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Section

B

Semister

6th

Subject

Plain and reinforced  
Concrete Design 1

Instructor

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Date

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Q.No.1:

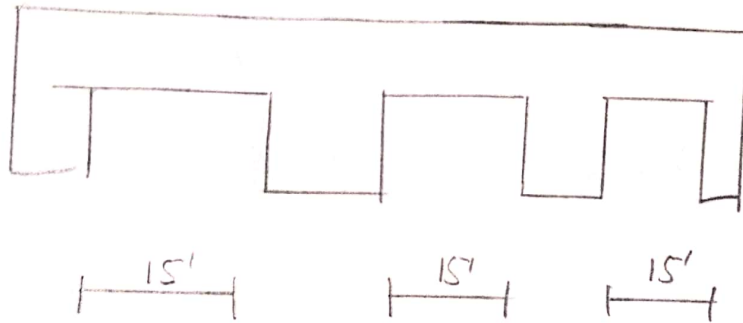
Given Data:

3 equal spans concrete slab

Clear span b/w supports = 15 ft

Factored Live Load = 1600 lb/ft<sup>2</sup>Service floor finish load = 20 lb/ft<sup>2</sup> $f'_c = 4000 \text{ psi}$  $f_y = 40 \text{ ksi}$ 

Solution



Step #1 (Minimum Thickness)

By using formula

$$t_{\min} = \frac{L}{28} = \frac{15}{28} = 0.54 \approx 6.5''$$

As  $f_y \rightarrow 40 \text{ ksi}$ 

So we will multiply a factor with thickness

$$\text{Factor} = \left(0.4 + \frac{f_y}{100}\right)$$

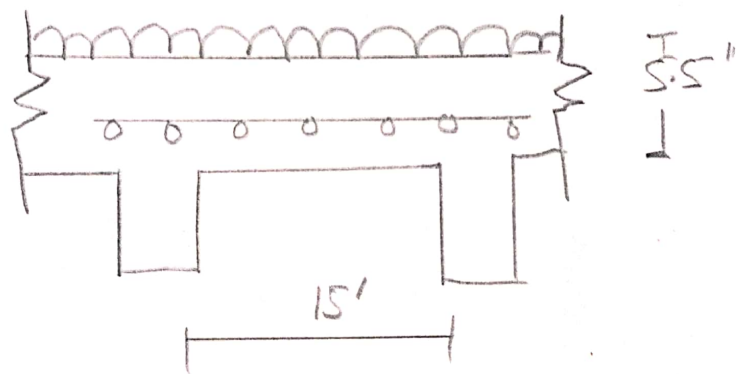
$$= \left(0.4 + \frac{40}{100}\right) = 0.8$$

Hence the minimum thickness will be

$$6.5 \times 0.8$$

$$t_{\min} = 5.2 \approx 5.5''$$

Step #2 : (Effective Depth)



By formula

$$d = t - \text{clear cover} - \frac{1}{2} (\text{dia of main bar})$$

$$= 5.5 - 0.75 - \frac{1}{2} \left(\frac{5}{8}\right)$$

$$d \approx 4.5''$$

(3)

Step # 3: (self wt. of slab)

By formula

$$\frac{L}{12} + \gamma_{\text{concrete}}$$

$$= \frac{5.5}{12} \times 150 = 68.75 \text{ lb/ft}^2$$

Step # 04: (Total Factored Load)

$$\text{Factored Live Load} = 160 \text{ lb/ft}^2$$

So the Factored Dead Load will be

$$D.L = 1.2 (20 + 68.75)$$

$$= 106.5 \text{ lb/ft}^2$$

$$\text{Total factored load} = D.L + L.L$$

$$= 106.5 + 160$$

$$= 266.5 \text{ lb/ft}^2$$

$$= 0.2665 \text{ k/ft}^2$$

Step #5:- (Ultimate Moment)

By Using formula

$$\begin{aligned} M_u &= \frac{w_u \times L^2}{8} \\ &= \frac{0.26665 \times (15)^2 \times 12}{8} \\ &= \boxed{89.94 \text{ kip-inches}} \end{aligned}$$

Step #6 Area of steel for Main Bars  
By Trial and Repeat Method

Trial #01

Let depth of compression block

$$\begin{aligned} a &= 0.2 \times t \\ &= 0.2 \times 5.5 = 1.1'' \end{aligned}$$

$$A_{st} = \frac{m_u}{\phi \times f_y \times \left(d - \frac{a}{2}\right)}$$

(5)

$$\frac{89.94}{0.90 \times 40 \times \left(4.5 - \frac{1.1}{2}\right)}$$

$$A_{st} = 0.63 \text{ in}^2$$

Trial # 02

$$a = \frac{A_s \times f_y}{0.55 \times f_c \times b} = \frac{0.63 \times 40}{0.55 \times 4 \times 12}$$
$$\Rightarrow 0.62 \text{ in}^2$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times \left(d - \frac{a}{2}\right)}$$

$$= \frac{89.94}{0.90 \times 40 \times \left(4.5 - \frac{0.6}{2}\right)}$$

$$A_{st} = 0.59 \text{ in}^2$$

Trial # 03

(6)

$$a = \frac{0.59 \times 40}{0.85 \times 4 \times 12}$$

$$= 0.57''$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times \left(4.5 - \frac{0.5}{2}\right)}$$

$$= 0.59 \text{ in}^2$$

So we will use  $A_{st} = 0.59 \text{ in}^2$

Step #07: Area of steel for distribution reinforcement

By formula

$$A_{min} = 0.002 \times b \times t \rightarrow (\text{for Grade 40 steel})$$

$$= 0.002 \times 12 \times 5.5 \Rightarrow \boxed{0.132 \text{ in}^2}$$

(7)

Step # 08 ~ Spacing for main bars

By formula

$$\text{Spacing} = \frac{A_b}{A_{st}} \times 12$$

We use #6 bar dia =  $\left(\frac{6}{8}\right)''$

$$\text{Area} = \frac{\pi}{4} \left(\frac{6}{8}\right)^2 = 0.442 \text{ in}^2$$

Step # 09 Spacing for distribution bars

$$\text{Spacing} = \frac{A_b}{A_{st}}$$

We use #5 bars so

$$\begin{aligned} \text{dia} = \left(\frac{5}{8}\right)'' &= \text{Area} = \frac{\pi}{4} \left(\frac{5}{8}\right)^2 \\ &= 0.31 \text{ in}^2 \end{aligned}$$

$$\text{Spacing} = \frac{0.31}{0.132} \times 12 = 2.81'' \approx 28'' \text{ c/c}$$



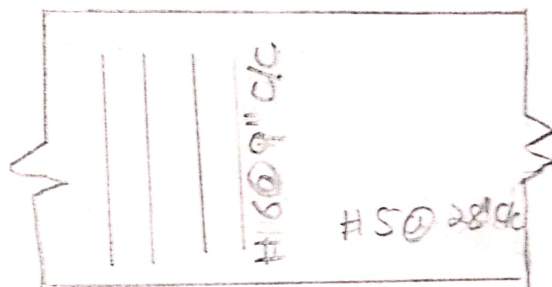
(8)

Step # 10 Find Sketch

$$f'_c = 4 \text{ ksi} \quad , \quad f_y = 40 \text{ ksi}$$

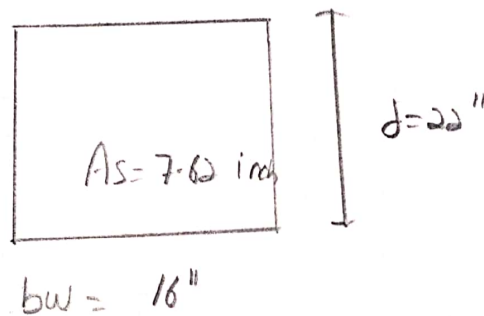
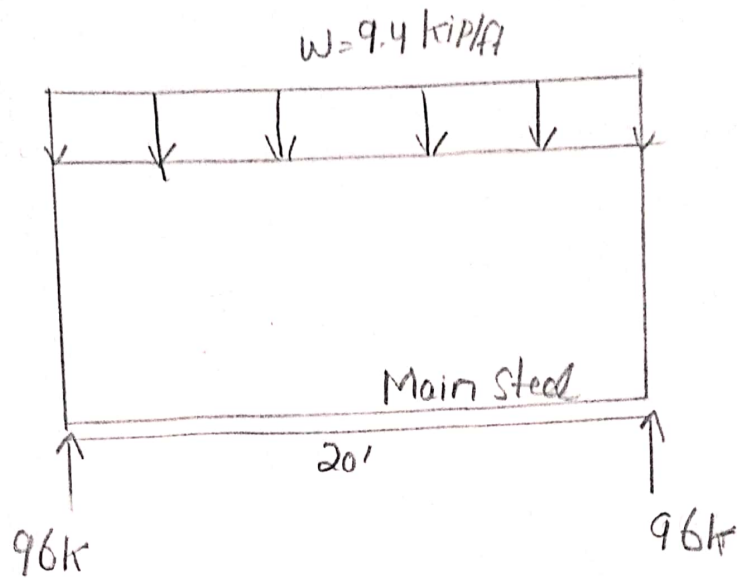
Main Steel # 6 at 9" c/c

Distribution steel # 5 at 28" c/c



Q No 2:

Sol:-



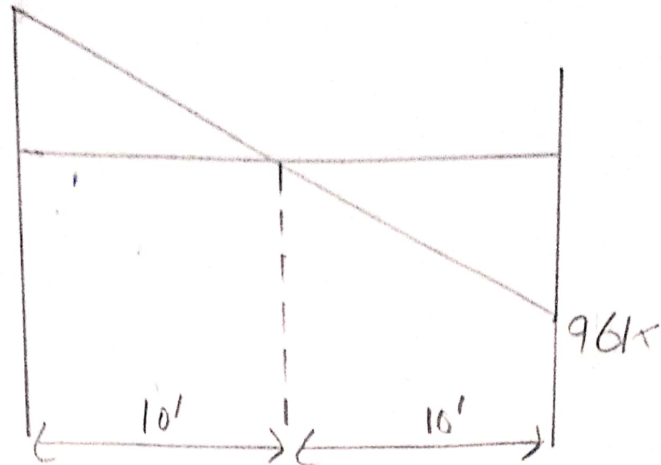
Step #01 find values of  $R_1$  and  $R_2$

$$\text{Total loads} = \frac{9.4 \times 20}{2} = \frac{188}{2} = 94 \text{ k}$$

Step #02

Draw its shear force diagram

(10)



Step #03

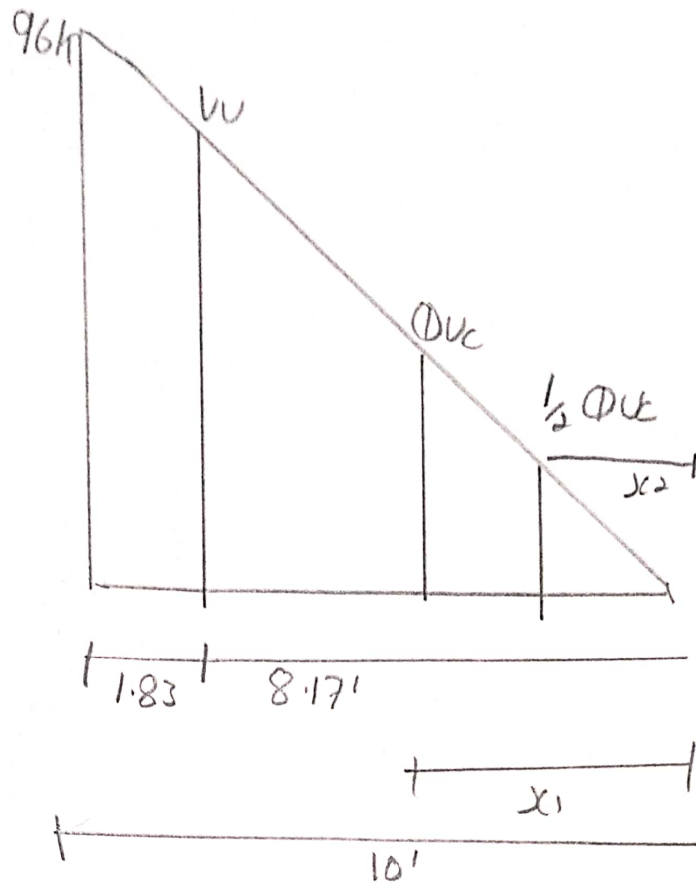
find the value of critical shear 'U<sub>c</sub>' and its location, As we know that critical section is located at distance 'd' from face of =  $d = 22'' = 1.83'$

Value of critical shear at distance 'd' by similarity of triangles

P.T.O



(11)



From similar  $\Delta$ 's  $\frac{96}{10} = \frac{UU}{8.17}$

$$UU = 78.43 \text{ k}$$

Step # 4 Find the value of  $\Phi U_c$  " $\{ \frac{1}{2} \Phi U_c$ " and also its distance from zero shear to right side

$$\Phi U_c = \Phi \times x_2 \times \sqrt{f_c} \times b_w \times d$$

$$\Rightarrow \frac{0.75 \times 2 \times \sqrt{4000} \times 16 \times 22}{1000}$$

(12)

$$\boxed{\Phi_{UC} = 33.40 \text{ k}}$$

Location of  $\Phi_{UC}$  by similarity of  $\Delta S'$ ,

$$\frac{96}{10} = \frac{33.40}{x_1}$$

$$x_1 = 3.48'$$

$$\text{Now } \frac{1}{2} \Phi_{UC} = \frac{33.40}{2} = 16.70 \text{ k}$$

$$\text{Location of } \frac{1}{2} \Phi_{UC} \Rightarrow \frac{96}{10} = \frac{16.70}{x_2}$$

$$\boxed{x_2 = 1.74'}$$

Step #5: Value of  $\Phi_{US}$  ( $U_U = \Phi_{US} + \Phi_{UC}$ )

$$\text{So } \Phi_{US} = U_U - \Phi_{UC}$$

$$\Phi_{US} = 78.43 - 33.40$$

$$\boxed{\Phi_{US} = 45.03 \text{ k}}$$

Step #6 Check on section adequacy.

(13)

$$\Rightarrow \phi \times 8 \times \sqrt{f_c} \times b_w \times d = \frac{0.75 \times 8 \times \sqrt{4000} \times 16 \times 22}{1000}$$
$$= 133.57 \text{ k}$$

As  $\phi \times 8 \sqrt{f_c} \times b_w \times d > \phi U_s \rightarrow \text{It}$   
means section is adequate.

Step 07# Check on min spacing for  
Stirrups.

$$\phi \times 4 \times \sqrt{f_c} \times b_w \times d = \frac{0.75 \times 4 \times \sqrt{4000} \times 16 \times 22}{1000}$$
$$= 66.79 \text{ k}$$

As  $\phi \times 4 \sqrt{f_c} \times b_w \times d > \phi U_s = 45.03 \text{ k}$

Thus max spacing will be selected  
from the following four condition

1)  $f_{\text{max}} = 24''$

2)  $\frac{d}{2} = \frac{22}{2} = 11''$

$$3) S_{max} = \frac{A_u \times f_y}{0.75 \times \rho_c \times b_w} \quad (14)$$

$$= 0$$

$$\therefore A_u = \frac{\pi}{4} \left(\frac{3}{8}\right)^2$$

$$= \frac{0.22 \times 60000}{0.75 \times 4000 \times 16}$$

$$= 17.40$$

$$4) S_{max} = \frac{0.22 \times 60000}{50 \times 16} = 16.50''$$

From above four condition least value of spacing for #3, 2 legged stirrup will be selected

$$\text{So } S_{max} = 11'' \text{ c/c}$$

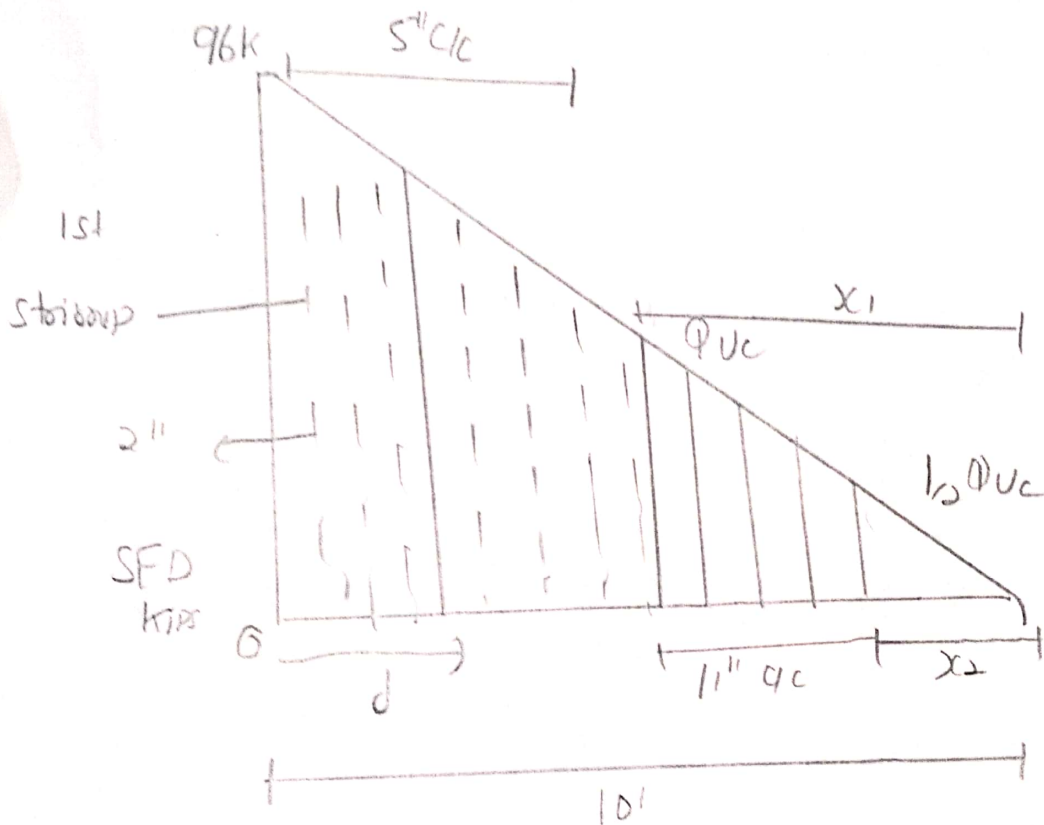
Step # 8 Spacing of stirrup formula  
Critical Section

$$S = \frac{0.75 \times 0.22 \times 60 \times 22}{76.80 - 33.44}$$

(15)

$$\int = 5'' \text{ @ } 9c$$

Step 11 a



As we know that first stirrup from face of support

$$= \int = \frac{S}{2} \approx 2''$$



QNo3:

Given Data

Column = 12 inch square

Reinforced = 4#9

Ties are #3 spaced @ 12 inches

$F_c' = 4000 \text{ psi}$

$f_y = 60 \text{ ksi}$

Solution.

Step #01

Find gross area of concrete

$A_g = b \times b$  (since it is square field)

$A_g = 12 \times 12 = 144 \text{ in}^2$  (Actual)

Step #02: Find area of steel

Since  $A_s = 5\%$  of  $A_g$

$$A_s = 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

Step #03: Ultimate load carrying capacity

$$P_u = \phi \times 0.80 \times [0.85 \times f_c \times (A_g - A_s) + A_s \times f_y]$$

$$P_u = 0.65 \times 0.80 [0.85 \times 4 (144 - 7.2) + 7.2 \times 60]$$

$$P_u = 466.50 \text{ k}$$

Step #04: Sketch of ties (c/c to distance)

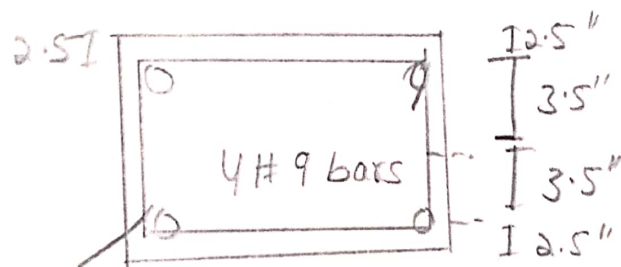
From the below value use chose  
the least value of all thus

$$\rightarrow 16 \times \text{dia of long bar} = 16 \times 9/8 = 18''$$

$$\rightarrow 48 \times \text{dia of tie bar} = 48 \times 3/8 = 18''$$

Least column dimension = 12''

the c/c distance b/w ties = 12''



#3 @ 12''

So it is a tied square column so there  
is no spiral stirrup used, the  
stirrup used is of rectangular shape due

(19)

the specification of the structure  
that we use tie stirrups instead.

Q No 4.

Sol:

Step #1

$$\text{let } h = 24''$$

Step #02

$$\text{Total weight} = \text{wt of soil} + \text{wt of Rc}$$

$$= 3 \times 120 + 2 \times 150 = 660 \text{ Psf}$$

$$= 0.660$$

Step #03

effective bearing capacity

$$V_e = V_a - W = 2.50 - 0.660$$

$$V_e = 1.84 \text{ ksf}$$

(21)

Step # 04

Required Area for foundation

$$A_{req} = \frac{\text{Service Load}}{q_c} = \frac{100 + 120}{1.84}$$

$$A_{req} = 119.56 \text{ ft}^2$$

Step # 5

Since foundation is square

$$A_{req} = B \times B = 119.56$$

$$B \Rightarrow 119' - 56''$$

Step # 6

$$q_{up} = \frac{\text{factored load}}{(B)^2}$$

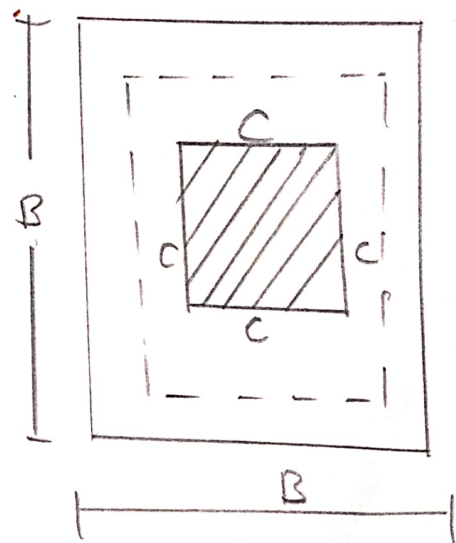
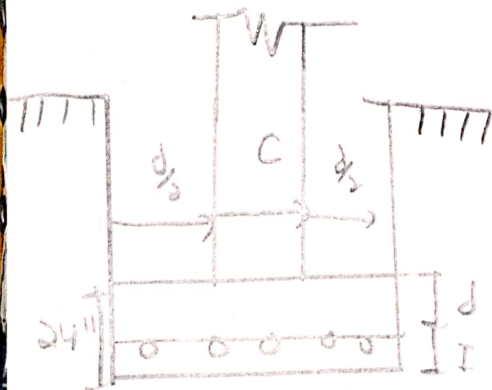
$$q_{up} = \frac{1.2 \times 100 + 1.6 \times 120}{(119.56)^2}$$

$$V_{up} = 0.021 \text{ k/ft}^2$$

Step#07

Punching shear,

$$b_o = 4(c+d)$$



$$d = h - \text{clear cover} - \text{dia of bar} - \frac{1}{2} \times d_b$$

$$d = 24 - 3 - 1 - \frac{1}{2} \times 1$$

$$= 19.5''$$

$$b_o = 4(16 + 19.5) = 142''$$

(25)

Step 11-08

$$VV_2 = VV_P \times [B^2 - (CID)^2]$$

$$= 0.001 \left[ (11956)^2 - \left( \frac{16117.5}{1.2} \right)^2 \right]$$

$$VV_2 = 300$$