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Section:- B

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Program:- B.Sc Civil Engineering

Assignment:- Plain &  
Reinforced Concrete Design-I

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## Question No - 01

Explain in detail types of stirrups with figures and also explain ACI codes for shear design

Stirrup :-

Stirrups are closed loop bars tied at regular intervals in beam reinforcement to hold the bars in position.

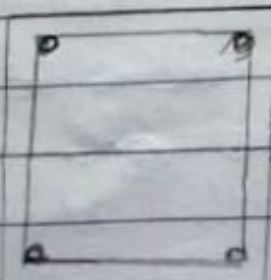
Types of stirrups :-

1) Single legged stirrup :-

The single leg stirrups have rarely been used because they are mostly used when binding only two rods.

2) Two legged stirrups :-

It is most commonly and widely used stirrup. Minimum 4 bars are required for providing this stirrup.

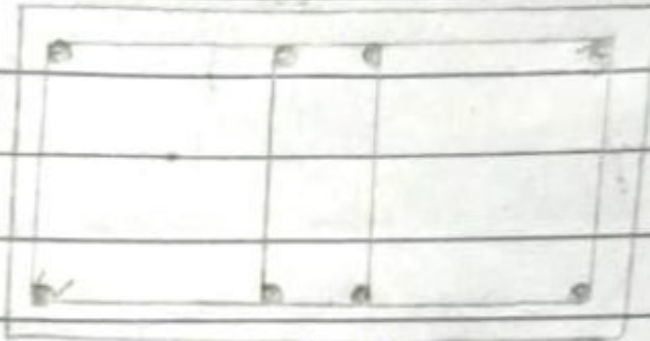


2 legged stirrup

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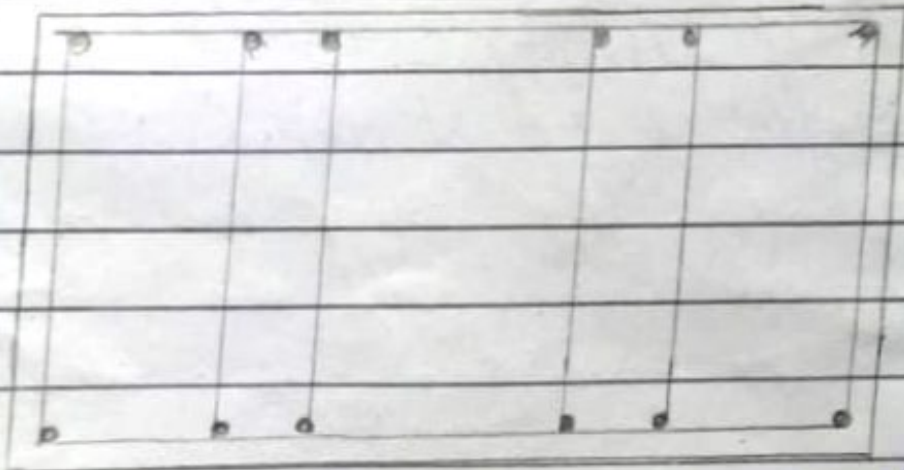
### 3 For Legged stirrup:-

These stirrups are used in case of web reinforcement.



4 - Legged stirrup

### 4. Six Legged stirrup:- page 02



### ACI codes for shear design of a Beam.

According to ACI - 318, following are formulas used for the shear design of a beam.

#### 1. Critical section:-

critical section occurs at  $u_s$  and equal to effective depth

#### 2. Shear strength capacity of

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concrete is..

$$V_c = 2 \sqrt{f_c} \times b_w \times d$$

3:- Minimum web Reinforcement:-

If  $V_u < \phi V_c$ , then theoretically no web reinforcement is required. However ACI code require provision of at least a minimum area of web reinforcement equal to  $\phi = 0.75 \rightarrow$  for shear design.

( $\because V_u =$  Total factored shear applied at a given section)

$\Rightarrow$  For minimum reinforcement area

$$A_{min} = 0.75 \sqrt{f_c} \times b_w \times S \text{ or } \frac{30 \times b_w \times S}{f_y} \rightarrow \begin{cases} \text{Higher} \\ \text{value is} \\ \text{selected} \end{cases}$$

By interchanging the above formulas we can obtain the formula maximum spacing

$$S_{max} = \frac{A_v \times f_y}{0.75 \sqrt{f_c} \times b_w} \text{ or } \frac{A_v \times f_y}{30 \times b_w} \rightarrow \begin{cases} \text{Lesser value} \\ \text{is} \\ \text{selected} \end{cases}$$

Q

Page 03

4 - No web-reinforcement is required if

$$v_u < \frac{1}{2} \phi v_c$$

→ Between the critical sections " $v_u$ " and " $\phi v_c$ ", spacing b/w web reinforcement can be found by

$$S = \frac{\phi + A_u + F_y + d}{v_u - \phi v_c}$$

5: -  $d_b v_s \leq 4\sqrt{f_c} b_w + d$  then max spacing for stirrups will be the smallest of the following

1 - 24"

2 -  $d/2$

3 -  $s_{max} = \frac{A_u + F_y}{0.75 + \sqrt{f_c} + b_w}$

4 -  $s_{max} = \frac{A_u + F_y}{s_o + b_w}$

$d_b v_s > 4\sqrt{f_c} + b_w + d$

Max - Spacing will be halved

$v_s > 8 + \sqrt{f_c} + b_w + d$

then either increase cross sectional dimensions or increase  $f_c$

## Q: No 2

A simply supported rectangular beam is wide having an effective depth of 22" to carry a lateral load of 6.5 K/ft on a 8' simple span. It is reinforced with 7 in<sup>2</sup> of tensile steel area. If  $f_c = 4 \text{ KSI}$  and  $f_y = 60 \text{ KSI}$ , then design the beam for shear.

Given,

Breadth of web of beam ( $b_w$ ) = 16"

Effective depth ( $d$ ) = 22"

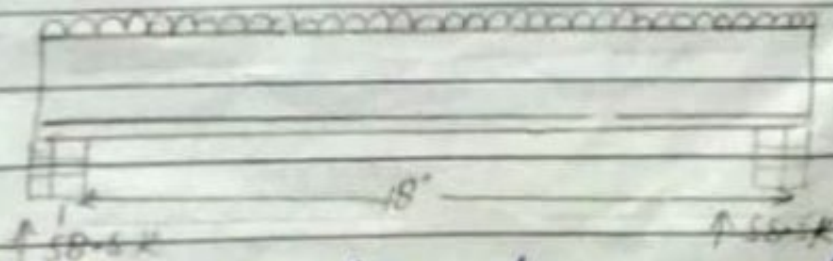
Given Load = 6.5 K/ft

Steel Area = 7 in<sup>2</sup>

$f_c = 4 \text{ KSI}$

$f_y = 60 \text{ KSI}$

Solution



**Step # 01 (Reactions on supports)**

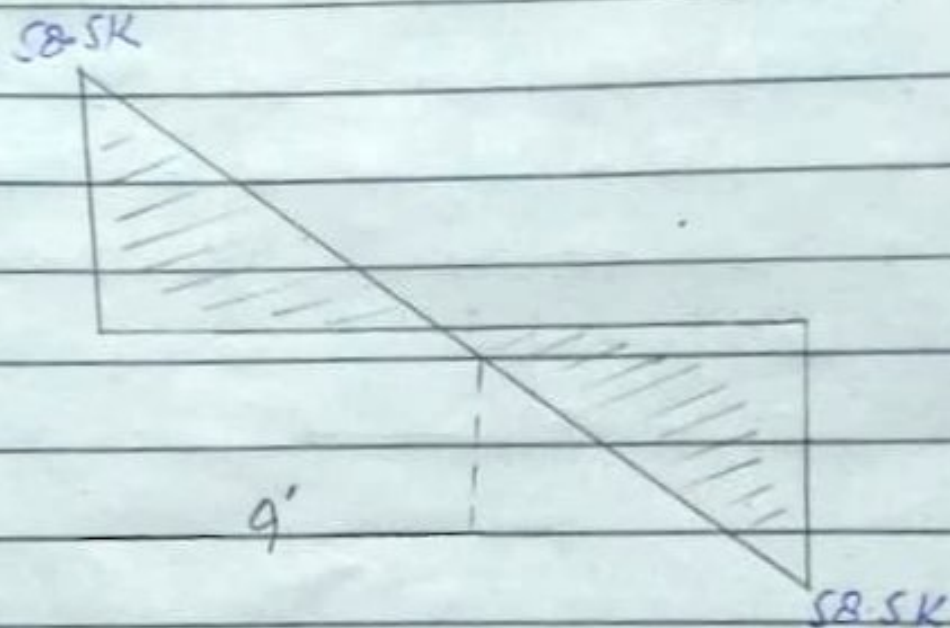
Finding the reactions due to applied load

$$\text{Total Load} = 6.5 \times 18 = 117 \text{ Kips}$$

Q6

Step # 02 (Shear force Diagram)

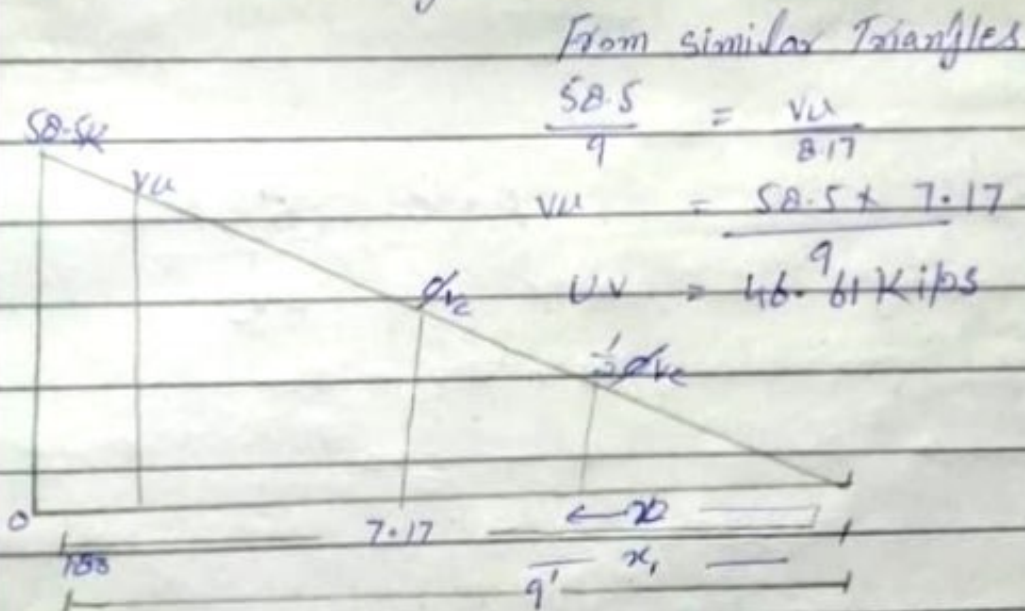
The required shear diagram will be



### Step # 3:-

Finding the value of critical shear " $V_u$ " and its location  $A_s$ , we know that critical shear is located at distance " $d$ " from face of support ( $d$ ) = 22" = 1.83

⇒ we will find values of critical shear at distance " $d$ " by use of similar triangles.



### Step # 04

Finding the values of " $\phi_{vc}$ " and  $\frac{1}{2} \phi_{vc}$ " and also its distance from zero shear to right side.

By formula.

$$\Rightarrow \phi_{vc} = \phi \times 2 \times \sqrt{f_c} \times b_w \times d$$

$$= 0.75 \times 2 \times \sqrt{4000} \times 14 \times 22 = 29219 \text{ lbs}$$

$$= 29.21 \text{ Kips}$$



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→ Location of  $\phi_{ve}$  by similar triangle

$$\frac{58.5}{9} = \frac{\phi_{ve}}{x_1} \Rightarrow \frac{58.5}{9} = \frac{29.21}{x_1}$$

$$\Rightarrow x_1 = \boxed{4.49'}$$

→ Similarly

$$\frac{1}{2} \phi_{ve} = \phi_{ve} \rightarrow \frac{29.21}{2} = 14.60 \text{ kips}$$

→ Location of  $\frac{1}{2} \phi_{ve}$  will be

$$\frac{58.5}{9} = \frac{14.60}{x_2}$$

$$\rightarrow 2.24$$

Step # 05 page 6

Finding the value of  $\phi_{vs}$   
by formula  $v_u = \phi_{vs} + \phi_{ve}$

$$\rightarrow \phi_{vs} = v_u - \phi_{ve}$$

$$= 146.61 - 29.21$$

$$= \phi_{vs} 117.4 \text{ kips}$$

Step # 06

Check on section adequacy  
by formula.

$$= \phi + 8 \times \sqrt{F_c} \times b_w \times d$$

$$= 0.75 \times 8 \times \sqrt{4000} + 14 \times 22 = 116877 \text{ lbs}$$

$$AS = \phi \times 8 \times \sqrt{F_c} \times b_w \times d > 0.9 \times 116.87 \text{ kips}$$

so section is adequacy

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Step # 07:-

check on maximum spacing for stirrups

By ACI formula,

$$= \phi \times 4 \times \sqrt{f_c} \times b_w \times d$$

$$= 0.75 \times 4 \times \sqrt{4000} \times 14 \times 22 = 58438 \text{ lbs}$$

$$= 58.43 \text{ Kips}$$

As  $\phi \times 4 \times \sqrt{f_c} \times b_w \times d > \phi V_u$

So maximum will be selected

from the following conditions

1 =  $S_{max} = 24"$

2 =  $d/2 = 22/2 = 11"$

3 =  $S_{max} = \frac{A_v \times F_y}{0.75 \times \sqrt{f_c} \times b_w}$

Here we are

using #3 stirrup

$$\text{dia} = \left(\frac{3}{8}\right) = 0.375$$

$$\text{So each } \frac{\pi (0.375)^2}{4} = 0.11 \text{ in}^2$$

for 2-legged stirrups

$$\rightarrow \text{area} \times 2$$

$$\rightarrow 0.11 \times 2 = 0.22 \text{ in}^2$$

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page

07

$$3: S_{max} = \frac{0.22 \times 60000}{0.75 \times \sqrt{14000 + 14}} = 14.87$$

$$4: S_{max} = \frac{A_u \times F_y}{50 \times b_w} = \frac{0.22 \times 60000}{50 \times 14} = 18.86$$

From above 4 conditions.

~~least~~ least value of spacing for #3, 2 legged stirrup will be selected as

$$S_{max} = 11$$

**Step # 08**

stirrup

stirrup spacing from/at critical section will be

By formula.

$$S = \frac{\phi \times A_u \times F_y \times d}{V_u - \phi V_c} = \frac{0.75 \times 0.22 \times 60 \times 12}{46.61 - 29.21}$$

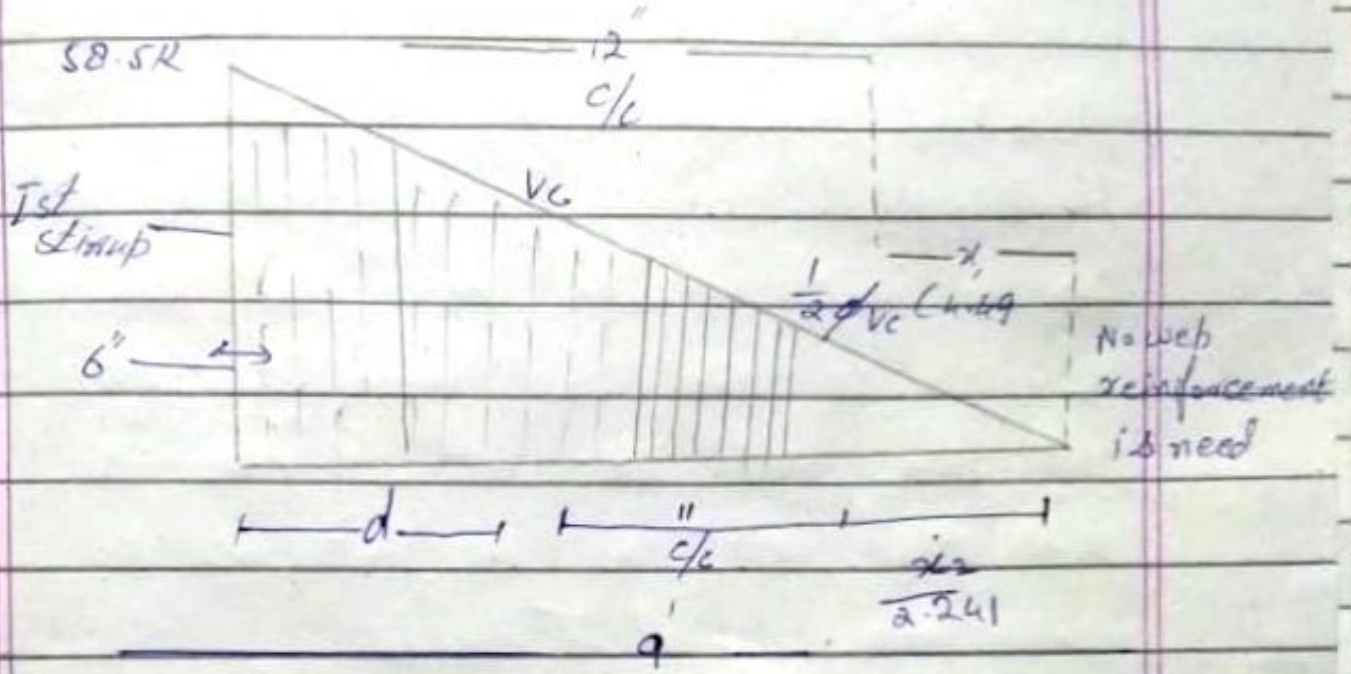
$$S = 12.5 \approx 12$$

so 12 c/c

**Step # 09**

Final sketch will be

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As first stirrup from face of support

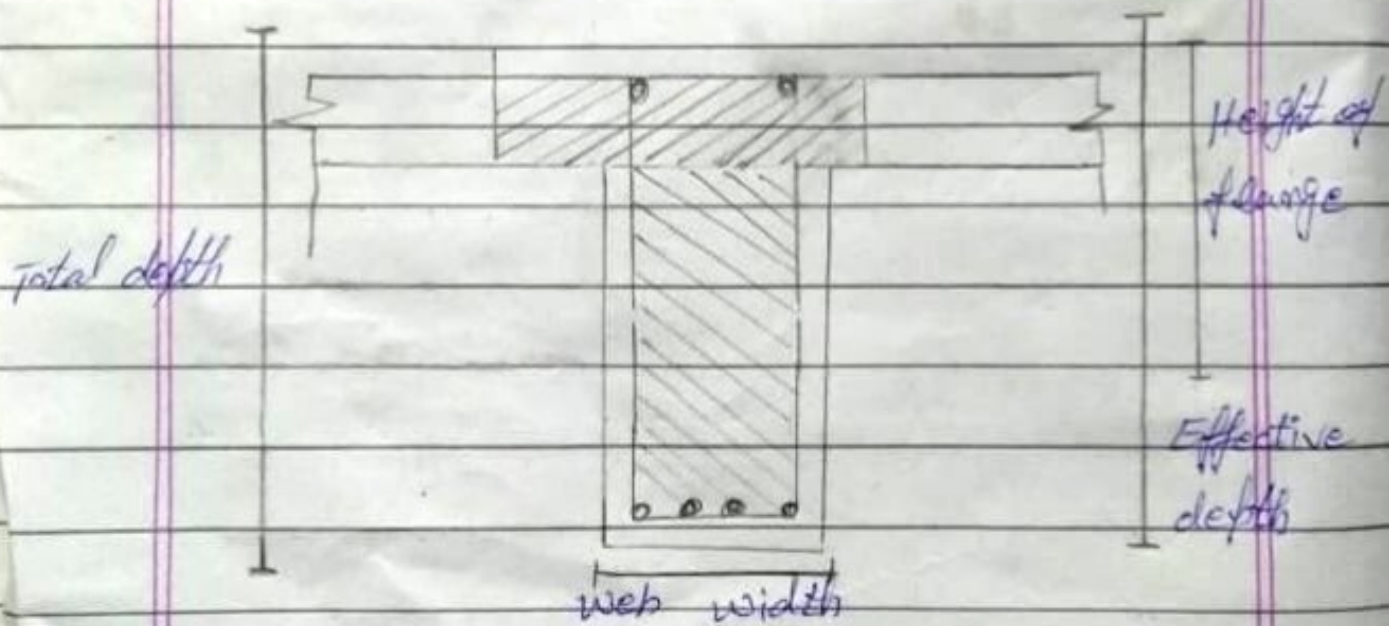
$$\frac{b}{2} = \frac{12}{2} = b''$$

### Question No. 03

Define both the T-beam and L-beam with the help of diagram. Also explain flexural analysis of T-Beam

#### T-Beam :-

→ in most of the reinforced concrete structures are cast monolithically with the slab so in this case the beam that act as an intermediate beam are called T-beams.



→ because of their T-shape these beams are called T-beams

→ It is provided at the center of the slab to resist the

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loads.

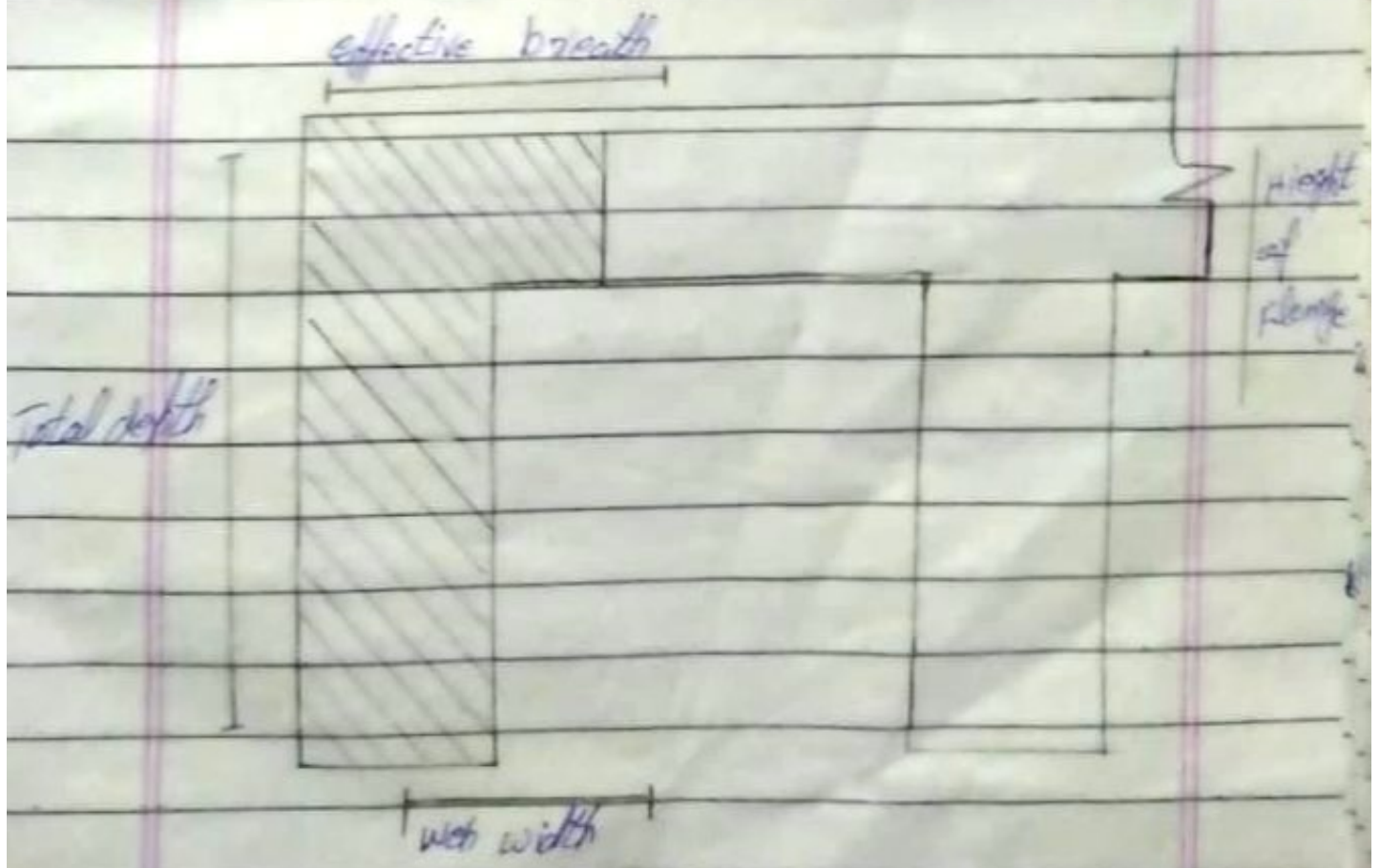
→ The upper most area of the beam attached to the slab is called flange.

→ The bottom rectangular portion of the beam is called web of beam.

L-Beam:

→ L-shaped structure that is in contact with the slab and present on the corner of the floor is called L-beam.

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→ L-Beams are also called edge beams

→ it is always provided at the corners of this lab.

→ L-Beams are typical floor beams because of their reduced overall structural depth the beams are in prestressed or reinforced concrete.

### Flexural Analysis of T-Beam:-

flexural analysis of T-Beam consists of the following steps

(1) For finding the ultimate factored moments we use the following

Formula:

$$M_u = \frac{W_u \times L^2}{8} \quad \because \quad \begin{aligned} W_u &= \text{Total factored load} \\ L &= \text{Total span of the beam} \end{aligned}$$

(2) Effective width ( $b_e$ ) for T-beam is calculated as:

1.  $16(h_f) + b_w$

2.  $c/\text{distance}$

3. span  $l_d$

4.  $\frac{CTS}{2} = b_w$

$\left( \begin{aligned} H_f &= \text{height of flange} \\ CTS &= \text{clear transverse span} \end{aligned} \right)$

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value from above formulas  
is c/s distance is given then there is  
no need of  $a = \frac{CTs}{2} + bw$

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3. Checking whether rectangular or  
T-beam Analysis is required.

(i) if  $a > hf \rightarrow$  special analysis is  
required

(ii) if  $a < hf \rightarrow$  Rectangular beam  
analysis is required

where

( $a =$  depth of compression block)  
( $hf =$  Height of flange)

(4) For finding area of steel, we  
have to use

$$A_{st} = \frac{M_u}{d \times f_y \times \left( d - \frac{a}{2} \right)}$$

where

$$a = \frac{A_{st} \times f_y}{0.85 \times F_c + bw}$$

$f_y =$  Strength of Reduction factor  
 $d =$  Effective depth  
 $a =$  compression block depth  
 $bw =$  web width of beam

(5) For checking the range of reinforcement  
Ratio

$$S_{max} = 0.85 \times B \times \frac{F_c}{F_y} \times \left( \frac{e_u}{e_u + e_y} \right)$$



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$$\rho = \frac{A_{st}}{b \cdot d}$$

6. Formula for finding No of bars required is

$$\text{No of bars} = \frac{\text{Area of steel}}{\text{Area of single bar}}$$

7. For checking minimum width for bars accommodation

$$b_{min} = 2(\text{clear cover}) + 2(\text{dia of stirrups}) + \text{No of bars (dia of bars)} + \text{spacing (dia of bars) b/w bars}$$

8:- Design moment is given by

$$M_d = \rho \cdot F_y \cdot A_{st} \cdot (d - \frac{a}{2}) \rightarrow \text{if } a < h_f$$

$$M_d = \rho \cdot F_y \cdot [A_s \cdot F_y \cdot (d - \frac{h_f}{2}) + (A_s - A_{st}) \cdot F_y \cdot (d - \frac{a}{2})] \rightarrow \text{if } a > h_f$$

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Question No. 04

What is difference b/w Case-1 and Case-2 design of T-beam

Case-I:-

From the figure

$a < h_f$

So in the case

Rectangular beam

Analysis is required

So,

The design moment

formula will be

$$M_d = \phi_x + \phi_y \times A_{ST} \times (d - a/2)$$

Case-2:-

From the figure

$a > h_f$

So in this special

beam analysis i.e.

T Beam Analysis

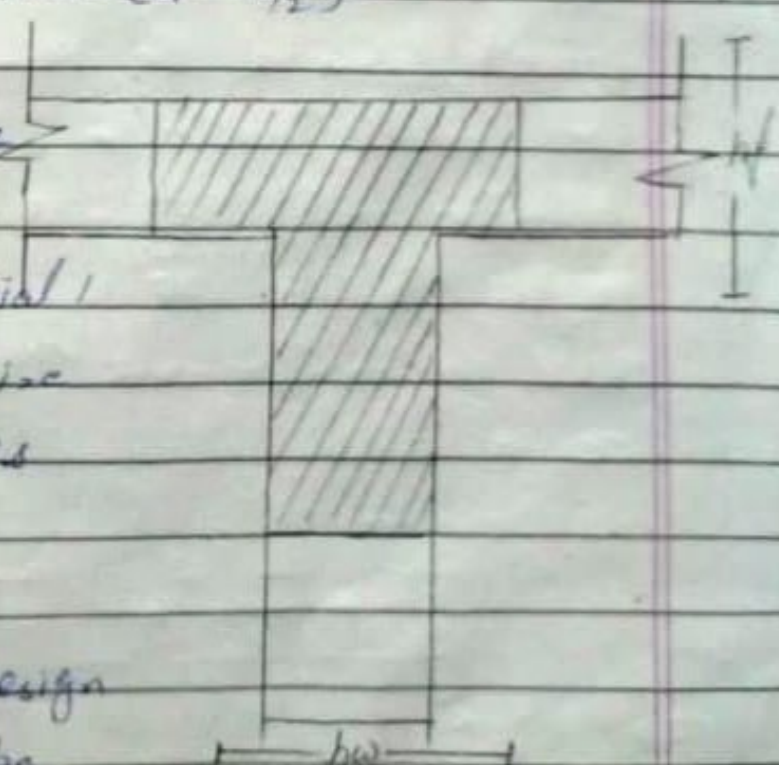
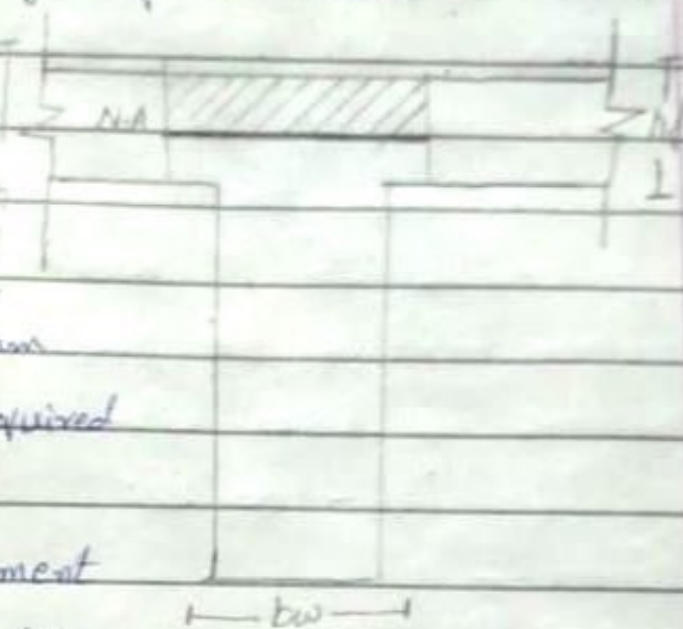
is required

So

The required design

moment will be

$$M_d = \phi_x \left[ a_s \times F_{yt} \times d \left( \frac{d - h_f}{2} \right) + (A_s - A_{ct}) F_{yt} \left( \frac{d}{2} \right) \right]$$



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Q.No 05

A floor system consist of 3.5 corrugated slab supported by 16 simple span spaced at 9' c/c the beam having web width of 16" and effective depth of 18" and total height is 23".

calculate the necessary flexural reinforcement if the factored applied moment is 5800 Kip-inch use  $f_c = 3 \text{ Ksi}$  and  $f_y = 60 \text{ Ksi}$

Given:-

Height of flange ( $h_f$ ) = 3.5"

c/c distance = 9'

Length / span of the beam = 16'

web width ( $b_w$ ) = 16"

effective depth ( $d$ ) = 18"

Height ( $h$ ) = 23"

Total factored moment ( $M_u$ ) = 5800 Kip inch

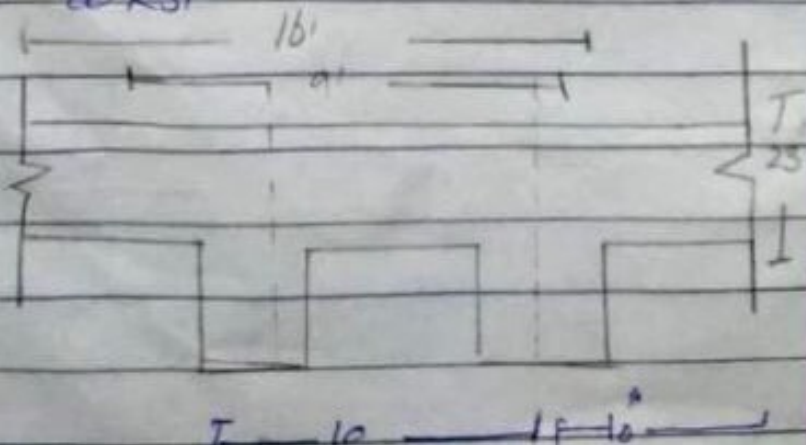
$f_c = 3 \text{ Ksi}$

$f_y = 60 \text{ Ksi}$

Sol:-

$h_f = 3.5$

↓



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step # 1

calculate the effective width ( $b_e$ ) for T beam

1.  $16(h_f) + b_w = 16(3.5) + 10 = 66$

2.  $\frac{1}{4}$  distance in  $9 \times 12 = 108$

3.  $\frac{\text{span}}{4} = \frac{16 + 12}{4} = 48$

selecting the least value of  $b_e$  as

$b_e = 48$

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step # 2:

check whether Rectangular or T beam Analysis is required.

Trial # 1 let  $a = h_f = 3.5$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{5800}{0.90 \times 60 \times (18 - 3.5)} = 6.61 \text{ in}^2$$

Trial # 02  $a = \frac{A_{st} \times f_y}{0.85 \times F_c \times b_e}$

$$a = \frac{6.61 \times 60}{0.85 \times 3 \times 48} = 3.2$$

and  $A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)}$

so Rectangular beam design is required

Trial # 03 :  $a = 3.21$

and  $A_{st} = \frac{5800}{0.90 \times 60 \times (18 - \frac{3.21}{2})} = 6.55 \text{ in}^2$

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So Area of steel is  $6.55 \text{ in}^2$

Step # 03:-

check Slenderness ratio

$$\Rightarrow S_{max} = 0.85 \times \frac{F_c'}{F_y} \left( \frac{E_u}{E_u + E_t} \right)$$