, i.e. \rightarrow the loading condition become failure modes, such a condition is referred to as limit state and it can be define as

* "A limit state is a condition beyond which a structural system or a structural component cease to fulfill the function for

which it is designed".

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Example of limit state for structure with
of order includes:

- ① Deflection
- ② Cracking
- ③ Fatigue
- ④ Flexure
- ⑤ Shear
- ⑥ Torsion
- ⑦ Buckling
- ⑧ Settlement
- ⑨ Bearing
- ⑩ Stability.

ASD
Safety in design is obtained by specifying that the effect of the load should produce stress that is a fraction of the yield stress " f_y " say one half.

$$\begin{aligned} \text{FOS} &= \text{Resistance } R / \text{effect of load } Q \\ &= f_y / 0.5 f_y \\ &= 2 \end{aligned}$$

* Mathematical description of ASD

$$\frac{\phi R_n}{\gamma} \geq \sum Q_i$$

ASD :- combined dead load and live load treats them in the same way.

ASD merit: ① Elastic analysis for load become compatible for design.

② Experience Engineering are used to this method. 114

③ In past it was the only method for design purpose.

④ this method is included in AISC-05 Specifications as an alternate method.

Demerits ASD

- ① latest Research and literature is very limited
- ② Same factor of Safety is used for different load.
- ③ Failure mode is not directly predicted
- ④ the failure mode can not be observed.

LRFD
⇒ Safety in the design is obtained by specifying that the reduced nominal strength of a design structure is less than the effect of factor load acting on the structure

$$\phi R_n \geq n \leq \gamma Q_p$$

LRFD: LRFD is more rational

as different factor of safety can be assigned to different loadings such as Dead load, live load, Earthquake load and Impact loads.

LRFD merits

- ① LRFD accounts for both variability in resistance and load
- ② It achieved fairly uniform factor of safety for different limit state
- ③ It provides a rational and consistent method design.

LRFD Demerits

- ① it is disadvantages is change in design philosophy from various method.
- ② It required an understanding of the basic concept of probability and statistics
- ③ It required availability of sufficient statistical data and probabilistic design algorithms to make adjustment in resistance factor to meet individual situation.

Q. NO#02 Types of bolt connection in Steel Structure

① Slip-critical connection → Connection transmit the force by friction produced between the faying surface by the clamping action of the bolt.

↳ Slip-critical connections are recommended for joints to stress reversal, severe stress fluctuation, impact, vibration or where slip is objectionable.

② Bearing type connection load is transmitted by shearing and bearing on the bolt.

Capacity in shear depends on whether shear plane intersects the body of the bolt or threaded portion.

In the bearing type connection in which the load is resisted by the bolt body without any friction between faying surface.

Failure in bolt connection

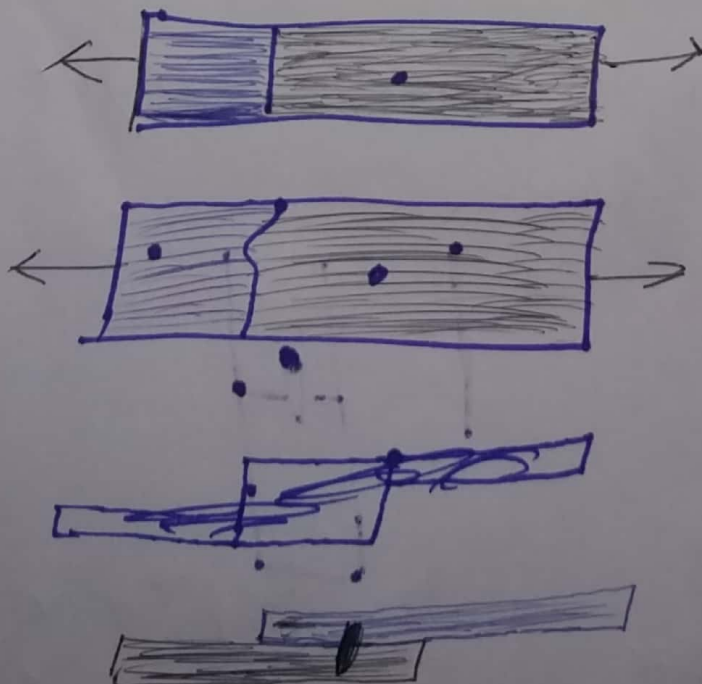
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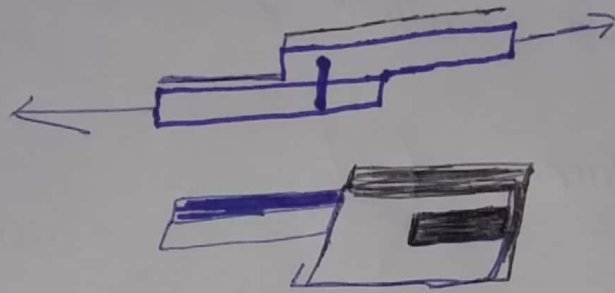
- ① ~~Shearing failure of bolt.~~
- ② ~~Bearing failure of plate bolt.~~
- ~~③ Tearing failure of edge of plate.~~

- ① Shear failure of bolt
- ② Bearing failure of bolt
- ③ Tension failure of bolt.

① Bearing failure of bolt if the connected plates are made of high strength steel than failure of bolt can take place by bearing of the plates on the bolt.



② Shearing failure of bolt = failure of member being connected due to fracture or or block shear - edge-tearing or fracture of the connected plate of between two bolt holes. (8)



③ Tension failure of bolt = tension failure of bolt connection to elongate to surface from each other that provides clamping force of a joint when torque measure of the twisting force.



Transverse tension failure



Shearing failure edge of plate -

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Given data: D.L = 130 K.

L.L = 265 K

C10 X 30

gusset plate thickness 1 inch

Bolt dia = $\frac{3}{4}$ inch

A-325 - A-36 steel.

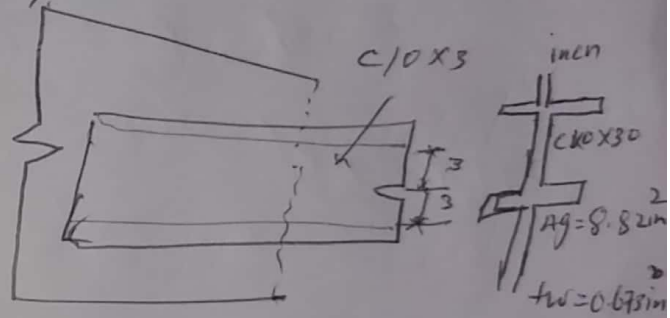
three bolts lines.

Required? no of bolts = ?

Using ASD = ?

Solⁿ:

Solⁿ →



① Finding total service load = D.L + L.L

$$= 130 + 265 = \boxed{395 \text{ Kips}}$$

② Bolts Design: for $\frac{3}{4}$ dia.

$A_{req} = 0.4418 \text{ in}^2$ (nominal area)

$F_v = 30 \text{ Ksi}$ (Shear strength of bolt in single shear table 2-11)

$$R_v = 0.4418 \times 30$$

$$R_v = 13.25 \text{ kips / shear surface}$$

↳ resistance effect by single shear.

As there are two shear surface per 10 bolt.

$$\text{No of bolt} = \frac{395}{2 \times 13.25} = 14.90 \approx \boxed{15 \text{ bolt}}$$

③ Bearing: $F_p = 1.2 f_u$

$$F_p = 1.2 \times 58$$

$$\boxed{F_p = 69.6 \text{ ksi}}$$

$$\Rightarrow L_e = 1 \frac{1}{2} d$$

$$L_e = 3d \quad (\text{table 2-9})$$

Channel

$$R_p = d + F_p = \frac{3}{4} \times 0.673 \times 69.6$$

$$R_p = 35.13 \text{ Kips (single bearing surface of channel)}$$

For bolt there are 30 bearing surface

So;

$$\text{Capacity} = 30 \times 35.13$$

$$= 1053.9 \Rightarrow 395 \text{ Kips}$$

Gusset plate

$$R_p = d + F_p$$

$$R_p = \frac{3}{4} \times 1 \times 69.6$$

$$\boxed{R_p = 52.2 \text{ Kips}}$$

single bearing surface of gusset plate.

For gusset plate these are 15 bearing surface

$$\begin{aligned} \text{Capacity} &= 15 \times 52.2 \\ &= 783 > 395 \text{ kips} \end{aligned}$$

OK

④ spacing
= End distance Shear edge = $1\frac{1}{4}$ minimum

$$\text{End distance} = 1\frac{1}{2}d = 1.13 \text{ in} \leq 1\frac{1}{4} \text{ in} \left[\begin{array}{l} \text{table 2-8} \\ 2-9 \end{array} \right]$$

$$\text{Center to center distance} = 3d = 2\frac{1}{4} \text{ in}$$

→ As we can see that R_p for both channel and gusset plate is considerably greater than required consider minimum end distance of $1\frac{1}{4}$ in and the minimum between connection spacing of 2 in

$$l_e = \frac{2P}{f_u t} = 1.25 \left[\begin{array}{l} t = 0.673 \\ \text{table 1-5 AISI manual} \end{array} \right]$$

$$\frac{2P}{58 \times 0.673} = 1.25$$

$$P = 24.4 \text{ kips}$$

P10

$$L = \frac{2P}{f_{ut}} + \frac{d}{2}$$

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$$2 = \frac{2P}{58 \times 0.673} + \frac{3/4}{2}$$

$$P = 31.7 \text{ kips}$$

$$\text{Capacity} = 2(3 \times (24.4) + 12(31.7))$$

$$\text{Capacity} = 907.2 > 395 \text{ kips OK}$$

gusset plate

$$1e = \frac{2P}{f_{ut}} = 1.25 = 2$$

$$\frac{2P}{58 \times 1}$$

$$P = 36.25 \text{ kips}$$

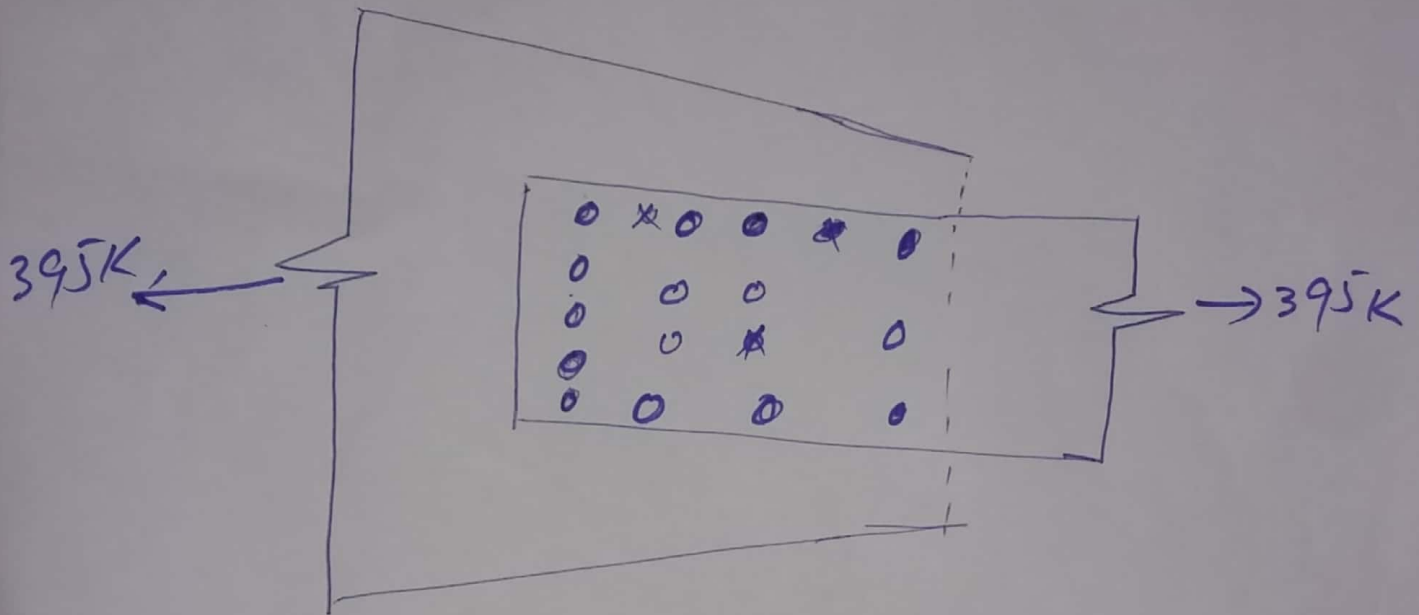
$$L = \frac{2P}{f_{ut}} + \frac{d}{2} \Rightarrow 2 = \frac{2P}{58 \times 1} + \frac{3/4}{2}$$

$$P = 47.13 \text{ kips}$$

$$\text{Capacity} = (3 \times (36.25) + 12(47.13))$$

$$\text{Capacity} = 674.31 > 395 \text{ kips}$$

~~So~~ So use 15 bolt in 3 rows $\frac{13}{4}$
 of five with End distance $1\frac{1}{4}$ in
 and center to center distance
 Spacing of 2 in



$$= \frac{7722}{\cdot}$$