

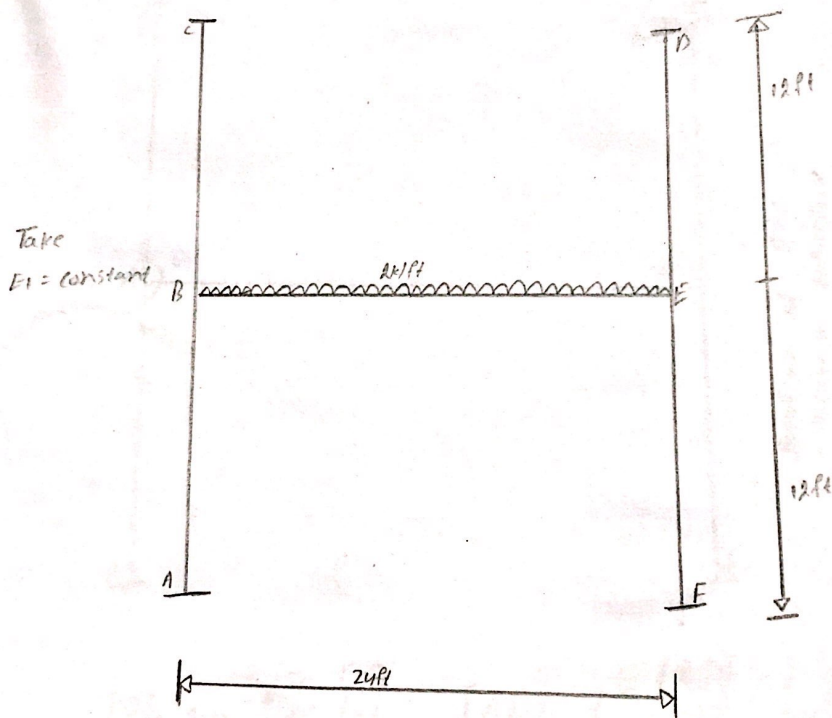
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Subject : Theory of structure II
Exam : Summer 2020
Semester : 8th B-tech
Instructor : Engr. Humaira Arshad

(page # 01)
Q.1: Analyze the given frame using stiffness method.

Take:

$EI = \text{constant}$

$k_1 = 2 \text{ degree}$ (neglecting the axial effect).

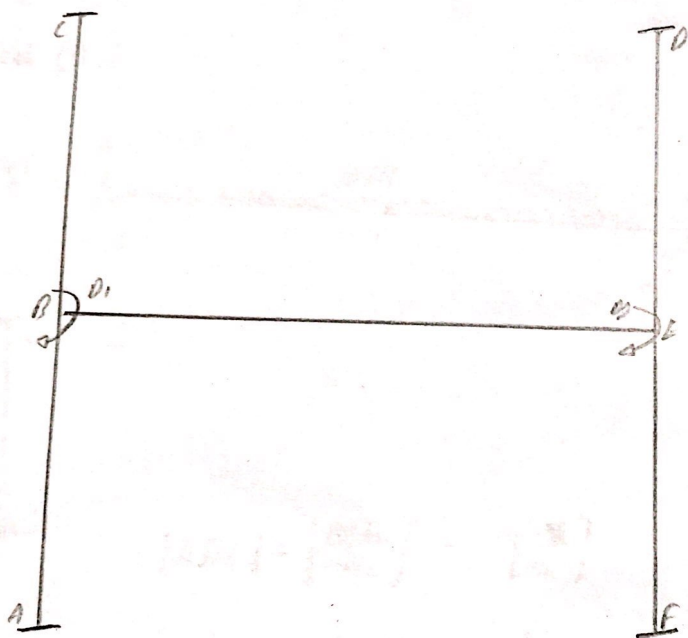


$k_1 = 2 \text{ degree}$ (neglecting the axial effects)

Solution:

(#02)

* step #01: Selection of redundant joint displacements and assign coordinates at those locations. Also compute AD values.



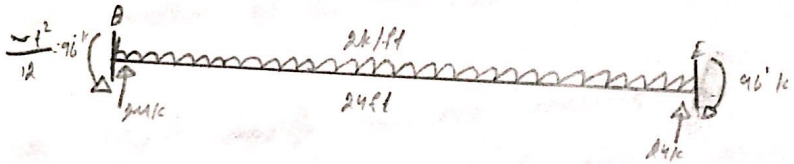
Rotation at B & D is taken as redundant joint displacement.

$$[D]_{2 \times 1} = \begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \begin{bmatrix} ? \\ ? \end{bmatrix}$$

$$[AD]_{2 \times 1} = \begin{bmatrix} AD_1 \\ AD_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

(#03)

step#02: Compute ADL matrix (fixed end actions)



$$[ADL] = \begin{bmatrix} ADL_1 \\ ADL_2 \end{bmatrix} = \begin{bmatrix} -96 \\ 96 \end{bmatrix}$$

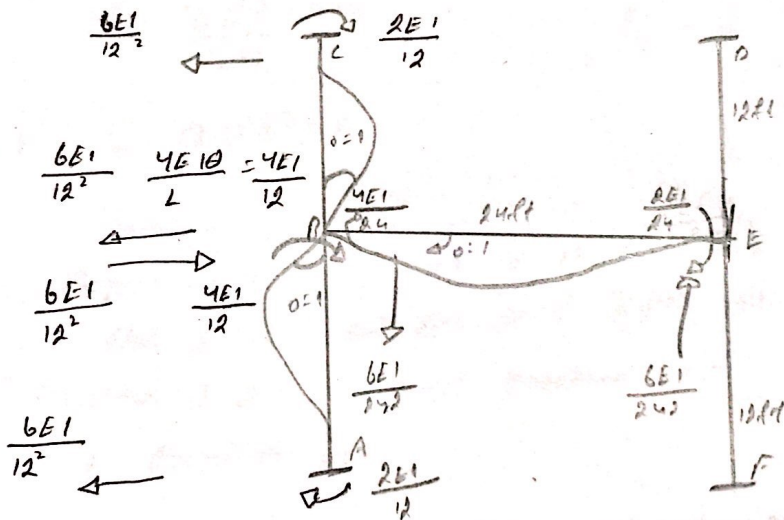
(#04)

step # 03: Primary structure acted upon by a unit value of D & computation of stiffness coefficients "S" values in the BKDS corresponding to the redundant joint displacement location

* 1st a unit rotation is applied at location 1 & prevented at 2 as shown compute the value of S_{11} and S_{21}

* Then apply a unit rotation at the redundant displacement location 2 and prevented at 1 as shown. compute the values of S_{12} & S_{22}

i. 1st $D_1 = 1$ & $D_2 = 0$ (#05) Compute the value of S_{11} and S_{21}



step #03 (i) contd... (#06)

$$S_{11} = \frac{4EI}{12} + \frac{4EI}{12} + \frac{4EI}{24}$$

$$S_{11} = 0.833EI$$

$$S_{21} = \frac{2EI}{24}$$

$$S_{21} = 0.0833EI$$

S_{11} = Action (sum of moments in this case) in the BKDS at redundant displacement location 1 due to unit rotation at that location.

S_{21} = Moment in the BDS at redundant displacement location 2 due to a unit rotation applied at location 1.

Step # 03: Contd... (#08)

$$S_{12} = \frac{2EI}{24}$$

$$S_{22} = \frac{4EI}{24} + \frac{4EI}{12} + \frac{4EI}{12}$$

$$S_{12} = 0.0833EI$$

$$S_{22} = 0.8333EI$$

S_{12} = Moment in the BKDS at redundant displacement location 1 due to unit rotation applied at redundant displacement location 2.

S_{22} = Moment in the BKDS at redundant displacement location 2 due to a unit rotation applied at that location.

step #03: contd.... (#09)

$$S_{11} = 0.833EI \quad S_{12} = 0.0833EI$$

$$S_{21} = 0.0833EI \quad S_{22} = 0.833EI$$

$$[S] = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}$$

$$[S] = EI \begin{bmatrix} 0.833 & 0.0833 \\ 0.0833 & 0.833 \end{bmatrix}$$

Stiffness coefficient matrix.

(#10)

Step #04: Apply equilibrium condition at the location of the redundant joint displacement to write equilibrium equations and solve for unknown joint displacement

$$AD_1 = ADL_1 + S_{11} D_1 + S_{12} D_2$$

$$AD_2 = ADL_2 + S_{12} D_1 + S_{22} D_2$$

$$\begin{bmatrix} AD_1 \\ AD_2 \end{bmatrix} = \begin{bmatrix} ADL_1 \\ ADL_2 \end{bmatrix} + \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix} \begin{bmatrix} D_1 \\ D_2 \end{bmatrix}$$

$$[AD]_{2 \times 1} = [ADL]_{2 \times 1} + [S]_{2 \times 2} \cdot [D]_{2 \times 1}$$

$$[D] = [S]^{-1} \cdot [AD - ADL]$$

$$\begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \begin{bmatrix} S_{11} & S_{12} \\ S_{12} & S_{22} \end{bmatrix}^{-1} \begin{bmatrix} AD_1 - ADL_1 \\ AD_2 - ADL_2 \end{bmatrix}$$

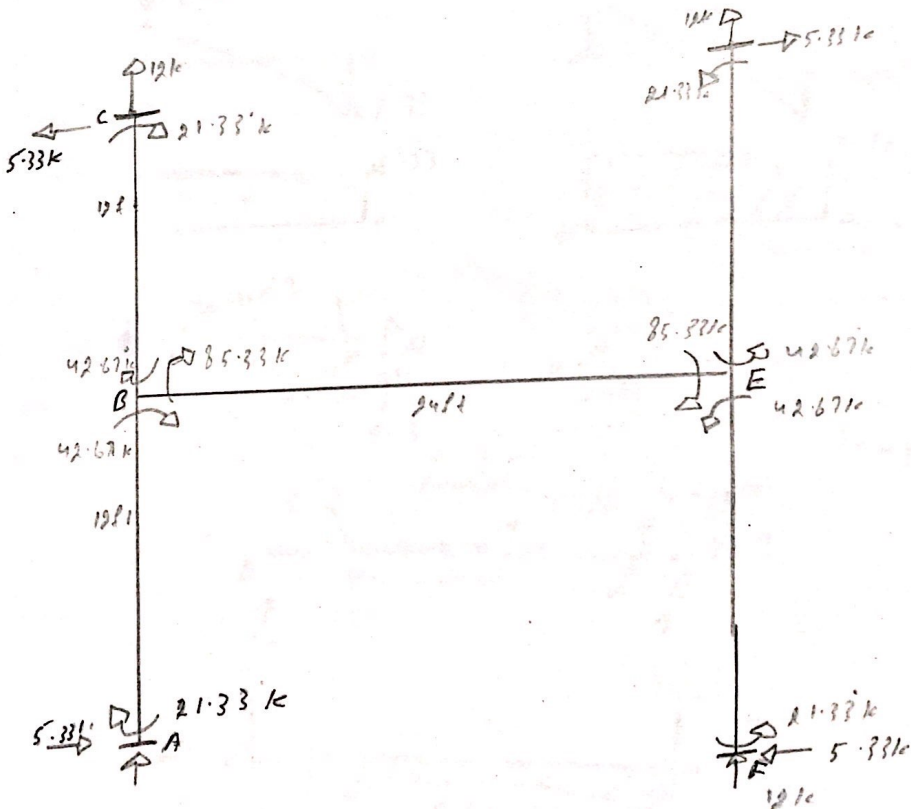
$$\begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \frac{1}{EI} \begin{bmatrix} 0.833 & 0.0833 \\ 0.0833 & 0.833 \end{bmatrix}^{-1} \begin{bmatrix} 0 - (-96) \\ 0 - 96 \end{bmatrix}$$

$$\begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \begin{bmatrix} 128 \\ -128 \end{bmatrix} \frac{1}{EI}$$

-ive sign shows that our assumed redundant joint displacement direction is wrong.

(# 11)

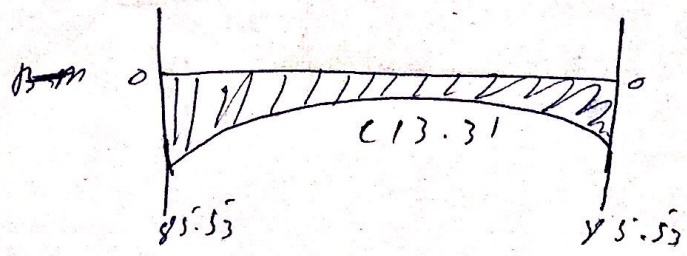
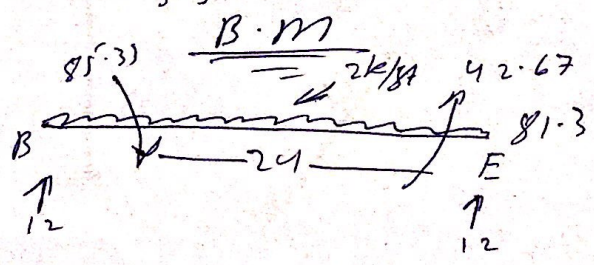
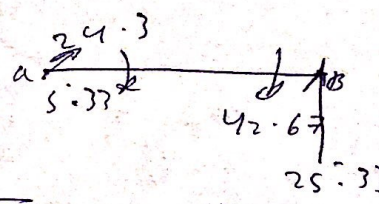
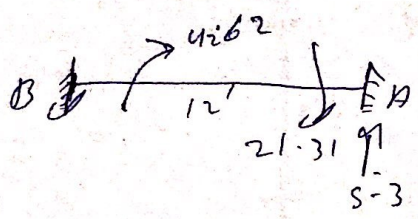
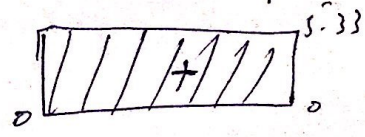
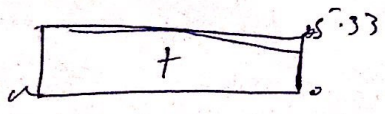
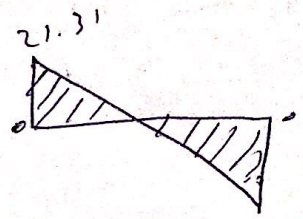
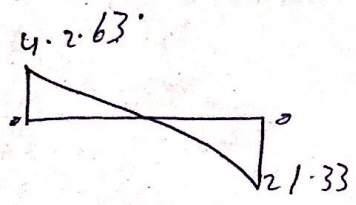
Step # 05: Complete the member end actions
you will get.



(# 12)

Step # 6 : Draw shear force & bending moment diagrams

Shear force



(page # 13)

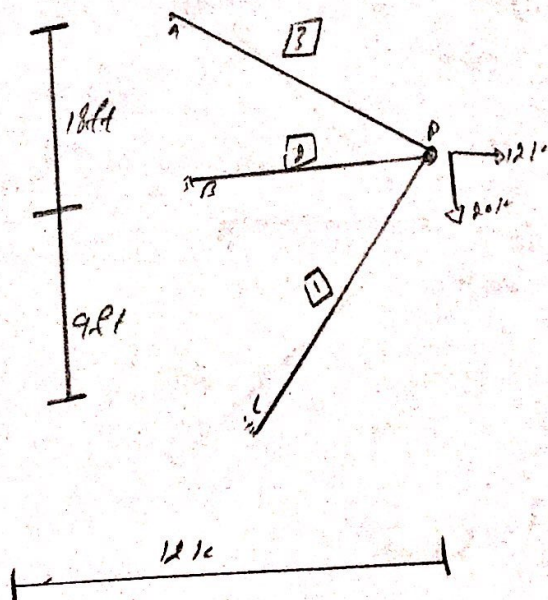
Q3: Analyze the given pin jointed frame using stiffness method.

Take $EA = \text{constant}$

$$L_1 = 15 \text{ ft}$$

$$L_2 = 12 \text{ ft}$$

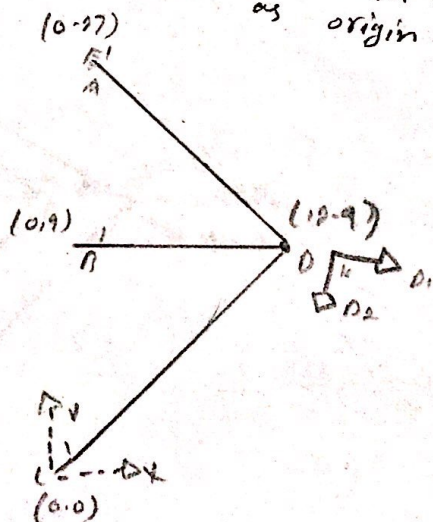
$$L_3 = 21.63 \text{ ft}$$



(page # 14)

Step # 02: Identify the unknown joint displacement and compute the values of $[AD]$ matrix.

Choose one point as an coordinates to each joint write the chosen origin. Here point C is taken as origin.

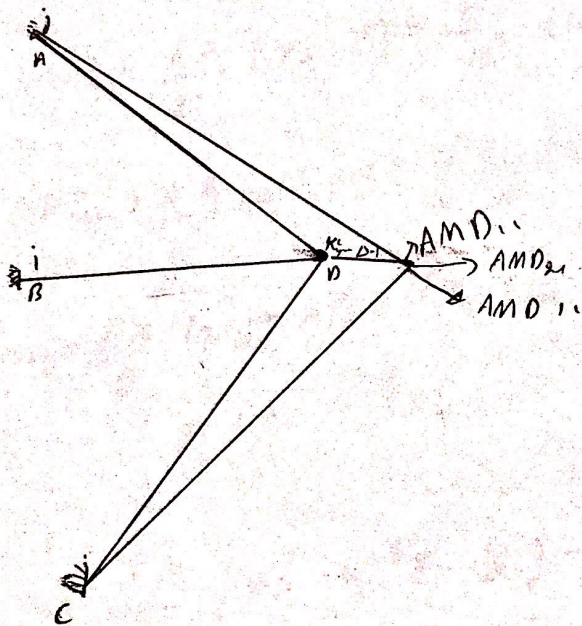


$$[D]_{2 \times 1} = \begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \begin{bmatrix} ? \\ ? \end{bmatrix}$$

$$[AD]_{2 \times 1} = \begin{bmatrix} AD_1 \\ AD_2 \end{bmatrix} = \begin{bmatrix} 12 \\ 90 \end{bmatrix}$$

step #02 : computation of AMD and stiffness matrices.

i. When $D_1 = 14 D_2 = 0$.



compute the values of AMD of then stiffness coefficients.

S_{11} will be the sum of all horizontal components of AMD. S_{21} will be the sum of all vertical components of AMD.

(16)
step #02: Computation of AMD and stiffness matrices.

i when $D_1 = 1$ and $D_2 = 0$

$$AMD_{11} = \frac{EA}{L^2} (u_k - u) = \frac{EA}{15^2} (12 - 0) = 0.0533 EA$$

$$AMD_{21} = \frac{EA}{L^2} (u_k - u) = \frac{EA}{12^2} (12 - 0) = 0.0833 EA$$

$$AMD_{31} = \frac{EA}{L^2} (u_k - u) = \frac{EA}{21.6^2} (12 - 0) = 0.0256 EA$$

$$S_{11} = \frac{EA}{L^3} (u_k - u_j)^2 = \frac{EA}{15^3} (12 - 0)^2 + \frac{EA}{12^3} (12 - 0)^2 + \frac{EA}{21.6^3} (12 - 0)^2$$
$$= 0.1402 EA$$

$$S_{21} = \frac{EA}{L^3} (u_k - u_j)(u_k - u_j) = \frac{EA}{15^3} (12 - 0)(-9 - 0)$$

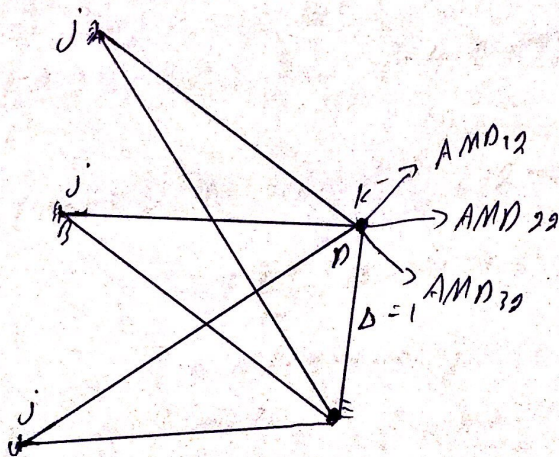
$$+ \frac{EA}{12^3} (12 - 0)(-9 - (-9)) + \frac{EA}{21.6^3} (12 - 0)(-9 - (-9))$$

$$(-27)) = -0.0107 EA.$$

(17)

Step # 02: Computation of AMD and stiffness matrix

ii. When $D_2 = 1$ and $D_1 = 0$.



Compute the values of AMD in then stiffness coefficients

S_{12} will be the sum of all horizontal components of S_{22} will be the sum of all vertical components of AMD.

Step #02: Computation of AMD and stiffness matrices.

(ii) when $D_2 = 1$ up $D_1 = 0$.

$$AMD_{12} = \frac{EA}{L^2} (y_{1k} - y_j) = \frac{EA}{15^2} (-9 + 0) = -0.04EA$$

$$AMD_{22} = \frac{EA}{L^2} (y_{1k} - y_j) = \frac{EA}{12^2} (-9 - (-9)) = 0$$

$$AMD_{32} = \frac{EA}{L^2} (y_{1k} - y_j) = \frac{EA}{21.63^2} (-9 - (-27)) = 0.0325EA$$

$$s_{12} = \frac{EA}{L^3} (u_k - u_j)(y_k - y_j) = \frac{EA}{15^3} [(12 - 0)(-9 - 0) + \frac{EA}{12^3} [(12 - 0)(-9 - (-9)) + \frac{EA}{21.63^3} (12 - 0)(-9 - (-27))] = -0.0107EA$$

$$s_{22} = \frac{EA}{L^3} (y_{1k} - y_j)^2 = \frac{EA}{15^3} (-9 - 0)^2 + \frac{EA}{12^3} (-9 + 9)^2$$

$$+ \frac{EA}{21.63} (-9 - 27)^2 = 0.056EA$$

(19)

Step # 02: Computation of AMD and stiffness matrices

AMD matrix will be.

$$AMD_{11} = 0.0533 EA \quad AMD_{21} = 0.0833 EA$$

$$AMD_{12} = -0.04 EA \quad AMD_{22} = 0$$

$$AMD_{31} = 0.0256 EA$$

$$AMD_{32} = 0.0385 EA$$

$$[AMD] = EA \begin{bmatrix} 0.0533 & 0.04 \\ 0.0833 & 0 \\ 0.0256 & 0.0385 \end{bmatrix}$$

stiffness matrix will be

$$S_{11} = 0.1402 EA \quad S_{21} = 0.0107 EA \quad S_{12} = -0.0107 EA$$

$$S_{22} = 0.056 EA$$

$$[S] = \begin{bmatrix} S_{11} & S_{12} \\ S_{21} & S_{22} \end{bmatrix}$$

$$[S] = EA \begin{bmatrix} 0.1402 & -0.0107 \\ 0.0107 & 0.056 \end{bmatrix}$$

(20)

step #03: Apply equilibrium condition at location of the redundant joint displacement to write equilibrium equations and solve for unknown joint displacement.

$$AD_1 = s_{11} D_1 + s_{12} D_2$$

$$AD_2 = s_{21} D_1 + s_{22} D_2$$

$$\begin{bmatrix} AD_1 \\ AD_2 \end{bmatrix} = \begin{bmatrix} s_{11} & s_{12} \\ s_{21} & s_{22} \end{bmatrix} \begin{bmatrix} D_1 \\ D_2 \end{bmatrix}$$

$$[AD]_{2 \times 1} = [S]_{2 \times 2} \cdot [D]_{2 \times 1}$$

$$[D] = [S]^{-1} \cdot [AD]$$

(21)

$$\begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \begin{bmatrix} s_{11} & s_{12} \\ s_{21} & s_{22} \end{bmatrix}^{-1} \begin{bmatrix} AD_1 \\ AD_2 \end{bmatrix}$$

$$\begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \frac{1}{EA} \begin{bmatrix} 0.1402 & -0.0107 \\ -0.0107 & 0.056 \end{bmatrix}^{-1} \begin{bmatrix} 12 \\ 26 \end{bmatrix}$$

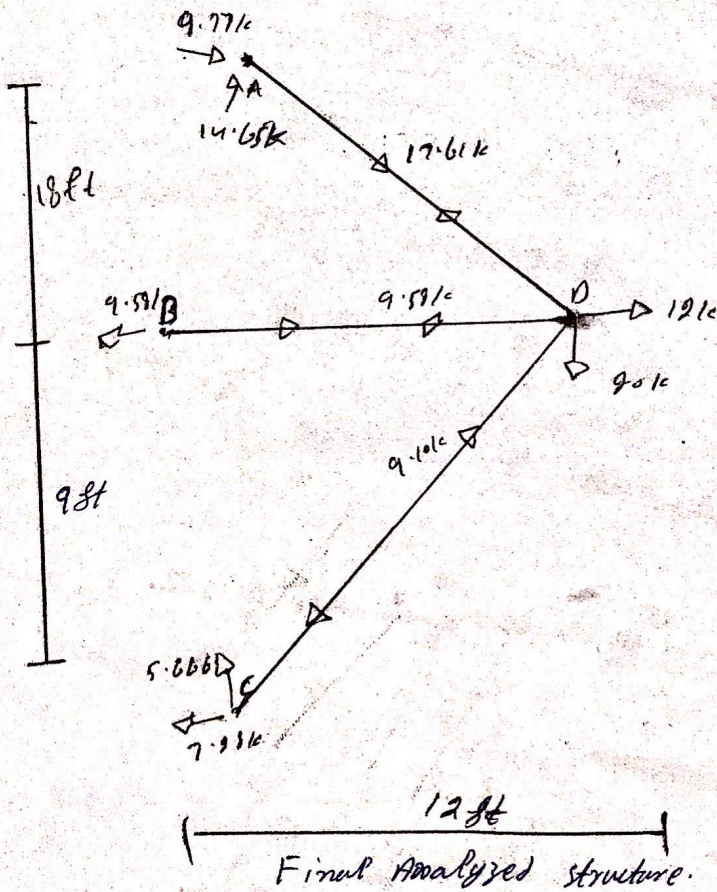
$$\begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \frac{1}{EA} \begin{bmatrix} 115.065 \\ 380.83 \end{bmatrix}$$

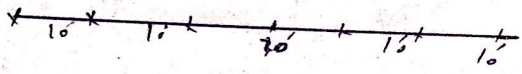
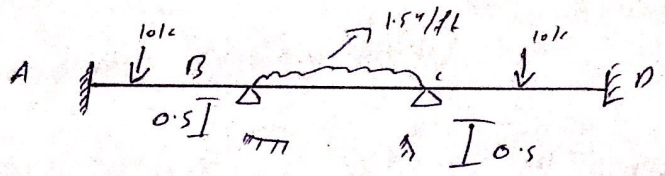
$$\begin{bmatrix} AM_1 \\ AM_2 \\ AM_3 \end{bmatrix} = \begin{bmatrix} AMD_{11} & AMD_{12} \\ AMD_{21} & AMD_{22} \\ AMD_{31} & AMD_{32} \end{bmatrix} \begin{bmatrix} D_1 \\ D_2 \end{bmatrix}$$

$$\begin{bmatrix} AM_1 \\ AM_2 \\ AM_3 \end{bmatrix} = EA \begin{bmatrix} 0.0533 & -0.04 \\ 0.0833 & 0 \\ 0.0256 & 0.0385 \end{bmatrix}$$

$$\begin{bmatrix} 115.065 \\ 380.83 \end{bmatrix} \frac{1}{EA} = \begin{bmatrix} -9.10k \\ 4.58k \\ 17.61k \end{bmatrix}$$

(22)
Stiffness Method for Truss Analysis.





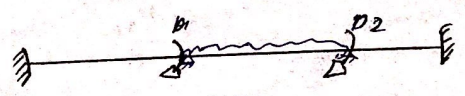
$E = 30,000 \text{ ksi}$ $I = 200 \text{ in}^4$

$EI = 41666.7 \text{ k-ft}^2$

$\Delta = \frac{1}{2} \times 20 = 10 \text{ ft}$

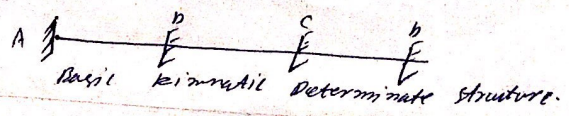
Step # 07

selection of reduced joint displacements



$$[D] = \begin{bmatrix} D_1 \\ D_2 \end{bmatrix} = \begin{bmatrix} ? \\ ? \end{bmatrix}$$

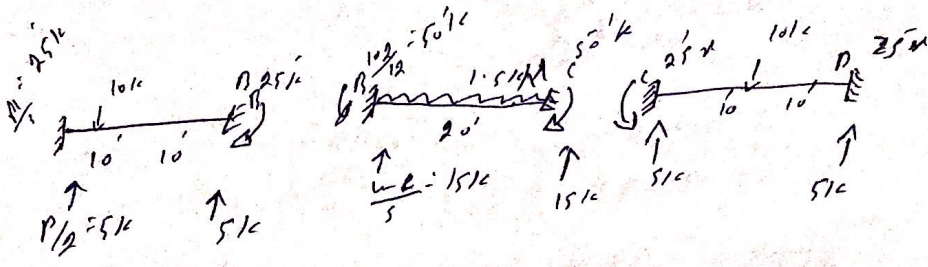
$$[AD] = \begin{bmatrix} AD_1 \\ AD_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$



step # 2

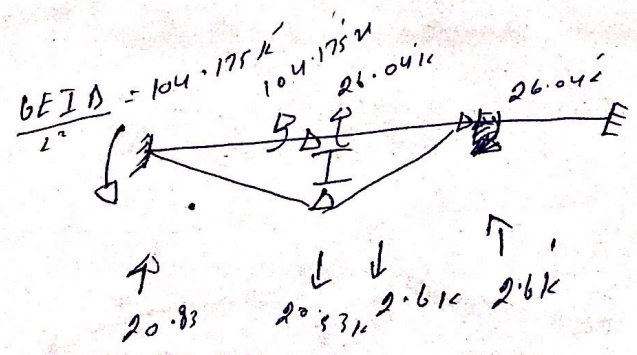
(#24)
Compute ADL Matrix

(i) Due to direct loading (ADL')



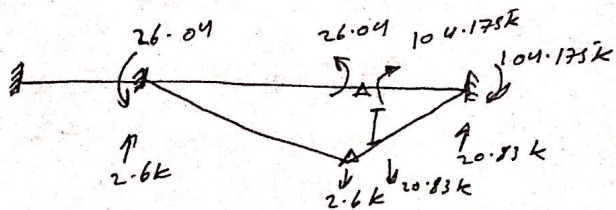
$$[ADL'] = \begin{bmatrix} ADL'_1 \\ ADL'_2 \end{bmatrix} = \begin{bmatrix} -25 \\ 25 \end{bmatrix}$$

(ii) Due to settlement at joint B



$$[ADL''] = \begin{bmatrix} ADL''_1 \\ ADL''_2 \end{bmatrix} = \begin{bmatrix} -78.135 \\ 26.04 \end{bmatrix}$$

(ii) Due to self-weight (25) at joint C



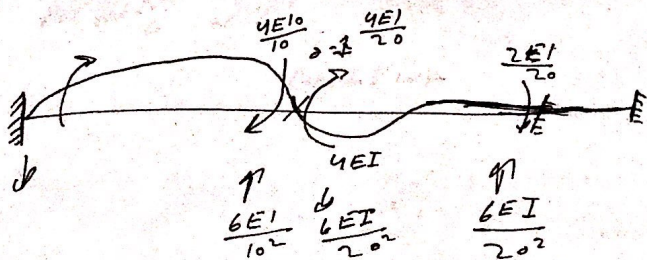
$$[ADP'''] = [APL_1'''] = \begin{bmatrix} -26.04 \\ 78.135 \end{bmatrix}$$

$$[ADL] = \begin{bmatrix} APL_1 \\ ADL_2 \end{bmatrix} = \begin{bmatrix} ADL_1' + ADL_1'' + ADL_1''' \\ ADL_2' + ADL_2'' + ADL_2''' \end{bmatrix}$$

$$= \begin{bmatrix} -129.175 \\ +129.175 \end{bmatrix}$$

step # 3 stiffness coefficients matrix (S)

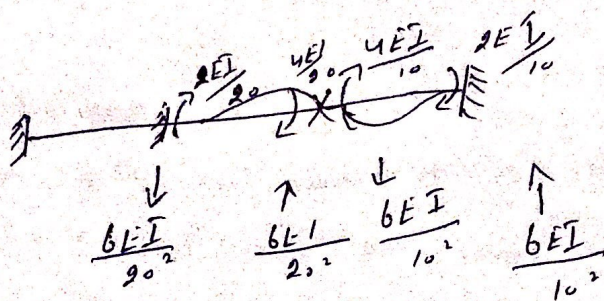
(i) $D_1 = 1 ; D_2 = 0$



$$s_{11} = \frac{4EI}{10} + \frac{4EI}{20} = \frac{3EI}{10} = 0.6 EI \quad (26)$$

$$s_{21} = \frac{2EI}{20} = 0.1 EI$$

$$(ii) \quad D_2 = 7, \quad D_1 = 0$$



$$s_{12} = 0.1 EI$$

$$s_{22} = 0.6 EI$$

$$[S] = \begin{bmatrix} s_{11} & s_{12} \\ s_{21} & s_{22} \end{bmatrix} = EI \begin{bmatrix} 0.6 & 0.1 \\ 0.1 & 0.6 \end{bmatrix}$$

step # 4 = Applying joint equilibrium condition

$$[AD] = [ADL] + [S] \{D\}$$

$$\text{or } \{D\} = [S]^{-1} [AD - ADL]$$

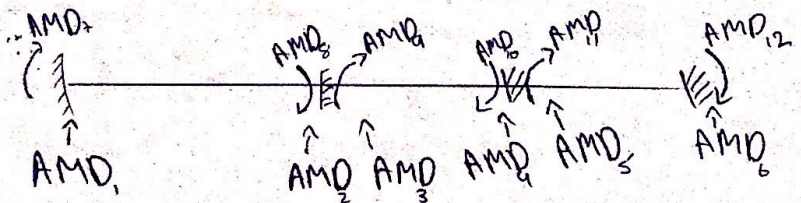
$$\begin{bmatrix} O_1 \\ O_2 \end{bmatrix} \xrightarrow{(27)} \frac{1}{E1} \begin{bmatrix} 1.7143 & -0.2857 \\ -0.2857 & 1.7143 \end{bmatrix} = \begin{bmatrix} 129.175 \\ -129.175 \end{bmatrix}$$

$$\begin{bmatrix} O_1 \\ O_2 \end{bmatrix} = \frac{1}{E1} \begin{bmatrix} 258.35 \\ -258.35 \end{bmatrix}$$

STEP A 5 (9) complete and values

(i) First apply unit rotation at redundant location 1 and compute the member end actions \rightarrow we will take these values from step #3 (i).

(ii). Then apply unit rotation at redundant location 2 and compute the member end actions \rightarrow we will take these values from step #3 (ii).



(6) (28)

AMD ₁₁	AMD ₁₂	-0.06	0
AMD ₂₁	AMD ₂₂	0.06	0
3)	AMD ₃₂	-0.015	-0.015
4)	42	0.015	0.015
5)	52	0	-0.06
6)	62 = EI	0	0.06
7)	72	0.2	0
8)	82	0.4	0
9)	92	0.2	0
10)	102	0.1	0.2
11-1	11-2	0	0.4
12-1	12-2	0	0.2

(6) Compute AML values. These are the member end actions when the actual load is applied on the structure. we will take from step #2.

AML ₁	25.83
2	-15.83
3	15
4	15
5	-15.83
6	25.83
7	-129.175
8	-79.125
9	-50
10	50
11	79.175
12	129.175

(29)

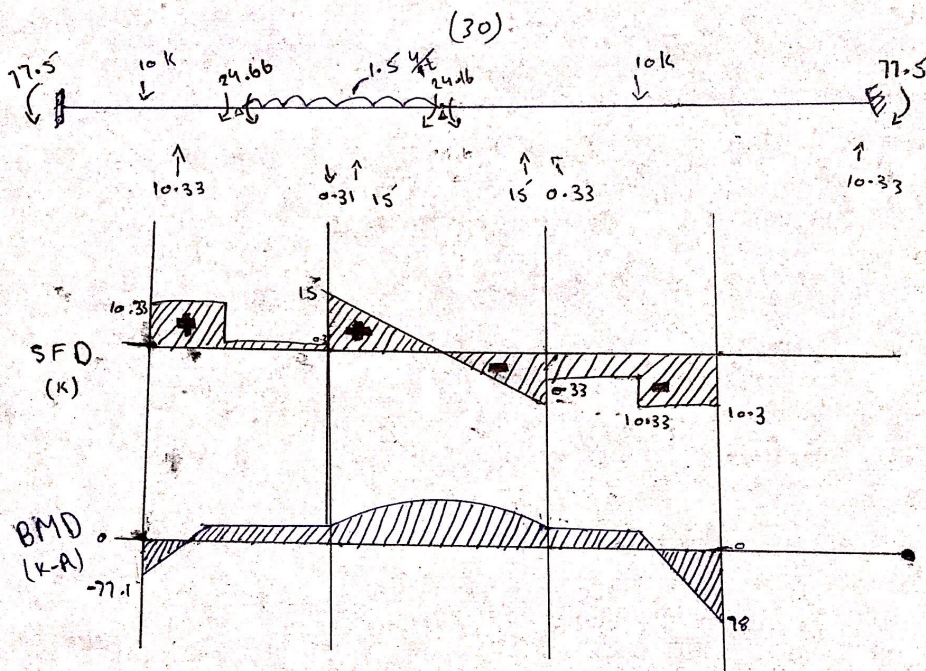
Now member end action are calculated

as

$$[AM] = [AML] + [AMD] [D]$$

AM ₁	25.83	-0.06	0	$\left[\begin{array}{l} 258.35 \\ -258.35 \end{array} \right]$
AM ₂	-15.83	0.06	0	
AM ₃	15	-0.015	-0.015	
AM ₄	15	0.015	0.015	
AM ₅	-15.83	0	-0.06	
AM ₆	25.83	0	0.06	
AM ₇	-129.175	0.2	0	
AM ₈	-79.175	0.4	0	
AM ₉	-50	0.2	0.1	
AM ₁₀	50	0.1	0.2	
AM ₁₁	+79.125	0	0.4	
AM ₁₂	+129.175	0	0.2	

AM ₁	10.33
AM ₂	-0.33
3	15
4	15
5	-0.33
6	10.33
7	-77.5
8	24.16
9	-24.16
10	24.16
11	-24.16
12	77.5



The End.