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x ————— x ————— x —————

QNo: 1 Part (A)

Drag:-

A body which is immersed in a homogeneous fluid may be subjected to two kind of forces arising from relative motion b/w body and fluid. These forces are termed as drag and lift. If the forces parallel to the motion then its

is turned as drag force

These are two components.

→ Pressure Drag (F_p):

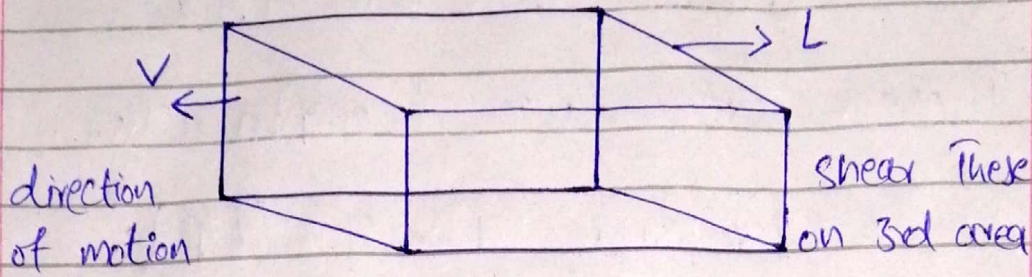
It is equal to integration of components in direction of components in direction of motion of all pressure forces exerted on surface of body.

$$F_p = C_p \int v^2/2 A \quad \text{where } C_p \text{ depends on shapes.}$$

Friction Drag (F_f):

It is equal to integration of components of shear stress along surface of body in direction of motion.

$$F_f = C_f \int v^2/2 BL$$



→ Friction Drag of boundary layer

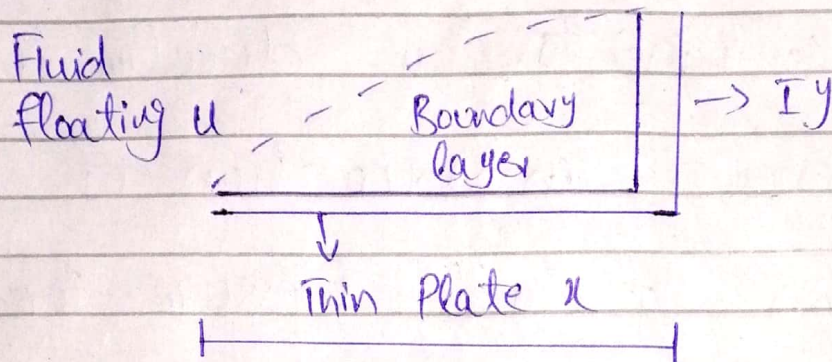
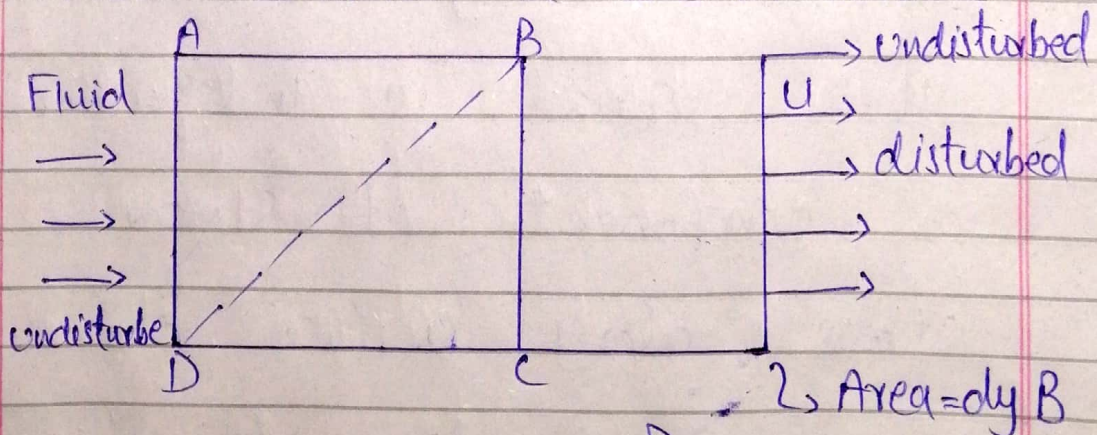


Fig shows growth of boundary layer along one side of smooth plastic inside the fluid.

Now consider a control volume.



where δ is thickness of boundary layer and u is undisturbed velocity
 Thus - F_x = drag (rate in momentum in x-direction)

$$\Delta P = P_{out} - P_{in}$$

Thus according to momentum.

$$\Sigma F = d/dt (P) = dm/dt$$

where $dm/dt = \rho Q$ Thus

$$F = \rho Q v$$

$$F = \rho A \cdot v \cdot v$$

$$F = \rho A v^2$$

$$DA \rightarrow \rho u (UB \rho)$$

$$BL \rightarrow \rho B \int u^2 - dy$$

$$\Delta B \rightarrow \rho u (UB \rho - B \rho \int u - dy)$$

Putting value

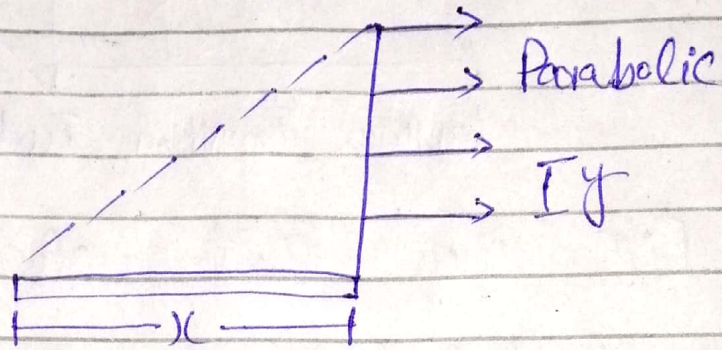
$$F_x = \rho B u^2 \rho \alpha \text{ "where } \alpha \text{ is friction of boundary layer"}$$

Now to find load wall shear stress. $T_0 = dF_x/B \cdot dx$ - area

$$F_x = \rho B u^2 \rho \alpha$$

$\tau_0 = \int u^2 \alpha ds/dx$ is general equation of shear stress.

→ Laminar Boundary layer:



Assume.

$$\eta = y/\delta \text{ or } y = \eta\delta$$

$$\text{Thus } u/u = f(\eta) \text{ or } u = uf(\eta)$$

In case of laminar flow.

$$\tau_0 = \mu (du/dy)$$

$$= \mu/\delta (du/dx) = \mu/\delta [df/d\eta(\eta)]$$

Solving the equation.

$$\tau_0 = \mu u \delta / \delta \rightarrow \textcircled{1}$$

As general equation is $\tau_0 =$

$$\int u^2 \alpha ds/dx.$$

Equating both equations.

$$\mu B/s = \int v^2 \alpha ds/dx$$

or

$$s ds = \frac{\mu B}{\rho u x} dx$$

Integrating the equation.

$$\frac{s^2}{2} = \frac{\mu B}{\rho u x} x + C$$

Now at $x=0$, $s=0$ Thus $C=0$

$$\frac{s^2}{2} = \frac{\mu B}{\rho u x} x$$

or

$$s = \frac{\sqrt{2\mu B x}}{\sqrt{\rho u x}} \quad \text{or} \quad \sqrt{\frac{2B}{\alpha}} \cdot \frac{\sqrt{\mu x}}{\sqrt{u}}$$

xing and ÷ing by 'x'

$$s = \frac{\sqrt{2B}}{\sqrt{\alpha}} \cdot \frac{\sqrt{\mu x}}{\sqrt{\rho u}} \cdot \frac{x}{\sqrt{x} \cdot \sqrt{x}}$$

where;

$$A = 0.135$$

$$B = 1.63$$

$$R_x = \frac{\rho u x}{\mu}$$

$$s = \frac{4.91 \cdot x}{\sqrt{R_x}} \quad \text{or} \quad \frac{s}{x} = \frac{4.91}{\sqrt{R_x}}$$

Now; $\tau_0 = \mu u B/s.$

Thus Putting value.

$$\tau_0 = 0.332 \frac{\mu u}{x} \sqrt{R_x}$$

where R_x is local Reynold number.

Now;

$$F_f = B \int \frac{\tau_0 dx}{\text{stress}}$$

Putting values.

$$F_f = 0.664 B \sqrt{\rho \mu L U^3}$$

As general equation is.

$$F_f = c_f \frac{\rho U^2}{2} BL \rightarrow \text{equating both equation.}$$

$$c_f = 1.328 \sqrt{\frac{\mu}{\rho U}}$$

$$= 1.328 / \sqrt{R}$$

x ————— x ————— x

⇒ Turbulant Boundary

layer:-

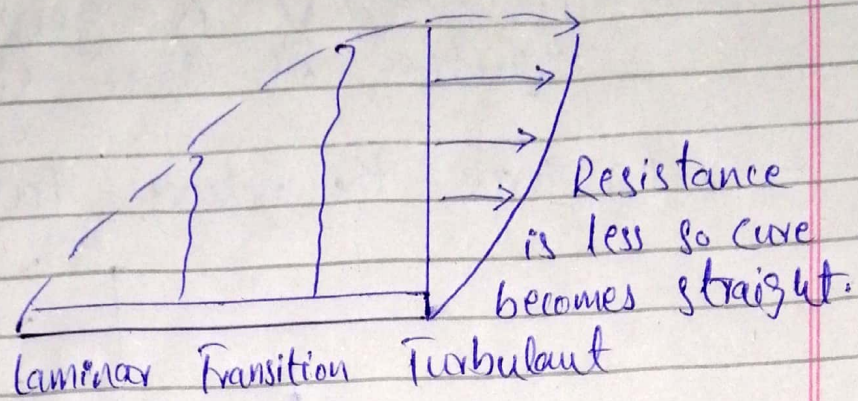


Fig show that velocity distribution is Turbulent boundary layer shows a much gradient near wall and flatter through out remaining layer.

The shear stress is greater in Turbulent than in laminar layer.

As we know.

$$\tau_0 = f \rho V^2 / 8 \quad \text{"where } V \text{ denotes average velocity of pipe."}$$

Now we have obtained an approximate relation b/w τ_0 and V by using Pipe factor equation at.

$$v/u_{\max} = \frac{1}{1+1.33 \sqrt{f}}$$

using friction factor of 0.028
from chart which is middle
critical value.

$$\text{So } u = 1.235 v$$

Now we have

$$\tau_0 = f S \frac{v^2}{8}$$

As we know.

$$f = 0.316 / 0.25$$

$$\text{Thus } \tau_0 = 0.316 / \left(\frac{Dv}{u} \right)^{1/4} \cdot \frac{v^2}{8}$$

$$\text{where } v = u / 1.235$$

$$\tau_0 = 0.316$$

$$\left(\frac{D}{r} \left(\frac{u}{1.235} \right) \right)^{1/4} \cdot \frac{v^2}{8} \left(\frac{v}{1.235} \right)^2$$

$$D = 28$$

$$\text{Thus } \tau_0 = 0.023 \frac{S u^2}{\left(\frac{S u}{v} \right)^{1/4}}$$

we have.

$$\tau_0 = \int u^2 \alpha \, ds / dx$$

Equating both & integrating
for boundary condition of.

$$x=0, \delta=0.$$

$$\delta = \frac{(0.0287)^{4/5}}{\alpha} (\nu/ux)^{1/5} x$$

$$\text{For } \alpha = 0.0972$$

$$\delta/x = 0.377 / (Rx)^{1/5}$$

Putting values in equation.

$$Z_0 = 0.0587 \int \frac{u^2}{x} (\nu/ux)^{1/5}$$

$$\text{Now; } Ff = B \int Z_0 dx$$

$$Ff = 0.0735 \int \frac{u^2}{x} (\nu/ux)^{1/5} BL$$

$$\text{As } Ff = Cf \int v^2/2 BL$$

evaluating both.

$$Cf = 0.0735 / R^{1/5}$$

R is less than
 10^7 for 500,000
 $Cf < 10^{-7}$

$$\text{for } R > 10^7$$

$$Cf = 0.455 / (\log R)^{2.58} \text{ (Ans)}$$

Q No: 1 (Part B)

Sol:- As specific energy.

$$E = y + v^2/2g$$

→ The flow Q Per unit width b can be expressed as.

$$qV = Q/b$$

Now average velocity will be.

$$V = Q/A = qb/by = q/y$$

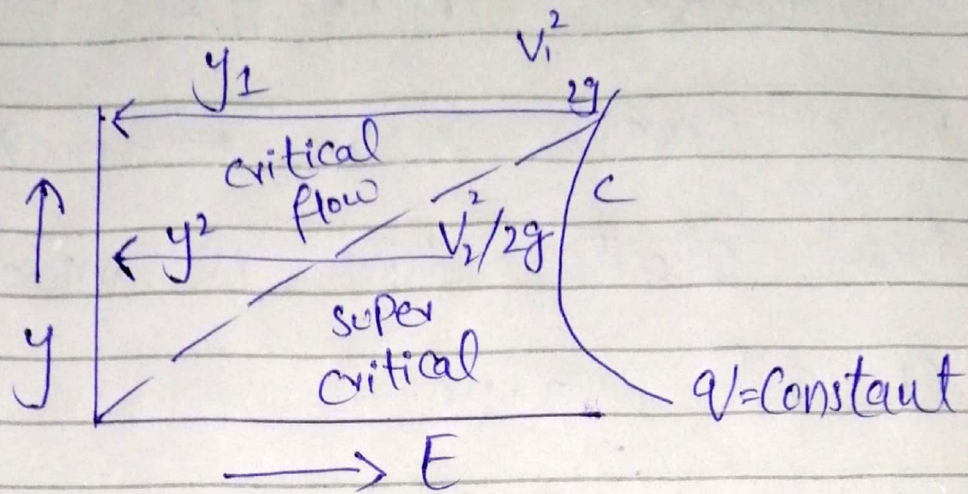
Thus, The point at which specific energy is least among it is called critical depth point.

$$E = y + v^2/2g \Rightarrow y + \frac{1}{2g} (q^2/y^2)$$

$$(E - y) = \frac{1}{2g} (q^2/y^2) \quad \text{or}$$

$$(E - y) y^2 = q^2/2g$$

Thus Plot of E vs Y will be parabolic. For particular q , there will be two kind of possible values of y , for a given E .



The equation is cubic with three roots with third root being negative. Point c represents dividing point b/w two regime of flows. Thus for given q and value of E is minimum of flow at that point is critical flow. Depth of flow at that point is critical depth y_c and velocity at that point is critical velocity v_c .

$$\text{Thus } E = y + \frac{1}{2g} \left(\frac{q^2}{y^2} \right)$$

For minimum specific energy =

$$\frac{dE}{dy} = 0$$

$$\text{Thus: } \frac{dE}{dy} = 1 - \frac{2}{2g} \left(\frac{q^2}{y^3} \right) = 0$$

$$\Rightarrow \frac{q^2}{gy^3} = 1 \Rightarrow q^2 = gy^3$$

$$\frac{q^2}{g} = y^3 = \left(\frac{q^2}{g} \right)^{\frac{1}{3}} = y_c$$

Now;

$$v^2 = gy^3$$

if

$$QV = Vy = V^2y^2 = gy^3$$

or

$$V^2 = gy \text{ or}$$

$$V_{CR} = \sqrt{gy \text{ or}} \quad (\text{Ans})$$

x ————— x ————— x

(Q No : (2)

Given:

Depth of Rectangular channel (d) = ?

Flow rate (Q) = 3.5 m³/sec

Slope of Bed (S₀) = 0.0008

$$n = 0.0219$$

width of Bed = 7395 mm

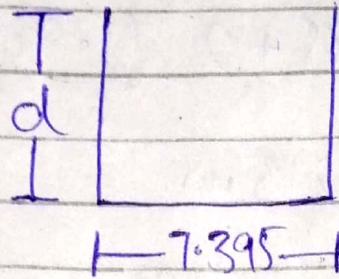
$$= 7.395$$

Critical Depth = ?

Flow sub-critical or super-critical = ?

Sol:-

$$\begin{aligned} \text{Area} &= 7.395 \times d \\ &= 7.395d \end{aligned}$$



$$\begin{aligned} \text{Perimeter} &= d + 7.395 + d \\ &= 7.395 + 2d \end{aligned}$$

$$\begin{aligned} \rightarrow \text{Hydraulic Radius} &= (R_h) = A/P \\ &= \frac{7.395d}{7.395 + 2d} \end{aligned}$$

By using Manning Equation.

$$Q = \frac{1}{n} A R^{2/3}, \text{ so } \frac{1}{2}$$

Putting values.

$$3.5 = \frac{1}{0.0219} \times 7.395d \times \left(\frac{7.395d}{2d + 7.395} \right)^{2/3} \times (0.008)^{1/2}$$

$$3.5 = 45.66 \times 7.395d (0.008)^{1/2}$$

$$3.5 = 4.063 \times 7.395d$$

$$d = 1.909 \text{ m}$$

$$\begin{aligned} \text{Area} &= 7.395 (1.909) \\ &= 14.71 \text{ m}^2 \end{aligned}$$

$$\begin{aligned} \text{Perimeter} &= 7.395 + 2 (1.909) \\ &= 21.213 \text{ m} \end{aligned}$$

$$\begin{aligned} \text{Hydraulic Radius (Rh)} &= \frac{14.71}{21.213} \\ &= 0.693 \text{ m} \end{aligned}$$

Finding critical depth:

$$y_{cr} = (q^2/g)^{1/3}$$

$$\begin{aligned} \text{As } q &= Q/B \\ &= 3.5/7.395 \end{aligned}$$

$$= 0.47 \text{ m}^3/\text{sec}$$

$$\begin{aligned} \Rightarrow y_{cr} &= \left(\frac{(0.47)^2}{9.81} \right)^{1/3} \\ &= 0.282 \end{aligned}$$

$$\text{As } y > y_{cr}$$

$$1.909 > 0.282$$

So flow is sub-critical

x ————— x ————— x

Q No: (3)

Given;

Friction Drag = (FD) = ?

width (B) = 200mm = 0.2m

length (L) = 800mm = 0.8m

Specific Gravity (S) = 0.89

undisturbed velocity (U) = 5m/sec

Kinematic viscosity (ν) = $0.93 \times 10^{-4} \text{ m}^2/\text{sec}$

Sol:

checking whether flow is laminar or not by Reynold no.

$$R = Du/\nu$$

For smooth flat plate

$$D = L, \quad \nu = \nu$$

$$\text{So; } R = Lu/\nu$$

$$= \frac{0.8 \times 5}{0.93 \times 10^{-4}} = 43010$$

$43010 < 500,000 \rightarrow$ laminar

By using formula:

$$F_f = c_f \cdot \rho \cdot v^2 / 2 \cdot BL$$

where;

$$c_f = \frac{1.328}{\sqrt{R}} = \frac{1.328}{\sqrt{43010}}$$

$$= 0.0064$$

$$\rho = \rho_{\text{oil}} / \rho_{\text{water}} \Rightarrow 0.89 = \rho_{\text{oil}} / 1000$$

$$\rho_{\text{oil}} = 0.89 \times 1000$$

$$\rho_{\text{oil}} = 890 \text{ kg/m}^3$$

$$\Rightarrow F_f = c_f \cdot \rho \cdot v^2 / 2 \cdot BL$$

$$= 0.0064 \times 890 \times \left(\frac{5}{2}\right)^2 \times 0.2 \times 0.8$$

$$F_f = 11.39 \text{ N}$$

x ————— x ————— x