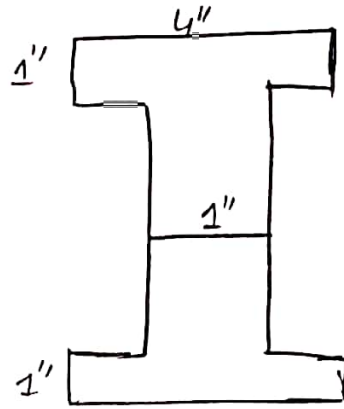
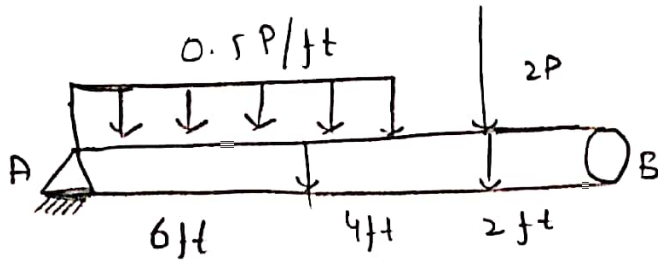


# Question

Construct the Mohr's circle diagram and find the principle stress and maximum in plane shear stress - for the stress state of point c located at the centre of ODL and 1 inch below the top fibre of beam cross section shown in figure.

How ever to construct Mohr's circle it is necessary to draw the shear stress and flexure stress variation diagram for maximum shear force and bending moment respectively - compare the results obtained from the Mohr's circle with the stress transformation equation

$$P=2$$



$P =$  last 2 digits of ID  
that is  $P = 39$

### Solution:-

~~use~~ we have to find

- Reactions
- Shear force
- Bending moment diagram

$$\sum F_y = 0 \quad \text{Upward positive}$$

$$\Rightarrow R_A + R_B - (0.5 \times 39 \times 6) - 2(39) = 0$$

$$R_A + R_B - 117 - 78 = 0$$

$$R_A + R_B = 39 \quad \text{--- (A)}$$

Now  $\sum M_A = 0$  ↺ anticlockwise

$$(R_A \times 12) - (78 \times 10) - (117 \times 3) = 0$$

$$R_A \times 12 - 780 - 351 = 0$$

$$\frac{R_A \times 12}{12} = \frac{1131}{12}$$

$$R_A = 94.25$$

$$P = 3$$

So put the value of  $R_B$  in eq (A)

$$\text{eq (A)} \Rightarrow R_B + 94.25 = 39$$

$$R_B = 94.25 - 39$$

$$R_B = 55.25$$

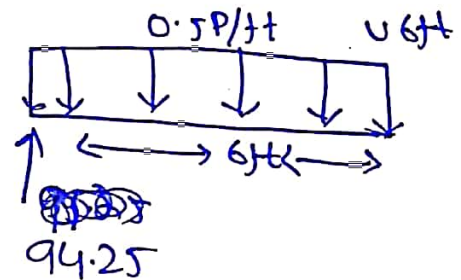
Shear force :- first where we have to find the shear force at 6ft from left support.

$$\sum f_y = 0$$

$$\Rightarrow -0.5P/ft + 94.25 - 117 = 0$$

$$\Rightarrow -0.5P/ft = 101.75$$

$$V_{6ft} = -101.75$$



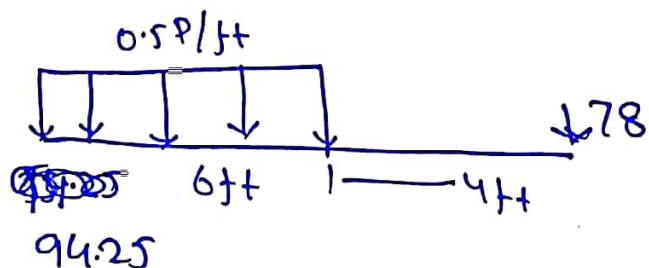
Now we have to find shear stress at 10ft from left support.

$$\sum f_y = 0$$

$$55.25 - 117 - 78 - V_{10ft} = 0$$

$$-V_{10ft} = +139.75$$

$$V_{10ft} = -139.75$$



$$P=4$$

Bending moment :-  
 $\overbrace{x} \quad \underbrace{x}$

$$\sum M_{6ft} = -(94.25 \times 0.5 \times 6) + (39 \times 6) \left(\frac{6}{3}\right)$$

$$\sum M_{6ft} = -282.75 + 468$$

$$\boxed{= 185.25}$$

Now we have to find moment at 3ft

$$\sum M_{3ft} = -(94.25 \times 3) + (39 \times 6 \times 3)$$

$$\Rightarrow \sum M_{3ft} = -(282.75 + 702)$$

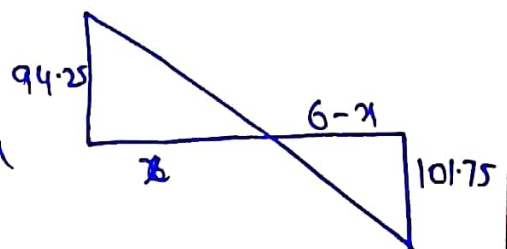
$$\boxed{\sum M_{3ft} = 419.25}$$

Now we have to find moment at changing point

$$\frac{94.25}{x} = \frac{101.75}{6-x}$$

$$\Rightarrow \text{~~101.75~~}$$

$$94.25 \times (6-x) = 101.75x$$



$$P=5$$

$$\Rightarrow 565.5 - 94.25x = 101.75x$$

$$\Rightarrow 565.5 = 101.75x + 94.25x$$

$$\Rightarrow \frac{565.5}{196} = \frac{196x}{196}$$

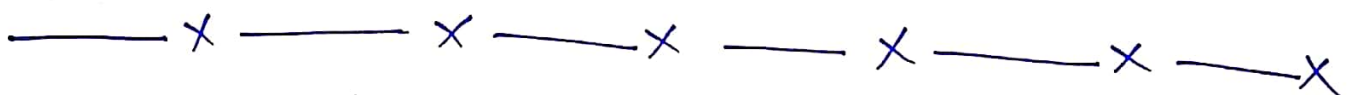
$$x = 2.88 \text{ ft}$$

$$\Sigma M_{2.88 \text{ ft}} = 0$$

$$\Rightarrow M_{2.88 \text{ ft}} - (94.25 \times 2.88) + (39 \times 6 \times \frac{2.88}{2}) = 0$$

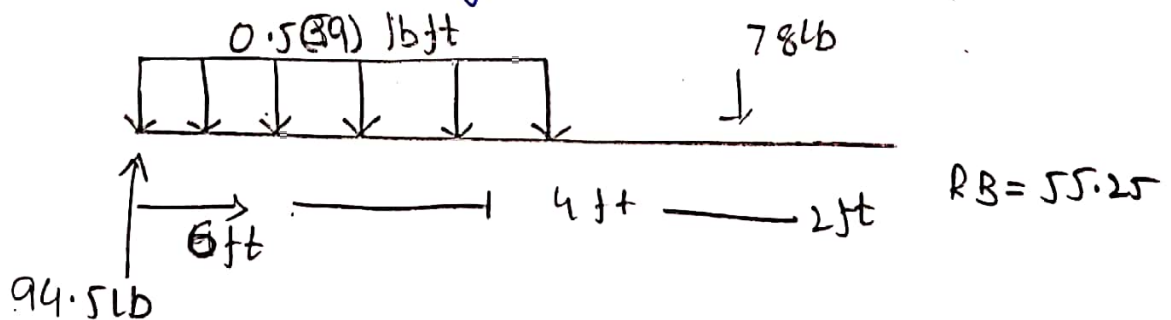
$$M_{2.88 \text{ ft}} = -(271.44) + (47.64) = 0$$

$$M_{2.88 \text{ ft}} = 319.08 \text{ lbft}$$

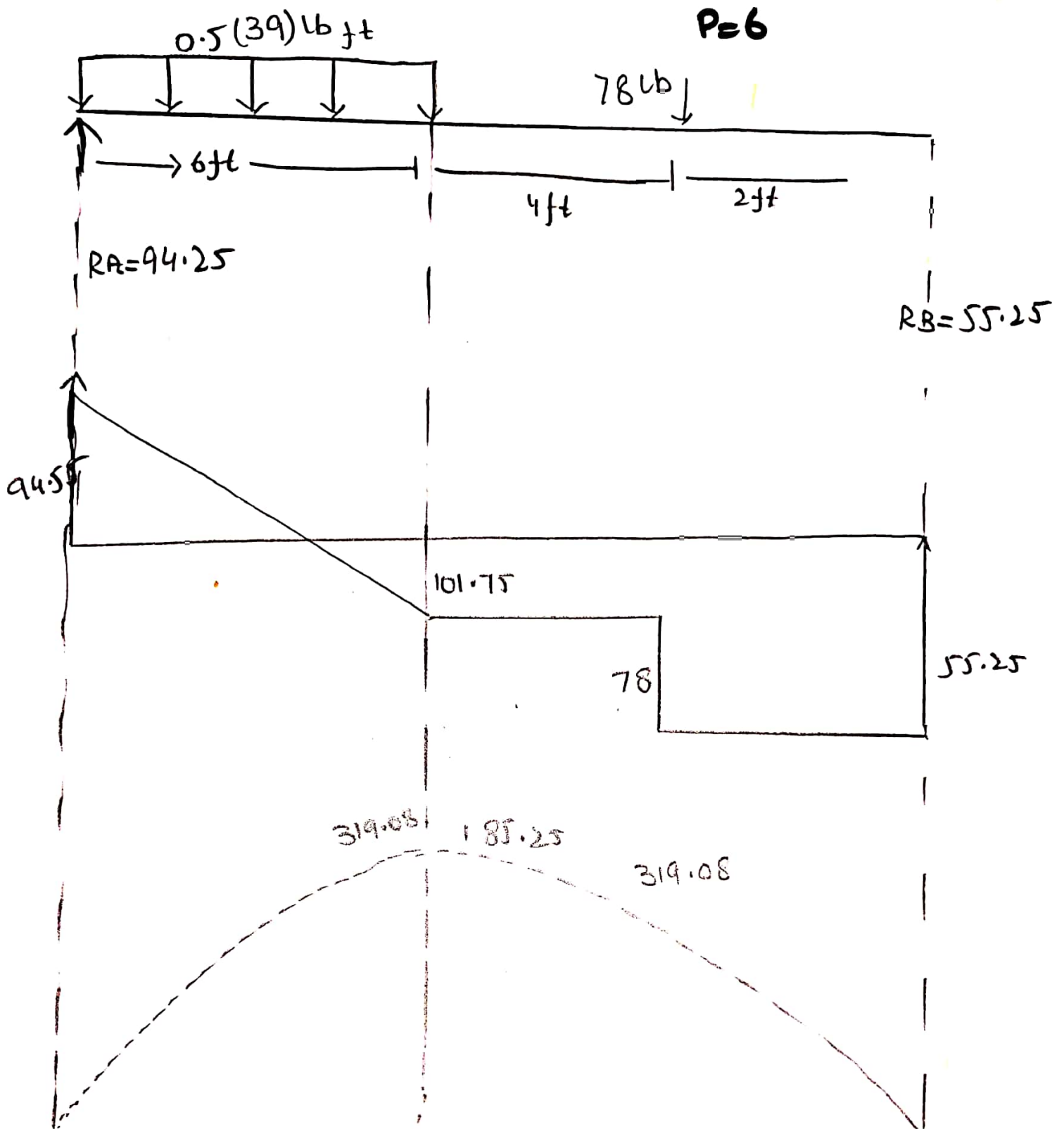


Shear force and Bending

moment diagram

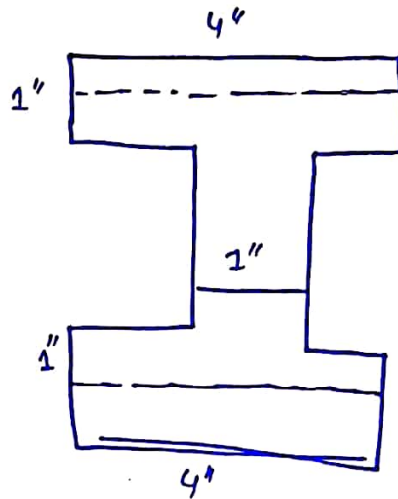






Part B:-

Now we have to find moment of inertia of Beam cross section



$$y_1 = 5.5$$

$$y_2 = 3$$

$$y_3 = 0.5$$

$$A_1 = 4 \text{ inch}^2$$

$$A_2 = 4 \text{ inch}^2$$

$$A_3 = 4 \text{ inch}^2$$

$$\bar{y} = \frac{(A_1 y_1) + (A_2 y_2) + (A_3 y_3)}{A_1 + A_2 + A_3}$$

Now putting values

$$\Rightarrow \bar{y} = \frac{(4 \times 5.5) + (4 \times 3) + (4 \times 0.5)}{4 + 4 + 4}$$

$$\Rightarrow \boxed{\bar{y} = 3''}$$

Now

$$I_1 = \frac{bh^3}{12}$$

$$I_1 = \frac{4 \times 1^3}{12} \Rightarrow$$

$$I_1 = 0.33 \text{ inch}^4$$

$$I_2 = \frac{bh^3}{12}$$

$$I_2 = \frac{1 \times 4^3}{12} \Rightarrow$$

$$I_2 = 5.33 \text{ inch}^4$$

$$I_3 = \frac{bh^3}{12}$$

$$I_3 = \frac{4 \times 1^3}{12} \Rightarrow$$

$$I_3 = 0.33 \text{ inch}^4$$

Now

"d"

$$d_1 = \bar{y} - y_1$$

$$\Rightarrow d_1 = 3 - 5.5 = -2.5$$

$$\Rightarrow d_2 = \bar{y} - y_2$$

$$\Rightarrow d_2 = 3 - 3$$

$$d_2 = 0$$

$$d_3 = \bar{y} - y_3 = 2.5$$

Ad<sup>2</sup>

$$A_1 d_1^2 = 4 \times (-2.5)^2$$

$$= 25 \text{ inch}^4$$

$$A_2 d_2^2 =$$

$$4 \times (0)^2$$

$$= 0$$

$$A_3 d_3^3 = 25 \text{ inch}^4$$



P=9

Now :-

$$I_{1x} = I_1 + A_1 d_1^2$$

$$\Rightarrow I_{1x} = 0.33 + 25$$

$$I_{1x} = 25.33 \text{ inch}^4$$

$$I_{2x} = I_2 + A_2 d_2^2$$

$$I_{2x} = 0 + 5.33$$

$$I_{2x} = 5.33 \text{ inch}^4$$

$$I_{3x} = I_3 + A_3 d_3^2$$

$$I_{3x} = 0.33 + 25$$

$$\Rightarrow I_{3x} = 25.33 \text{ inch}^4$$

Now  $I_{xx} = I_{1x} + I_{2x} + I_{3x}$

$$I_{xx} = 25.33 + 5.33 + 25.33$$

$$I_{xx} = 55.99 \cong 56 \text{ inch}^4$$

## Part 'c'

- ⇒ we have to find
- Shear Stress
  - flexure Stress
  - variation diagram

Shear stress :- Case ⇒ 1

so we have to find the shear stress at top fibre

we know that

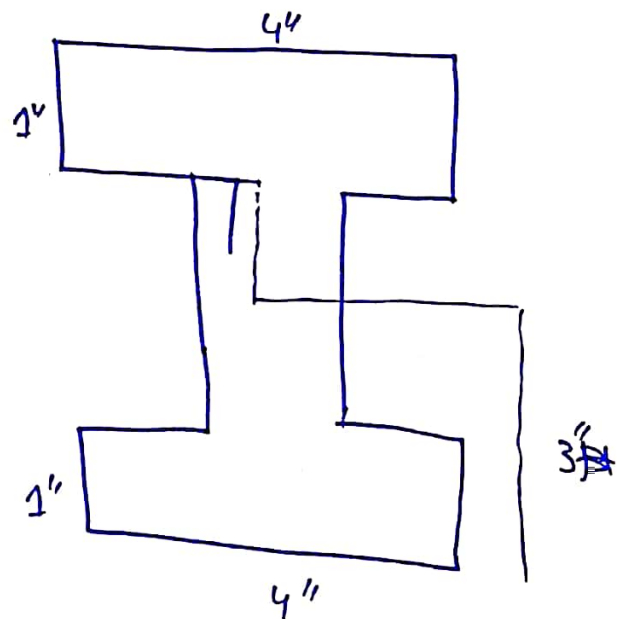
$$\tau = \frac{VQ}{It}$$

As top fibre  $A=0$

$$Q = \bar{y} A \quad \therefore \bar{y} = 3''$$

$$\tau = \frac{55.25 \times 0}{56 \times 4}$$

$$\tau = 0$$



~~55.25~~  
~~56~~  
 $V = 55.25 \quad I = 56 \quad b = 4$

Case # 2

find stress 1 inch below  
the top fibre but here  
two cases

$$y = 2 + \frac{1}{2} = 2.5$$

$$A = 1 \times 4 = 4$$

$$\Rightarrow \frac{(55.25)(10)}{56 \times 4}$$

$$Q_A = yA$$

$$\Rightarrow Q_A = 2.5 \times 4 = 10$$

$$\Rightarrow \tau_A = 2.46 \text{ PSI}$$

$$\tau_B = VQ_B$$

$$\Rightarrow \tau_B = \frac{(55.25)(10)}{56 \times 1}$$

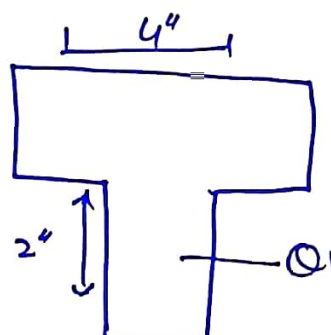
$$\Rightarrow \tau_B = 9.86 \text{ PSI}$$

Case # 3

find stress at centroid  
axis

Now here

$$Q = Q_1 + Q_2 \quad \text{--- } \textcircled{1}$$



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$$P=12$$

$$Q_1 = \bar{y}_1 A_1 = 2_{/2} (1 \times 2) = 2$$

$$Q_2 = 2.5 \times 4 = 10$$

So  $Q = 2 + 10$

$$Q = 12$$

Now  $\tau_{max} = \frac{VQ}{Ib}$

$$b = 1 \text{ inch}$$

$$\tau_{max} = \frac{55.25 \times 12}{56 \times 1}$$

$$\tau_{max} = 11.83 \text{ PSI}$$

### Case # 4

Find out shear stress 1 inch above the bottom fibre

Now again we have two cases

$$\tau_A = \frac{55.25 \times (2.5 \times 4)}{56 \times 1}$$

$$\tau_A = 9.86 \text{ PSI}$$

$$\tau_B = \frac{55.25 \times (2.5 \times 4)}{56 \times 4}$$

$$\tau_B = 2.46 \text{ Psi}$$

case # 5

find shear stress at

bottom fibre

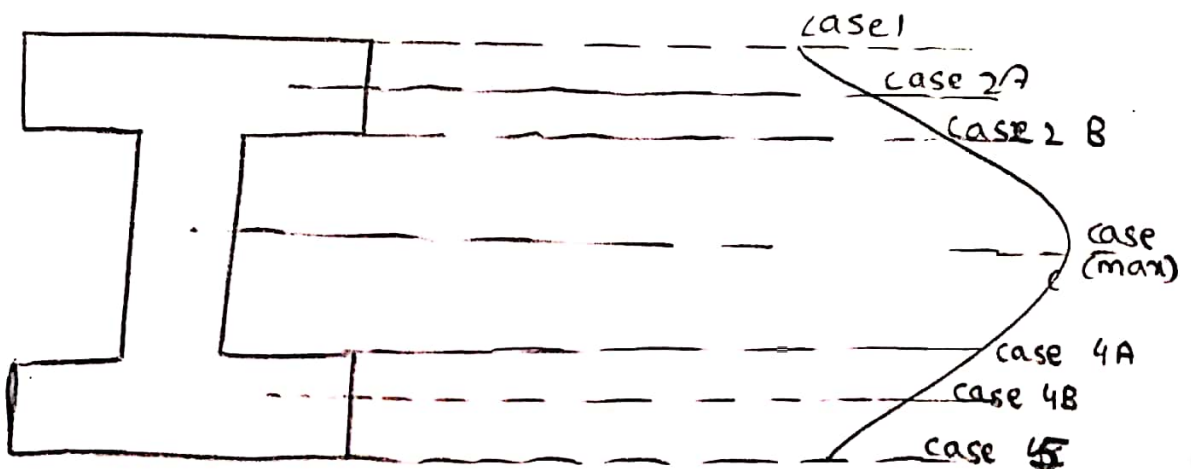
here  $\bar{y} = 0$  so  $Q = 4 \times 0 = 0$

$$\tau = \frac{VQ}{IB}$$

$$\Rightarrow \frac{55.25 \times 0}{56 \times 1} = 0$$

$$\tau = 0 \text{ Psi}$$

— x — x — x — x — x  
 Shear stress Variation diagram





Case #6

Now we have to find maximum shear stress at a distance of 6ft from left support of beam along its length.

As we know that shear force at 6ft is

$$V = 101.75 \text{ lb}$$

$$\tau_{\max} = \frac{VQ}{Ib} \Rightarrow \frac{101.75 \times 12}{56 \times 1} = \tau$$

$$\tau_{\max} \Rightarrow 21.80 \text{ psi}$$

Case #7

Now we have to find Shear stress at a distance of 6ft from left support and 4inch below the top fibre.

$$\tau = \frac{VQ}{Ib}$$

$$\Rightarrow \tau = \frac{101.75 \times 4}{56 \times 4} \Rightarrow$$

$$4.54 \text{ psi}$$

# Flexure stress analysis :-

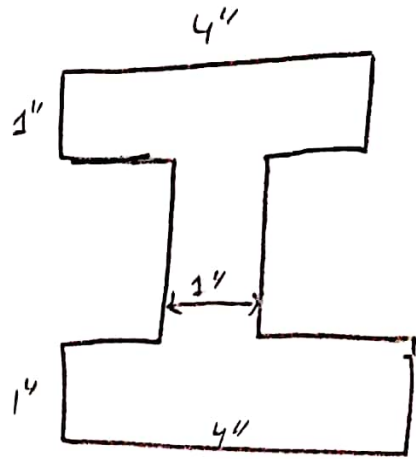
P=15

as we know that

$$\sigma = \frac{My}{I}$$

The maximum bending moment

is 185.25 psi



Case 1 find stress at top fibre

$$\sigma_{cp} = \frac{(185.25)(3)}{56}$$

$$= 9.92 \text{ PSI}$$

Case 2 find stress at 1 inch below top fiber

$$= \frac{(185.25)(2)}{56}$$

$$= 6.61 \text{ PSI}$$

$$P=16$$

case 3

find flexure stress at centroid axis

$$\sigma_{\text{cent}} = \frac{185.25 \times 0}{56} = \boxed{0 \text{ Psi}}$$

case 4

find flexure stress at 1 inch above the bottom fibre

$$\sigma = \frac{My}{I}$$

$$\Rightarrow \frac{185.25 \times 2}{56} = \boxed{6.61 \text{ Psi}}$$

case 5

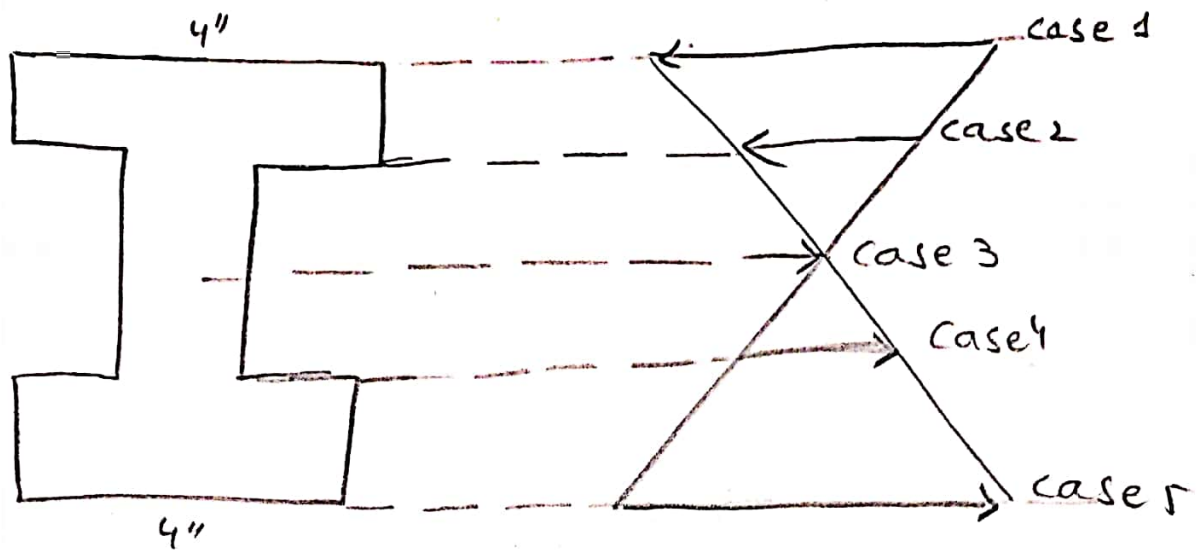
find flexure stress at bottom fiber

$$\sigma_{\text{bot}} = \frac{My}{I}$$

$$\sigma_{\text{Bot}} = \frac{185.25 \times 3}{56}$$

$$\sigma_{\text{Bot}} = \boxed{9.89 \text{ Psi}}$$

# flexure stress variation diagram



## stress state of a point element:-

Now we have to find stress state of a point element located at a distance of 3ft from left support and 1 inch below from the top fibre. As to the condition of stressed elements at point C in this given I section - It require to find all the section stresses at this point -

As in given problem the stresses acting on point C is flexural

and shear stresses - there is no torsional stress force acting on this beam - due to load symmetry along the beam axis (longitudinal axis)

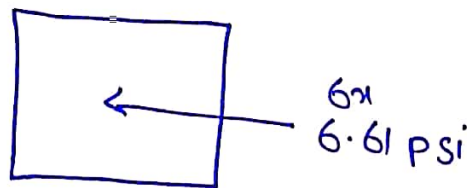
Flexure stress at point c

$$\sigma = 6.61 \text{ psi} \quad \text{Case \#2}$$

" shear stress at point c "

$$\tau = 4.54 \text{ psi} \quad \text{Case \#7}$$

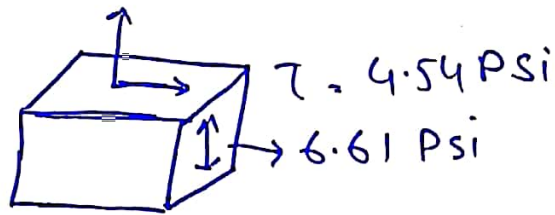
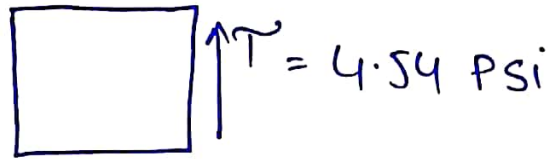
consider this point "c" is a planer element



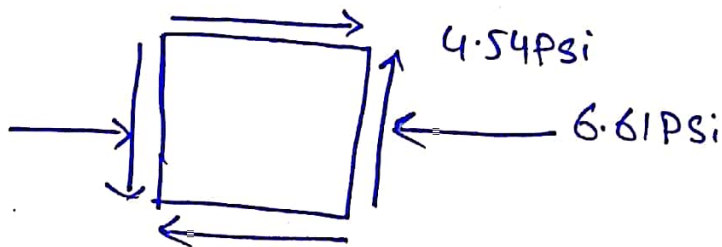
6.61 is a compressive because point "c" lies in compression zone of beam cross section

If the point c lies below the centroidal then stress would be tensile.





combine stress on 2D element



Part D :- we have to find

- Principle Stresses
- stresses transformation
- mohr's circle
- comparison of mohr's circle result with principle stress equation

$$P=20$$

Principle stresses:-

we have to

find  $\theta_p$

$$\tan 2\theta_p = \frac{\tau}{(6x - 6y) / 2}$$

$$\tan 2\theta_p = \frac{4.54}{(-6.61 - 0) / 2}$$

$$|\tan 2\theta_p| = -1.3736$$

$$2\theta_p = \tan^{-1}(-1.3736)$$

$$\frac{2\theta_p}{2} = \frac{53.54}{2} \quad \boxed{= -26.57}$$

Now for  $6_x$

$$6_x' = \frac{6x + 6y}{2} + \frac{6x - 6y}{2} \cos 2\theta_p + \tau \sin 2\theta_p$$

$$\Rightarrow 6_x' = -3.305 + 3.305 \cos 2(26.97) + 4.54 \times \sin 2(26.54)$$

$$\Rightarrow \boxed{6_x' = 18.47 \text{ psi}}$$

$$P=21$$

$$\sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos 2\theta - \tau_{xy} \sin 2\theta$$

$$\sigma_{y'} = \frac{(-6.61 + 0)}{2} - \frac{(-6.61 - 0)}{2} \cos 2(-4.552) -$$

$$(4.54 \times \sin 2(26.94))$$

$$\sigma_{y'} = -0.0977 \text{ Psi} \quad \text{Compression}$$

Shear plan

$$\tau_{x'y'} = \frac{\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta$$

$$\tau_{x'y'} = \frac{(-6.61 - 0)}{2} \sin 2(40.47) + (4.54 \cos 2) 40.47$$

$$\Rightarrow \tau_{x'y'} = 3.34$$

Stress transformation

Now find stress state condition

of point c at a clockwise

orientation  $\theta = -30^\circ$  (assumed)

$$\sigma_{x'} = \frac{\sigma_x + \sigma_y}{2} + \frac{\sigma_x - \sigma_y}{2} \cos 2\theta + \tau_{xy} \sin 2\theta$$

$$\Rightarrow \sigma_{y'} = \frac{(6 \cdot 61 + 0)}{2} - \frac{(-6 \cdot 61 - 0)}{2} \cos 2(-30) - 4 \cdot 54 \sin 2(-30)$$

$$\boxed{\sigma_{y'} \Rightarrow -8.268 \text{ psi} \text{ compression}}$$

$$\sigma_{y'} = \frac{\sigma_x + \sigma_y}{2} - \frac{\sigma_x - \sigma_y}{2} \cos 2\theta - \tau_{xy} \sin 2\theta$$

$$\Rightarrow \frac{-6 \cdot 61 + 0}{2} - \frac{(6 \cdot 61 - 0)}{2} \cos 2(-30) - 4 \cdot 54 \sin 2(-30)$$

$$\boxed{\sigma_{y'} = -4.45 \text{ psi} \text{ compression}}$$

$$\tau_{x'y'} = \frac{-\sigma_x - \sigma_y}{2} \sin 2\theta + \tau_{xy} \cos 2\theta$$

$$\Rightarrow \tau_{x'y'} = \frac{6 \cdot 61 - 0}{2} \sin 2(-30) + 4 \cdot 54 \cos 2(-30)$$

$$\Rightarrow \tau_{x'y'} = -6.9436 \text{ psi}$$

# Mohr's circle:-

coordinates

$$(h, k) = \left( \frac{6 \cdot 61}{2}, 0 \right)$$

$$(h, k) = (-3.34, 0)$$

$$(h, k) = (3.34, 0)$$

Radius

$$r = \sqrt{\left(\frac{6x - 6y}{2}\right)^2 + \tau_{xy}^2}$$

$$r = \sqrt{\frac{6 \cdot 61 - 0}{2} + (4.54)^2}$$

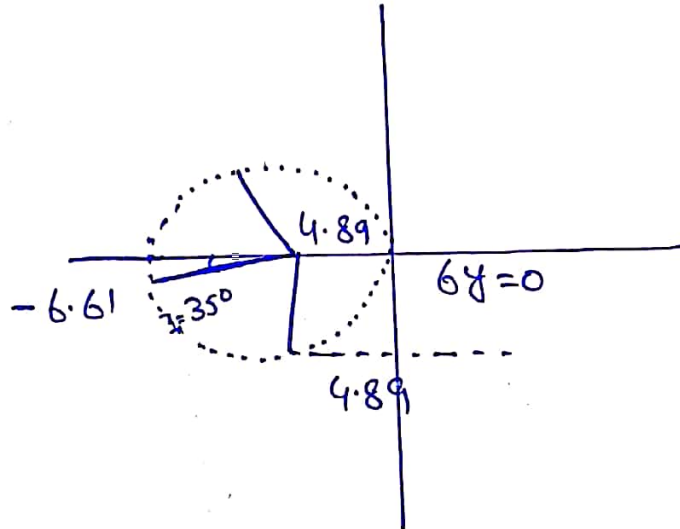
$$r = 4.89$$



$$P = 24$$

$$V = 6.61 \text{ PSI}$$

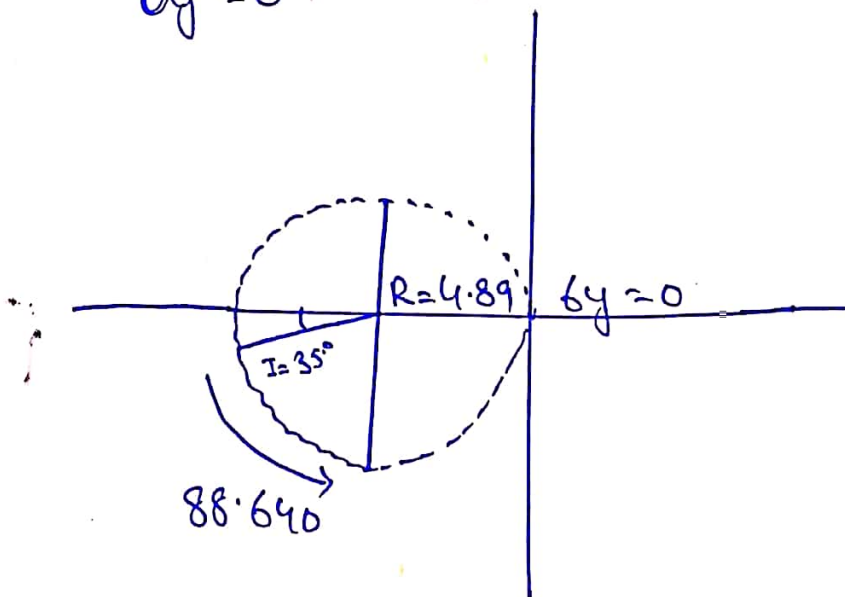
~~Scale~~ Scale :-  $2 \text{ PSI} = 1 \text{ cm}$



for principle stress:-

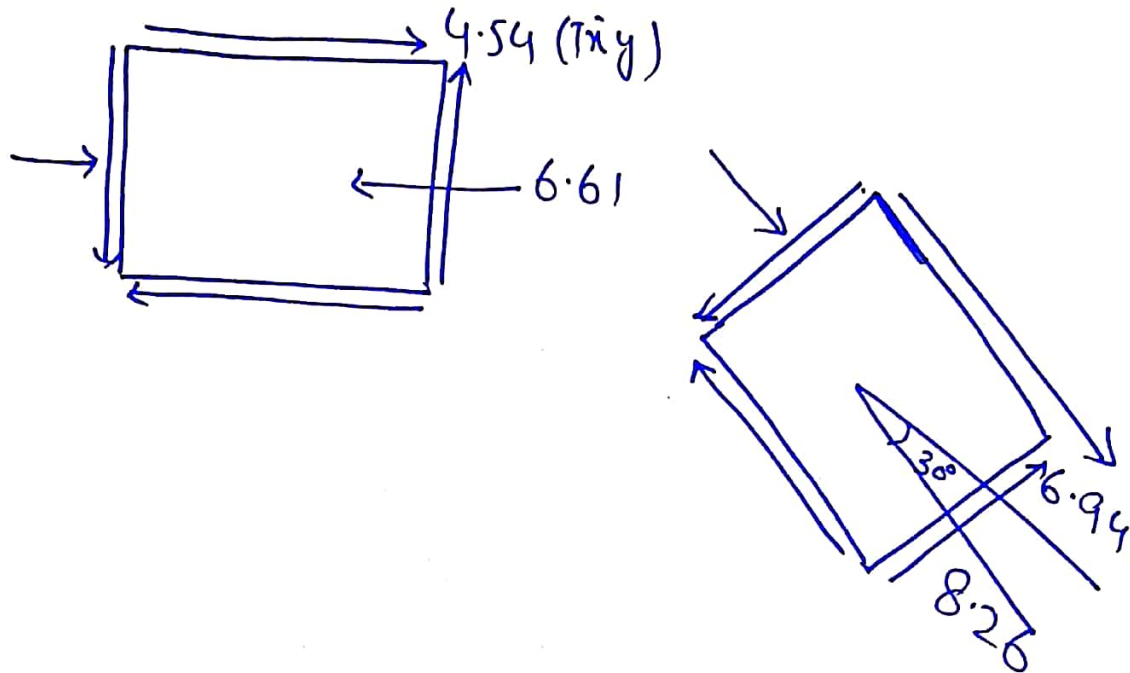
$$\sigma_x = -6.61$$

$$\sigma_y' = 0$$



$A=25$

# Comparison of Mohr's Circle with Shear Stress Transformation



Principle and plan Shear Stress

