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ID :- 7462

Subject :- PIRCD-I

Program :- BEC

Exam :- Final terms

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Q #02:

page #01

Ans:

A simply supported rectangular beam 16" wide ---
Draw a sketch of your final diagram:

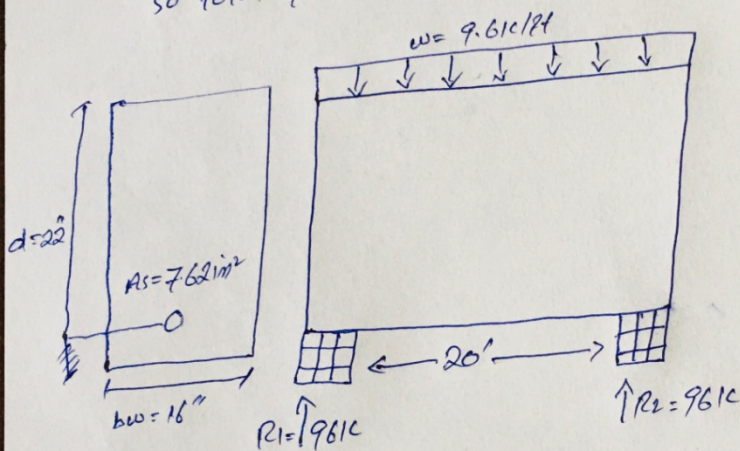
Sol:

First we find the unit load of beam.

$$So \quad b \times r_c$$

$$= 16/12 \times 150 = 200 \text{ lb/ft} = 0.2 \text{ k/ft}$$

$$So \text{ total factored load} = 9.4 + 0.2 = 9.6 \text{ k/ft}$$



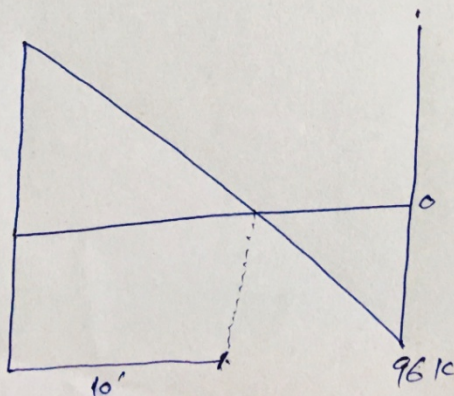
Step #01:

Find the value of R_1 & R_2

$$\text{Total load} = 9.6 \times \frac{20}{2} = 96 \text{ k}$$

Step #02 draw a shear force diagram:

S.F.D
(1 cop)

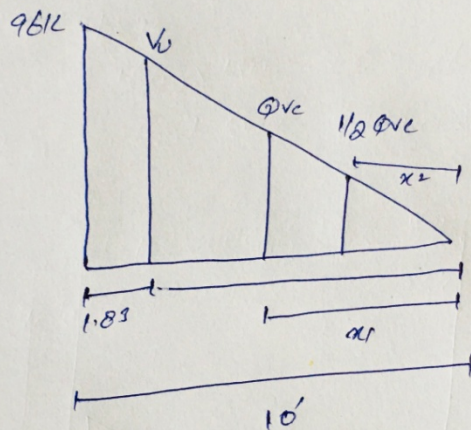


page #02

step #03

Find the value of critical stress " v_u " on its location.

As we know that critical section is located of distance " d " from face of support = $a = 22" = 1.83'$
 value of critical shear of distance " d " by similarity of triangles



from similar Δ 's $96/10 = \frac{v_u}{8.17} = 78.432 \text{ kips}$

step #4

Find the value of (ϕv_c) and $1/2 \phi v_c$ and also its distances from zero shear to right side

$$\phi v_c = \phi \times 2 \times \sqrt{f_c'} \times b_w \times d = \frac{0.75 \times 2 \times \sqrt{4000} \times 16 \times 22}{1000}$$

=> 33.40 k

location of ϕv_c by similarity of Δ 's

$$96/10 = \frac{33.40}{x_1} = 3.47' \quad x_1 = 3.47'$$

$$\text{Now } 1/2 \phi v_c = \frac{33.40}{2} = 16.70 \text{ k}$$

page #05

$$\text{location of } 1/2 \phi V_c = 96/10 = 16.70/x_2 = x_2 = 1.73'$$

step #05

value of ϕV_s ($V_u = \phi V_s + \phi V_c$)

$$\phi V_s = V_u - \phi V_c = 76.80 - 33.40 = 43.40 \text{ k}$$

step #6:

check on section adequacy

$$\begin{aligned} \phi \times 8 \times \sqrt{f_c' \times b_w \times d} &= 0.75 \times 8 \times \sqrt{4000 \times 16 \times 22} \\ &= 133.57 \text{ k} \end{aligned}$$

As $\phi V_s < \phi 8 \sqrt{f_c' b_w d} \Rightarrow$ ft means section is adequate.

step #7

check on maximum spacing for stirrups

$$\begin{aligned} \phi \times 4 \times \sqrt{f_c' \times b_w \times d} &\Rightarrow 0.75 \times 4 \times \sqrt{4000 \times 16 \times 22} \\ &= 66.79 \text{ kip} \end{aligned}$$

$$\text{As } \phi 4 \sqrt{f_c' b_w d} > \phi V_s = 43.40 \text{ k}$$

So max-spacing will be selected from following four conditions.

$$1) s_{\text{max}} = 24'' \quad 2) d/2 = 22/2 = 11''$$

$$3) s_{\text{max}} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c'} \times b_w} = 17.46''$$

$$4) s_{\text{max}} = A_v \times f_y / s_u \times b_w = 16.50''$$

From above shear condition - best value of spacing for #3, 2 legged stirrups will be selected.

$$S_0 > S_{max} = 11" c/c$$

Step #8:

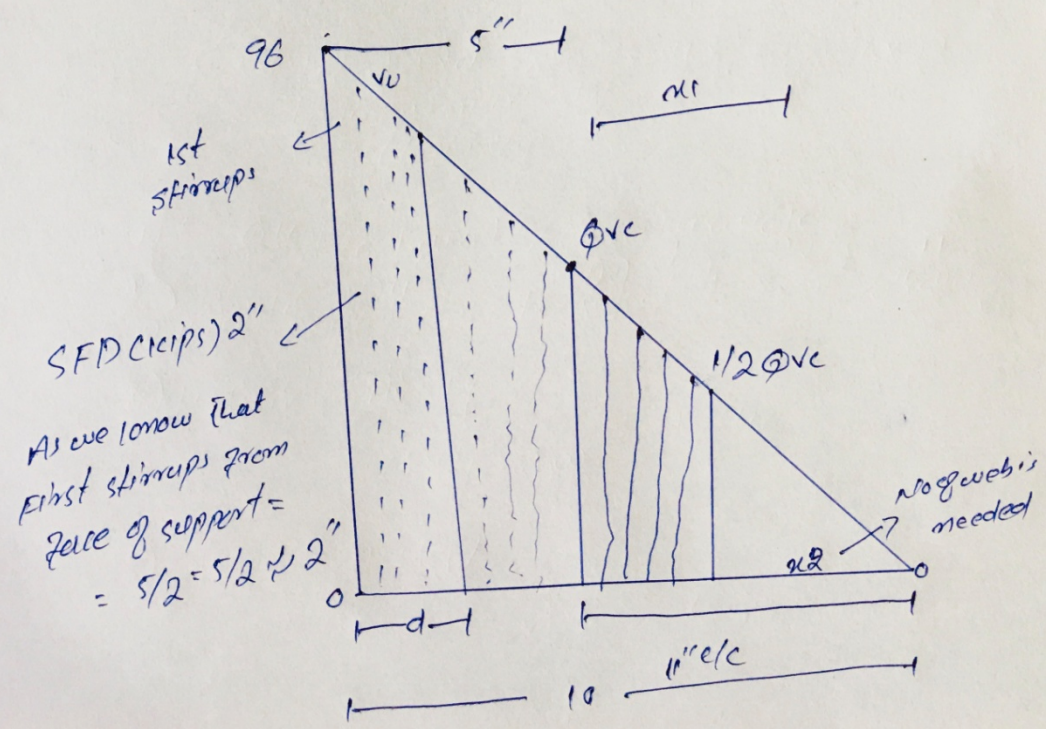
spacing of stirrups from at critical section

$$S = \frac{\phi \times A_v \times f_y \times d}{V_u - \phi V_c} = \frac{0.75 \times 0.22 \times 60 \times 22}{76.80 - 33.44}$$

$$S = 5" c/c$$

Step #9:

Final sketch.



Q # 1

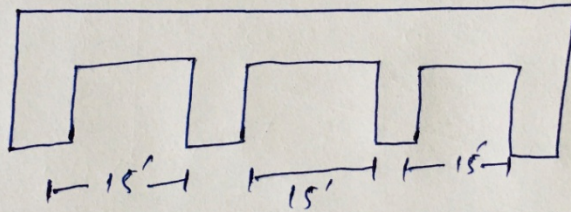
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Ans

Given data:

- (*) 3 equal spans concrete slab
- (*) clear span b/w supports = 15 ft
- (*) Factored live load = 160 lb/ft^2
- (*) Service floor finish load = 20 lb/ft^2
- (*) $f_c' = 4000 \text{ psi}$
- (*) $f_y = 40 \text{ ksi}$

Sol:



Step # 01:

Minimum Thickness

Formula

$$t_{\min} = L/28 = 15/28 = 6.4 \text{ ft} \approx 6.5''$$

As $f_y = 40 \text{ ksi}$

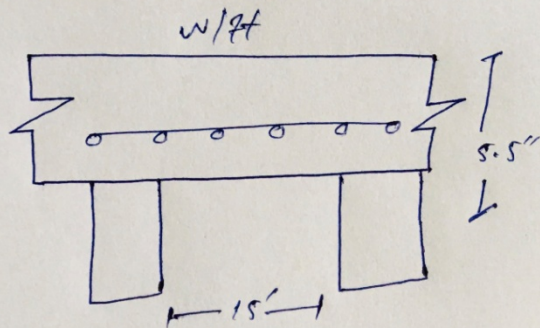
So we will multiply a factor with this thickness

$$\text{Factor} = (0.4 + f_y/100) = (0.4 + 40/100) = 0.8$$

The minimum thickness will be 6.5×0.8

$$t_{\min} = 5.2 \text{ ft} \approx 5.5''$$

Step #2:



Formula

$$d = t - \text{clear cover} - 1/2 (\text{dia of main bars})$$

$$= 5.5 - 0.75 - 1/2 (5/8)$$

$$d = 4.5''$$

Step #03:

self wt of slab

$$t/12 + \gamma_{\text{concrete}}$$

$$\Rightarrow 5.5/12 \times 150 = 68.75 \text{ lb/ft}^2$$

Step #04:

$$\text{factored live load} = 160 \text{ lb/ft}^2$$

$$\text{so the factored dead load will be } D.L = 1.2(80 + 68.75)$$

$$= 106.5 \text{ lb/ft}^2$$

$$\text{Total factored load} = D.L + L.L \Rightarrow 106.5 + 160$$

$$\Rightarrow 266.5 \text{ lb/ft}^2$$

$$\Rightarrow 0.265 \text{ k/ft}^2$$

Step #05: ultimate moment:

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (15)^2}{8} \times 12$$

$$= 89.94 \text{ kip-inches}$$

Step # 6:

Area of steel for main bars by Trial and repeat method.

Trial # 01:

let depth of compression block

$$a = 0.2 \times t = 0.2 \times 5.5 = 1.1''$$

$$A_{st} = \frac{mV}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - 1.1/2)} = 0.632 \text{ in}^2$$

Trial # 02:

$$a = \frac{A_{st} \times f_y}{0.85 \times f_c \times b} = \frac{0.632 \times 40}{0.85 \times 4 \times 12} = 0.57''$$

Step # 07:

Area of steel distribution reinforced.

Formula

$$A_{min} = 0.002 \times b \times t \quad (\text{for grade 40 steel})$$

$$= 0.002 \times 12 \times 5.5 = 0.132 \text{ in}^2$$

Step # 08: spacing for main bars.

$$\text{spacing} = \frac{A_0}{A_{st}} \times 12 \quad \text{use \#6 bars dia} = (6/8)''$$

$$\text{Area} = \pi/4 (6/8)''^2 = 0.442 \text{ in}^2$$

Step # 09:

Spacing for distribution bar

$$\text{spacing} = \frac{A_0}{A_{st}} = \text{we use \#5 bars}$$

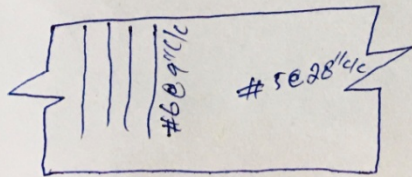
$$\text{dia} = 5/8)'' \quad \text{Area} = \pi/4 (5/8)''^2 = 0.31 \text{ in}^2$$

$$\text{spacing} = \frac{0.31}{0.132} \times 12 = 2.81'' \rightarrow 28'' \text{ c/c}$$

Step # 10:

Find steel:

$f_c = 4 \text{ ksi}, f_y = 40 \text{ ksi}$. main steel #6 at 9" c/c
 o distribution steel #5 at 28" c/c



Q #03:

page #8

sol:

Step #1: Find gross area of concrete.

$$A_g = b \times b \text{ (since it's square tied column)}$$

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

Step #2: Find the area of steel.

Since $A_s = 5\%$ of A_g

$$= 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

Step #3: ultimate load carrying capacity.

$$P_u = \phi \times 0.80 \times \{0.85 \times f'_c \times (A_g - A_{st}) + A_s \times f_y\}$$

$$= 0.65 \times 0.80 \{0.85 \times 4 \{144 - 7.2\} + 7.2 \times 60\}$$

$$P_u = 466.50 \text{ k}$$

Step #4:

sketch & design of ties (c/c to distance)

from the below value we chose the least value of all these

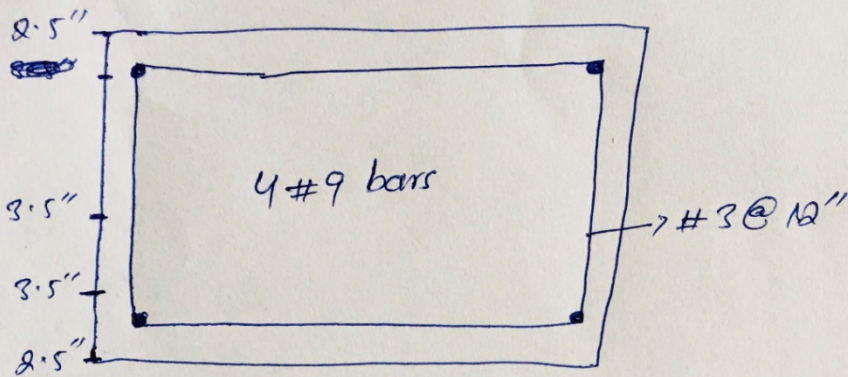
(1) $16 \times \text{dia of long bar} = 16 \times 9/8 = 18''$

(2) $48 \times \text{dia of tie bar} = 48 \times 3/8 = 18''$

(3) least column dimension = 12''

so c/c distance btw ties = 12''

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→ since it's a tied square column so there is no spiral stirrup used. the stirrup used is of rectangular shape due to the set spacing of the structure thus we will use tie stirrups - instead.

Q#04

page #10

Ans:-

Sol:-

Step #1:-

$$\text{let } h = 24''$$

Step #2

$$\begin{aligned} \text{Total wt} &= \text{wt of soil} + \text{wt of RC} \\ 3 + 120 + 2 \times 150 &= 660 \text{ psf} = 0.660 \end{aligned}$$

Step #03:-

Effective Bearing capacity.

$$q_e = q_u - u = 2.50 - 0.660$$

$$q_e = 1.84 \text{ ksf}$$

Step #04:-

Required Area for foundation

$$\text{Area} = \frac{S.L}{q_c} = \frac{100 + 120}{1.84} = \text{Area} = 119.56 \text{ ft}^2$$

Step #05:-

Since foundation is square

$$\text{Area} = B \times B = 119.56$$

$$B \cong 119.56''$$

Step #06:-

$$q_{VP} = \frac{\text{Factored load}}{(B)^2}$$

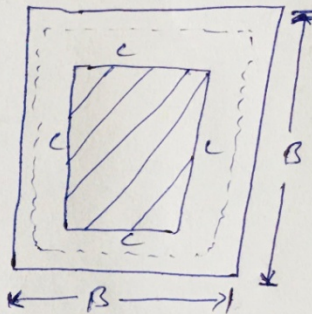
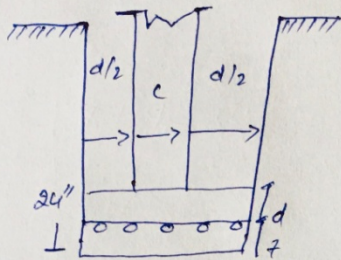
$$\Rightarrow \frac{1.2 \times 100 + 1.6 \times 120}{(119.56)^2}$$

$$q_{VP} = 0.02114 \text{ /ft}^2$$

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Step # 7: punching shear

$$b_o = 4(c+d)$$



$$d = h - \text{clear cover} - \text{dia of bar} - 1/2 \times db$$

$$d = 24 - 3 - 1 - 1/2 + 1 = 19.5''$$

$$b_o = 4(16 + 19.5) = 142''$$

Step # 08

$$\Rightarrow V_{u2} = \rho V_p \times \left[(13^2 - (c+d)^2) \right]$$

$$\Rightarrow 0.021 \left[(11956) - \frac{(16+19.5)^2}{2} \right]$$

$$\Rightarrow V_{u2} = 300$$

Step # 9:

$$\phi V_c / P = \phi \times 4 \times \sqrt{f_c'} \times b_w \times d$$

$$\Rightarrow 0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5$$

$$\phi V_c / P = 525.38$$

Step # 10:

Beam shear / one way shear check

$$V_u = 2.0P \times 13^2 \left\{ 13/2 - c/2 - d \right\}$$

$$V_u = 2.58 \times 11 \times \left\{ 11/2 - 16/2 - 19.5 \right\}$$

$$V_u = 90.951k$$

Step # 11: self shear capacity

$$\phi V_c = \phi \times 2 \times \sqrt{f_c} \times b \times d$$

$$\Rightarrow \frac{0.75 \times 2 \times \sqrt{4000} \times (11 - 16)}{1000}$$

$$\Rightarrow 110.041k > V_u = 90.951k$$

Step # 12: ultimate ~~moment~~
moment

$$M_u = \frac{2.0P \times 11^2}{8} \times (13 - c)^2 = \frac{2.58 \times 11}{8} \times \frac{(11 - 16)^2}{2}$$

$$M_u = 331.491k' = 3977.931k''$$

Step # 13:

Area of steel for main bars
by trial and repeat method.

$$\text{Trial \#01 let } a = 0.2 \times h = 0.2 \times 24 = 4.8''$$

$$A_s = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{3977.93}{0.90 \times 60 \times (11 - 4.8/2)}$$

$$= 8.56 \text{ in}^2$$

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Trial # 02:

$$a = \frac{A_s \times f_y}{0.85 \times f_c \times b} = \frac{8.56 \times 60}{0.85 \times 3 \times 12 \times 11} = 1.53''$$

$$A_s = \underline{3977.93}$$

$$0.90 \times 60 \times (11 - 1.53/2) = 7.197 \text{ m}^2$$

Trial # 03

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$A_s = \underline{3977.93}$$

$$0.90 \times 60 (11 - 1.28/2) = 7.11 \text{ m}^2$$

$$\text{thus Area} = \boxed{7.11 \text{ m}^2}$$

Step # 14:

Check the min reinforcement by the following
03 method.

$$A_{s \text{ min}} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24$$

$$\boxed{A_{s \text{ min}} = 5.76 \text{ m}^2}$$

$$A_{s \text{ min}} = \frac{200}{f_y} \times B \times d = \frac{200}{60000} \times (11 \times 12) \times 19.5$$

$$\boxed{= 8.58 \text{ m}^2}$$

$$A_{s \text{ min}} = 3 \times \sqrt{\frac{f_c'}{f_y}} \times B \times d = 3 \times \sqrt{\frac{3000}{60000}} \times 11 \times 12 \times 19.5$$

$$\boxed{= 7.05 \text{ m}^2}$$

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From the above value greater value will be selected thus

$$A_{smin} = 8.58 \text{ in}^2$$

step # 15:

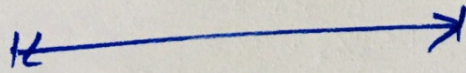
using #8 bars

$$A_b = 0.785 \text{ in}^2$$

$$\text{No of bars} = A_s / A_b = 8.58 / 0.785$$

$$= 10.92 \approx 11 \text{ bars in each}$$

direction



The End
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