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Section: A

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Paper: PRCD-1

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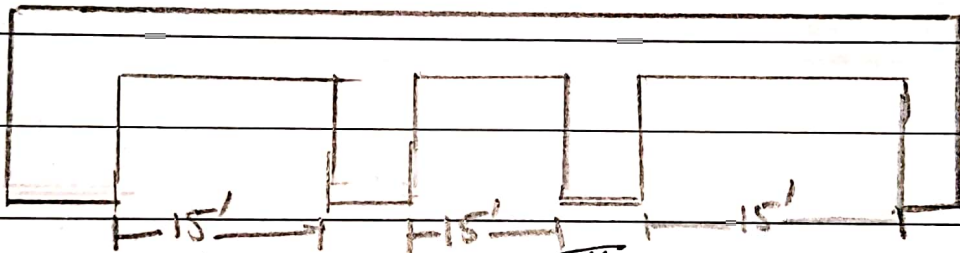
(Question-01)

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Given data:-

- ⇒ 3 equal spans Concrete Slab.
- ⇒ $f'_c = 4000 \text{ psi}$
- ⇒ $f_y = 40 \text{ ksi}$
- ⇒ clear span b/w supports = 15 ft
- ⇒ Factored Live load = 160 lb/ft^2
- ⇒ Service Floor finish load = 20 lb/ft^2

Solution:-



Step #1 (Minimum Thickness):-

By using formula

$$t_{\min} = L/28$$

$$\Rightarrow 15/28$$

$$\Rightarrow 6.4 \text{ ft} \approx 6.5 \text{ ft}$$

As $f_y \rightarrow 40 \text{ ksi}$

So we will multiply a factor with this thickness.

$$\text{Factor} = \left(0.4 + \frac{f_y}{100} \right)$$

$$= \left(0.4 + \frac{40}{100} \right)$$

$$= 0.8$$

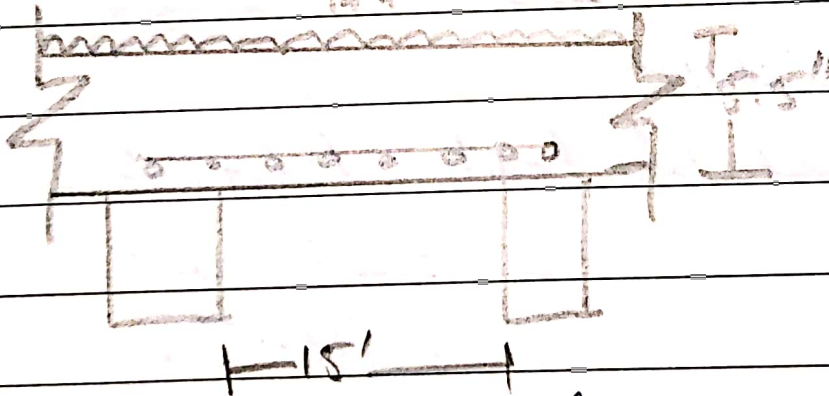
Hence the minimum thickness will be

$$6.5 \times 0.8$$

$$t_{\min} = 5.2 \text{ to } 5.5''$$

Step #2:-

(Effective Depth)



By using formula

$$d = t - \text{clear cover} - \frac{1}{2} (\text{dia of main bar})$$

$$= 6.5 - 0.75 - \frac{1}{2} (5/8)$$

$$d \approx 4.5''$$

Step # 03: (self wt. of slab)

By using formula

$$\frac{t}{12} \times \text{Concrete}$$

$$= \frac{5.5}{12} \times 150$$

$$\Rightarrow 68.75 \text{ lb/ft}^2$$

Step # 04: - (Total Factored Load)

Factored live load = 160 lb/ft²

So the factored dead load will be

$$D.L = 1.2(20 + 68.75)$$

$$= 106.5 \text{ lb/ft}^2$$

Total factored load = D.L + L.L

$$= 106.5 + 160$$

$$= 266.5 \text{ lb/ft}^2$$

$$= 0.2665 \text{ K/ft}^2$$

Step # 5: - (Ultimate Moment)

By using formula

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (15)^2 \times 12}{8}$$

$$= 89.94 \text{ kip-inches.}$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times \left(\frac{45 - 0.5}{2} \right)} = 0.59 \text{ in}^2$$

So we will use $A_{st} = 0.59 \text{ in}^2$

"Step # 7" :-

Area of steel for distribution reinforcement:

By using formula

$$A_{min} = 0.002 \times b \times t \rightarrow (\text{for Grade 40 steel})$$
$$= 0.002 \times 12 \times 5.5 \Rightarrow \boxed{0.132 \text{ in}^2}$$

Step # 8 :-

Spacing for main bars.

By formula

$$\text{Spacing} = \frac{A_b \times 12}{A_{st}}$$

We use #6 bar dia = $(6/8)''$

$$\text{Area} = \frac{\pi}{4} (6/8)^2 = 0.442 \text{ in}^2$$

"Step # 9" :-

Spacing for distribution bars.

$$\text{Spacing} = \frac{A_b}{A_{st}}$$

We use #5 bars so
 $dia = (5/8)"$, $Area = \frac{\pi}{4} (5/8)^2 = 0.31 in^2$

$$Spacing = \frac{0.31 \times 12}{0.132}$$

$$= 2.81" \approx 28" c/c$$

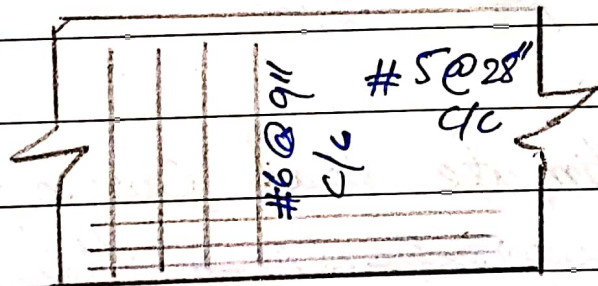
Step #10:-

Find Sketch

$$f'_c = 4 \text{ ksi}, f_y = 40 \text{ ksi}$$

Main steel #6 at 9" c/c

Distribution steel #5 at 28" c/c



Q. No (02)

Sol:-

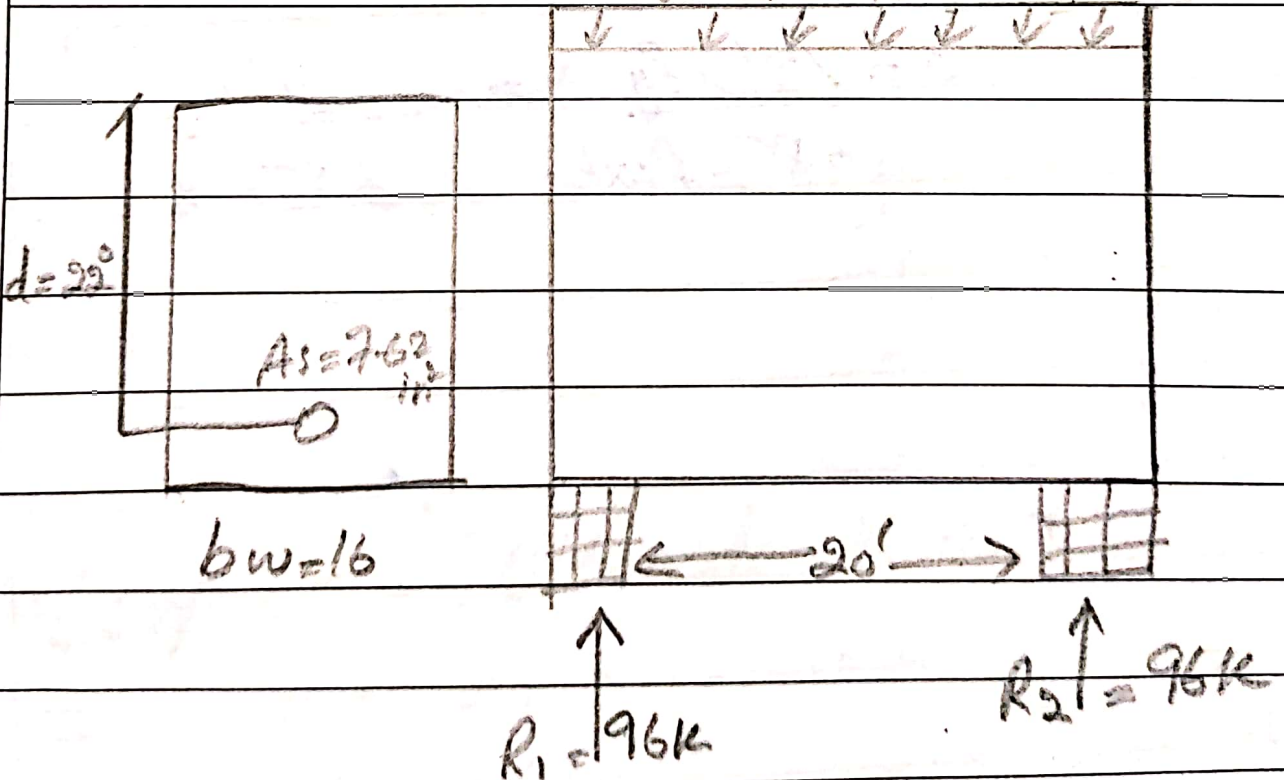
First of all find the unit load of beam.

$$\text{So } b \times d_c = \frac{16 \times 150}{12}$$

$$\Rightarrow 200 \text{ lb/ft} = 0.2 \text{ k/ft}$$

$$\text{So total factored load} = 9.4 + 0.2 = 9.6 \text{ k/ft}$$

$w = 9.6 \text{ k/ft}$

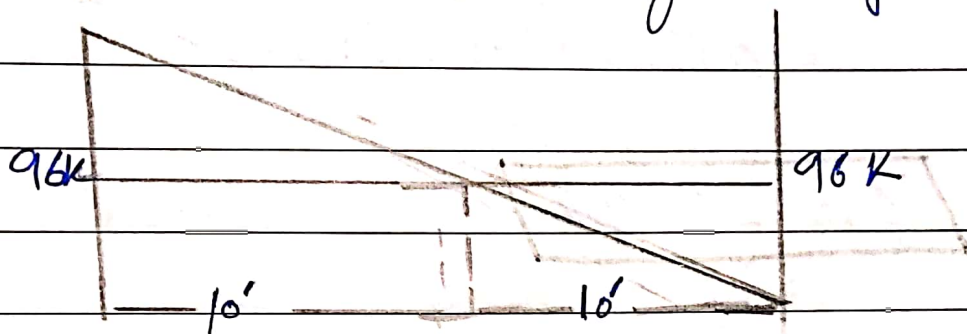


Step # 01: find values of R_1 and R_2

$$\text{Total loads} = 9.6 \times 20 = \frac{188}{2} = 96 \text{ k}$$

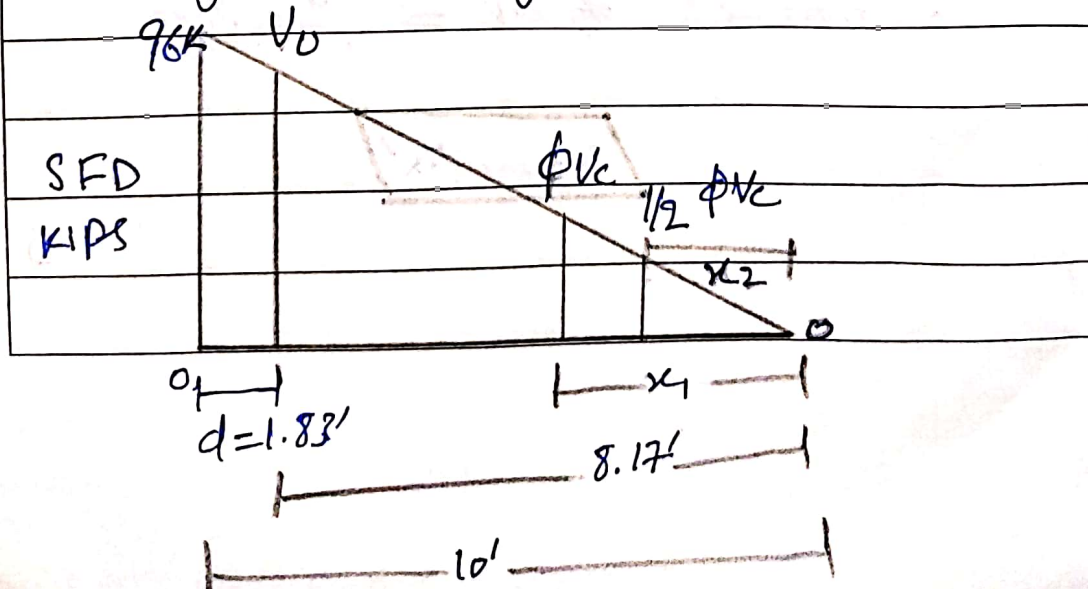
Step # 02 :-

Draw its shear force diagram



Step # 03 :-

find the value of critical shear " V_c " and its location. As we know that critical section is located at distance " d " from face of $-d = 22'' = 1.83'$ value of critical shear at distance " d " by similarity of triangles



Step# 04:-

find the value of ' ϕV_c ' and $\frac{1}{2} \phi V_c$ and also its distance from zero shear to right side.

$$\begin{aligned}\phi V_c &= \phi \times 2 \times \sqrt{f'_c} \times b \times d \\ &= 0.75 \times 2 \times \sqrt{4000} \times 16 \times 22 \\ &\quad 1000\end{aligned}$$

$$\boxed{\phi V_c = 33.40k}$$

Location of ϕV_c by Similarity of ' Δ_s '

$$\frac{9.6}{10} = \frac{33.40}{x_1} \Rightarrow \boxed{x_1 = 3.4}$$

Now

$$\frac{1}{2} \phi V_c = \frac{33.40}{2} = 16.70k$$

$$\text{Location of } \frac{1}{2} \phi V_c \Rightarrow \frac{9.6}{10} = \frac{16.70}{x_2}$$

$$\boxed{x_2 = 1.74''}$$

Step # 05:

Value of ϕV_s

$$(V_u = \phi V_s + \phi V_c)$$

So $\phi V_s = V_u - \phi V_c$

$$= 78.80 - 33.40$$

$$\boxed{\phi V_s = 45.03 \text{ k}}$$

Step # 06:

Check on Section adequacy

$$\phi \cdot 8 \sqrt{f'_c} \cdot b_w \cdot d = \frac{0.75 \cdot 8 \sqrt{4000} \cdot 16.22}{1000}$$

$$= 133.57 \text{ k}$$

As

$$\phi V_s < \phi 8 \sqrt{f'_c} \cdot b_w \cdot d$$

\Rightarrow It means section is adequate.

Step # 7

check on Maximum Spacing for

stirrups $\phi \cdot 4 \sqrt{f'_c} \cdot b_w \cdot d = \frac{0.75 \cdot 4 \sqrt{4000} \cdot 16.22}{1000}$

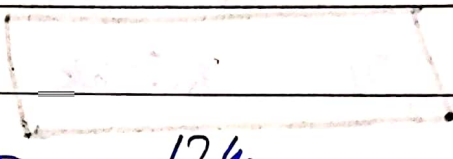
$$= 66.79 \text{ k}$$

As $\phi 4 \sqrt{f'_c} b_w d > \phi V_s = 43.40 k$

So Max Spacing will be selected from following four conditions

(1) $S_{max} = 24"$

(2) $\frac{d}{2} = \frac{22}{2} = 11"$



(3) $S_{max} = \frac{0.22 \times 60,000}{0.75 \sqrt{4500} \times 16} = 17.40$

(4) $S_{max} = \frac{0.22 \times 60,000}{50 \times 16} = 16.50"$

from above four conditions, least value of Spacing for #3, 2 legged stirrup will be selected

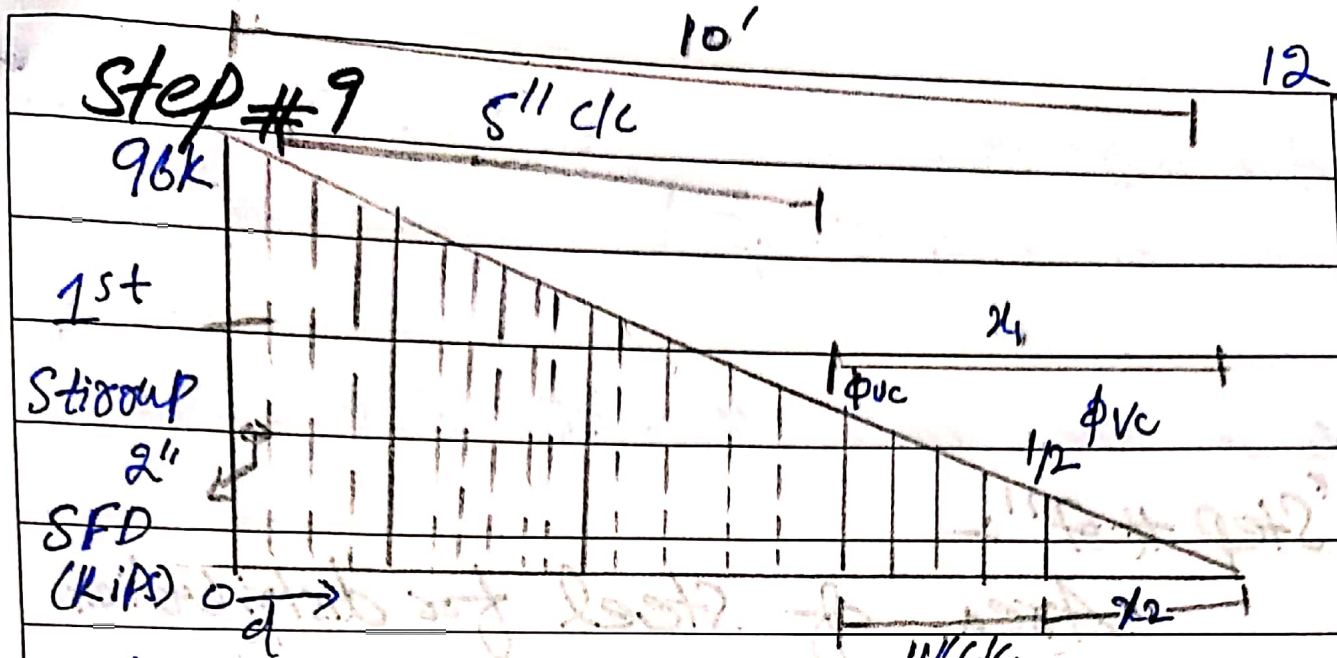
So $S_{max} = 11" c/c$

Step # 2

Spacing of stirrup from/at Critical Section

$$S = \frac{0.75 \times 0.22 \times 60 \times 22}{76.80 - 33.44}$$

$$S = 5" c/c$$



As we know that first stirrup from face of support

$$= \frac{s}{2} = \frac{5}{2} \approx 2.5$$

Q. No (03)

Ans:-

Step # 01

Finding gross area of concrete.

$$A_g = b \times b \text{ (since it is squared column)}$$

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

Step # 02

Find the area of steel

$$\text{Since } A_s = 5\% \text{ of } A_g$$

$$= 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

Step # 03:-

Ultimate load carrying capacity

$$P_u = \phi \times 0.80 \times [0.85 \times f'_c \times (A_g - A_s) + A_s \times f_y]$$

$$P_u = 0.65 \times 0.80 [0.85 \times 4 [144 - 7.2] + 7.2 \times 60]$$

$$P_u = 463.58 \text{ k}$$

Step # 04:-

Sketch and design of Ties (c/c to distance)

From the below value we choose

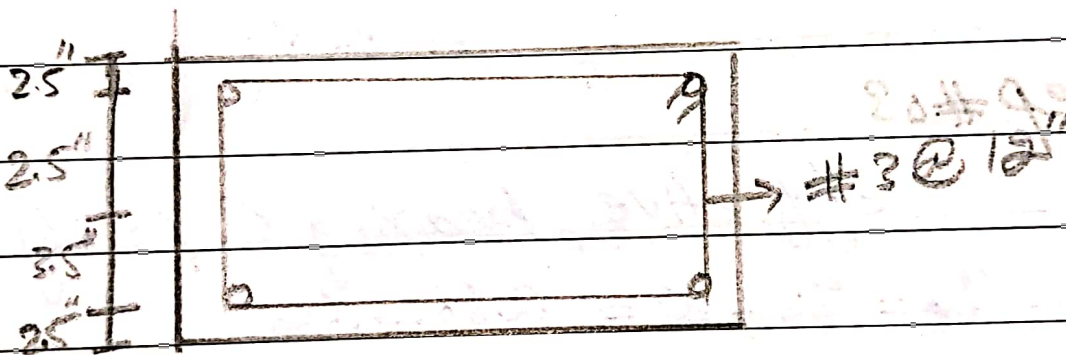
the cost value of all this.

$$(1) - 16 \times \text{dia of long bar} = 16 \times 9/8 \\ = 18''$$

$$(2) 48 \times \text{dia of Tie bar} = 48 \times 3/8 \\ = 18''$$

$$(3) \text{ least column dimension} = 12''$$

So c/c distance b/w ties = 12''



Since it is a tied square column
so there is no spiral stirrup used,
the stirrup used is of rectangular
shape due to the specification of
the structure thus we will use
tie stirrups instead.

Q.No # 4

Solution:-

Step # 1

$$\text{let } h = 24''$$

Step # 02:

$$\begin{aligned} \text{Total weight} &= \text{wt of Soil} + \text{wt of c/c} \\ &= 3 \times 120 + 2 \times 150 = 660 \text{ Psf} \\ &= 0.660 \end{aligned}$$

Step # 03

effective bearing Capacity

$$q_e = q_a - w = 2.50 - 0.660$$

$$q_e = 1.84 \text{ ksf}$$

Step # 04:

Required area for foundation

$$\text{Area} = \frac{\text{Service load}}{q_c}$$

$$= \frac{100 + 120}{1.84}$$

$$\boxed{\text{Area} = 119.59 \text{ ft}^2}$$

Step # 05

Since foundation is square

$$A_{req} = B \times B$$

$$= 119.56 \Rightarrow B \approx 11'$$

Step # 06: Upward bearing Capacity of Soil

$$q_{up} = \frac{\text{Factored Load}}{(B)^2}$$

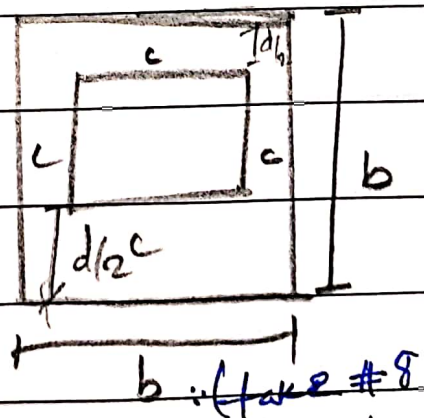
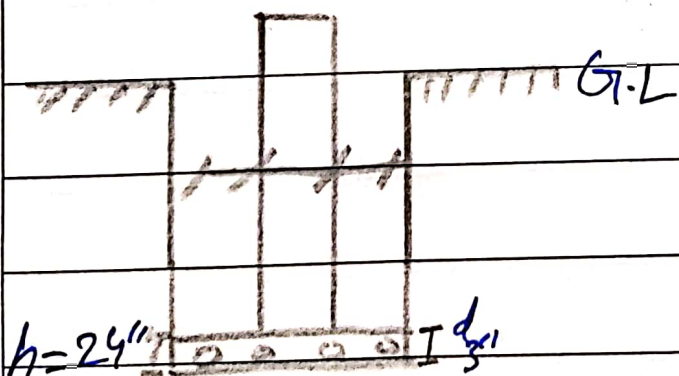
$$q_{up} = \frac{1.2 \times 100 + 1.6 \times 120}{11^2}$$

$$q_{up} = 2.58 \text{ K/ft}^2$$

Step 07:-

Punching Shear:

$$b_o = 4 \times (c + d)$$



$$d = h - c - \text{dia of bar} - 1/2 d_b$$

$$= 24 - 3 - 1 - 1/2(1) = 19.5''$$

bar dia =

$$\left(\frac{8''}{8} = 1''\right)$$

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$$b_o = 4 \times (16 + 19.5) \\ = 142''$$

Step #08

$$V_{v2} = q_{up} \times [B^2 - (C+d)^2]$$

$$= 0.021 \left[(19.56)^2 - \left(\frac{16 + 19.5}{12} \right)^2 \right]$$

$$V_{v2} = 300$$