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7894

Sec A

Mechanics of SOLID - 2

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Q No (1) (a).

(1)

Given Data:

Section Height = 50 mm.

Thickness = $b = 26$ mm.

$T_f = 2$ mm.

Required:

Shear Center = ?

Solution:

In case of Unsymmetrical member, Shear Centre is some distance away from geometrical centre, that some is known as eccentricity, which is given by.

$$e = \frac{I_{yf} h^2 b^2}{4I}$$

$\therefore I_2$ Moment of inertia

$$I_2 = 2 \left(\frac{bh^3}{12} + Ay^2 \right) + \left(\frac{bh^3}{12} + Ay^2 \right)$$

$$I_2 = 2 \left(\frac{26 \times (50)^3}{12} + (20 \times 2)(25)^2 \right) + \left(\frac{2(50)^3}{12} + 0 \right)$$

$$I_2 = 50034.67 + 20833.33$$

$$I_2 = 70868.0033$$

(2)

$$e = \frac{T_8 h^2 b^2}{4I}$$

$$e = \frac{2 \times 50^2 \times 25^2}{4(70888.0033)} = \frac{3125000}{283472.01}$$

$$e = 11.024 \text{ mm}$$

Hence, Shear Center is 11.024 mm
from geometrical center.

away



Q No (1) (b)

Given Data:

Height = 26 ft

Diameter = 22 ft.

Circumferential stress = ~~62.4 lb/ft²~~ 6000 PSI

Specific weight = 62.4 lb/ft³

Required:

Thickness of walls = ?

Solution:

As we know.

$$P = \gamma h$$

$$\sigma_t = \frac{PD}{2t}$$

$$\sigma_t = \frac{\gamma h D}{2t}$$

$$t = \frac{\gamma h D}{2\sigma_t} = \frac{62.4 / (12)^3 \times (26 \times 12) \times (22 \times 12)}{2 \times 6000}$$

$$t = 0.247 \text{ in.}$$



Q2a

(4)

~~Given Data:~~Solution:

Moment of Inertia

$$I_z = \frac{bh^3}{12} = \frac{0.1(0.15)^3}{12}$$

$$I_z = 2.8125 \times 10^{-5}$$

Now

$$I_y = \frac{bh^3}{12} = \frac{(0.15)(0.1)^3}{12}$$

$$I_y = 1.25 \times 10^{-5}$$

$$\delta = \frac{M_z Y}{I_z} + \frac{M_y Z}{I_y}$$

$$\delta = \frac{M \cos \theta}{I_z} + \frac{M \sin \theta}{I_y}$$

Where

$$M_z = \cos \theta \Rightarrow P \cos \theta = M_z$$

$$M_z = 12 \cos 30^\circ$$

$$M_z = 1.8510$$

$$M \sin \theta \Rightarrow P \sin \theta = M_y$$

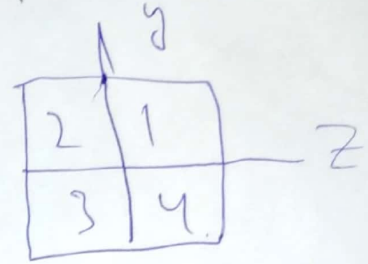
$$M_y = 12 \sin 30^\circ = 1.8563$$

(5)

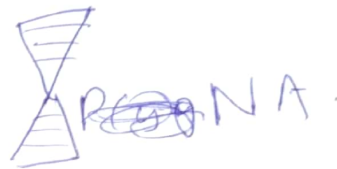
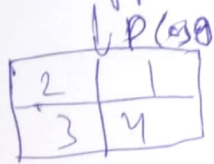
$$\sigma_z = \left(\frac{M_z}{I_z} \right) + \left(\frac{M_y}{I_y} \right)$$

$$= \frac{1.851}{2.812 \times 10^{-5}} + \left(\frac{-11.8563}{1.25 \times 10^{-5}} \right)$$

$$\sigma_z = 882678 \text{ N/m}^2$$

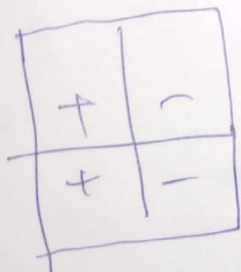


Now if we take Compression as negative and tension as positive and beam is simply supported



Quadrant 1, 2 \rightarrow -ve

Quadrant 3, 4 \rightarrow +ve.



$\leftarrow P \sin \theta$



Quadrant 1, 4 \rightarrow -ve

Quadrant 2, 3 \rightarrow +ve.

(6)

Unsymmetrical loading the Neutral axis lies at an angle of "X". The Principle axis and Algebraic Sum of Stress at NA is zero

$$\sigma_z = \frac{M \cos \theta \cdot y}{I_z} + \frac{M \sin \theta \cdot z}{I_y} - Z \quad \text{--- (9)}$$

NA Passes through 2,4.

$$\sigma_z = \frac{M \cos \theta \cdot y}{I_z} + \frac{M \sin \theta \cdot z}{I_y}$$

let us Consider a Point A on NA
Lies on Quadrant 2 where

Bending stress due to $P \cos \theta$ is Compressive

Bending stress due to $P \sin \theta$ is tensile.

Q(2) Part (b):



Given Data:

~~Centre concentrated load~~

length of beam = 16 ft.

Angle of inclination = 60° .

$$I_x = 112.6 \text{ in}^4$$

$$I_y = 18.7 \text{ in}^4$$

$$\sigma_T = 5000 \text{ PSI,}$$

$$\sigma_C = 12000 \text{ PSI,}$$

Required:

Maximum load = ?

Solution:

There will be tension as well as compression which will reduce the effect of each other, so we will calculate stress at A and C so.

$$\sigma_A = \frac{M \times y}{I_x} + \frac{M \times y \times \mu}{I_y} \quad (\text{Compression})$$

$$\sigma_C = \frac{M \times y}{I_x} + \frac{M \times y \times \mu}{I_y} \quad (\text{Tension})$$

Now M_x and M_y

(8)

$$M_x = P \cos 60^\circ (16 \times 12)$$

$$M_x = 48 P \cos 60^\circ$$

$$M_y = \frac{P \sin 60^\circ (16 \times 12)}{4}$$

$$M_y = 48 P \sin 60^\circ$$

$$\sigma_A = \frac{M_x y}{I_x} + \frac{M_y x}{I_y}$$

$$\sigma_A = \frac{48 P \cos 60^\circ \times 3.07 + 48 P \sin 60^\circ \times 3.07}{1126 + 18.7}$$

$$P = 1638.6 \text{ lb}$$

Now

$$\sigma_c = \frac{M_x y}{I_x} + \frac{M_y x}{I_y}$$

$$5000 = 48 P \cos 60^\circ + 595 + \frac{48 P \sin 60^\circ \times 0.5}{18.7}$$

$$P = 2104.9 \text{ lb}$$

Maximum stress load = 1638.6 lb

Q(3)

(9)

Given Data:

$$\text{length} = 10 \text{ ft.}$$

$$E = 10.3 \times 10^6$$

$$b = 0.75$$

$$h = 2$$

$$\text{Factor of Safety} = 2$$

Required:

a) Safe load at hinged = ?

b) Safe load at fixed = ?

Solution

a) For hinged column

$$L_e = L$$

$$I_z = I_x = \frac{(0.75)(2)^3}{12} = 0.5 \text{ in}^4$$

$$P_{cr} = \frac{\pi^2 EI L^2}{L_e^2} = \frac{(1)^2 (10.3 \times 10^6) (0.5) \pi^2}{(10 \times 12)^2}$$

$$P_{cr} = \frac{50776940}{14400} = 3526.176 \text{ lb.}$$

$$P \text{ Safe load} = \frac{P_{cr}}{\text{Factor of Safety}} = \frac{3526176}{2} = 1763.088 \text{ lb}$$

5) Strut act Column.

le = 1/2 (for fixed ended)

le = 10 / 2 = 5 ft.

Ix Iy = 2 x (0.75)^3 / 12 = 0.07 in^4.

Pcr = n^2 EI / le^2 = (1)^2 (10.3 x 10^6) (0.07) (3.14)^2 / (5 x 12)^2

Pcr = 7108771.6 / (60)^2 = 1974.65811

Pcr = 1974.658 lb.

Psafe load = 1974.658 / 2 = 987.3293 lb.