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Q<sub>1</sub> A Rectangular beam that must carry a service live load of 2.47 kips/ft. and a calculated dead load of 1.05 kips/ft (without self-weight) on an 18-ft simple span is limited to 10 inches width and 20 inches total depth for architectural reasons. If  $f_y = 60000 \text{ psi}$  and  $f'_c = 4000 \text{ psi}$ , what steel area must be provided? Draw sketch of your final design.

Sol Given Data

Dead load = 1.05 kip/ft

Live load = 2.47 kip/ft

$f_y = 60000 \text{ psi}$

$f'_c = 4000 \text{ psi}$

$d = h - 3 = 20 - 3 = 17''$

$d' = 2.5''$

$h = 20'' , w = 10''$

Step 1

$$P_{max} = 0.85 \times \beta \times \frac{f'_c}{f_j} \times \left( \frac{\epsilon_u}{\epsilon_u + \epsilon_y} \right)$$

$$= 0.85 \times 0.85 \times \frac{4}{60} \times \left( \frac{0.003}{0.003 + 0.005} \right)$$

$$P_{max} = 0.0181$$

Step 02 Area of steel [ $A_{st}$ ]

$$P_{max} = \frac{A_{st}}{b \times d}$$

$$A_{st} = P_{max} \times b \times d$$

$$A_{st} = 0.0181 \times 10 \times 17$$

$$A_{st} = 3.077 \text{ in}^2$$

Step 03 Design factored moment [ $M_{u2}$ ]

$$M_{u2} = \phi \times A_{st} \times f_j \times \left( d - \frac{a}{2} \right)$$

$$a = \frac{A_{st} \times f_j}{0.85 f'_c b}$$

$$a = \frac{3.08 \times 60}{0.85 \times 4 \times 10} = 5.4''$$

$$M_{u2} = 0.90 \times 3.08 \times 60 \times \left( 17 - \frac{5.4}{2} \right)$$

$$M_{u2} = 2378.38 \text{ k}''$$

Now

Moments of the given load

$$\begin{aligned} \text{Beam self weight} &= b \times t \times \delta c \\ &= \frac{10}{12} \times \frac{20}{12} \times 150 \\ &= 208.33 \text{ lb/ft} \end{aligned}$$

Now

$$\begin{aligned} \text{Total factored load} &= 1.2 D\text{-Load} + 1.6 L\text{-Load} \\ &= 1.2(1050 + 208.33) + (1.6)(2470) \\ &= 5461.996 \text{ lb/ft} \\ &= 5.46 \text{ k/ft} \end{aligned}$$

$$\text{Ultimate factored moment} = \frac{wL^2}{8}$$

$$\begin{aligned} M_u &= \frac{5.46(18)^2}{8} \times 12 \\ &= 2653.56 \text{ k}'' \end{aligned}$$

$$\text{Thus } 2378.38 < 2653.56$$

It should be double designed beam

Step 04

$$M_{u1} = M_u = M_{u2}$$

$$M_{u1} = 2653.56 - 2378.38$$

$$M_{u1} = 275.18 \text{ k}''$$

Step 05

$$M_{u1} = \phi \times A_s' \times f_y \times (d - d')$$

$$A_s' = \frac{M_{u1}}{\phi \times f_y \times (d - d')}$$

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$$A_s' = \frac{275.18}{0.90 \times 60 (17 - 2.5)}$$

$$A_s' = 0.35 \text{ in}^2$$

step 06

$$\begin{aligned} A_s &= A_{sT} + A_s' \\ &= 3.08 + 0.35 \\ &= 3.43 \text{ in}^2 \end{aligned}$$

This lies in the tension zone of steel.

step 07 Selections of Bars

For tensile steel

Let's take #8 having an area of  $0.785 \text{ in}^2$

$$\text{No of bars} = \frac{A_s}{A_b} = \frac{3.43}{0.785} = 4.36 \approx 5 \text{ bars}$$

For compression steel

→ let's take #6 having an area of  $0.442 \text{ in}^2$

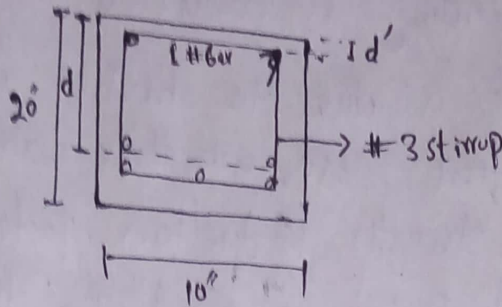
$$\begin{aligned} \Rightarrow \text{No of bars} &= \frac{A_s'}{A_b} \\ &= \frac{0.35}{0.442} = 0.79 \text{ bar} \approx 1 \text{ bar} \end{aligned}$$

Step 08 Beam minimum width

$$b_{min} = (2 \times 1.5) + 2\left(\frac{3}{8}\right) + 5 \times \frac{8}{8} + \left(4 \times \frac{8}{8}\right)$$

$$= 12.75'' > 10''$$

It should be in multiple layers.



Now

$$d = 20 - 1.5 - \frac{3}{8} - \frac{8}{8} - \frac{1}{2}\left(\frac{8}{8}\right)$$

$$d = 16.625''$$

$$d' = 1.5 + \frac{3}{8} + \frac{1}{2}\left(\frac{6}{8}\right) = 2.25''$$

Step 09 Design Moment

So

$$M_d = \phi \times \left[ A_s' \times f_y \times (d - d') + (A_s - A_s') \times f_y \times \left(\frac{d - a}{2}\right) \right]$$

$$a = \frac{(A_s - A_s') \times f_y}{0.85 f_c \times b} = \frac{5 \times 0.785 - 1 \times 0.44}{0.85 \times 4 \times 10} \times 60$$

$$a = 6.15''$$

$$M_d = 0.90 \times \left[ 1 \times 0.44 \times 60 \times (16.625 - 2.25) + (5 \times 0.785 - 1 \times 0.44) \times 60 \times \left(16.625 - \frac{6.15}{2}\right) \right]$$

$$M_d = 2891.5245$$

which is

$$M_d = 2891.5245 > 2653.56 k''$$

Designed is OK

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## Bond stress

1- The stress which is acting on the outer interface of steel to the surrounding concrete is called bond stress.

→ This stress helps in keeping bond b/w reinforcement and concrete together.

## Development length

A development length can be defined as "The amount of reinforcement (bar) length needed to be embedded or project into the column to establish the desired bond strength b/w the concrete and steel."

## Condition in which doubly reinforced beam used

- (i) ⇒ when the cross section of the beam is fixed.
- (ii) when moment to be carried by the beam is more than the balanced moment.
- (iii) In case of a continuous beam.
- (iv) when dimension of the beam are restricted for architectural or structural purpose.
- (v) The portion of the beam over middle support in continuous T-beams has to be designed as double reinforced section.

## (C) T-Beam Analysis

- ① T-Beam is more economical than rectangular beam
- ② In case of T-shaped structure.
- ③ In case of T-Beam slab and beam are connected with one another and act as one member
- ④ Analysis is required when
  - $a > h_f$
  - $a = \text{depth}$
  - $h_f = \text{slab thickness}$

## Rectangular Beam Analysis

- ① Rectangular beam is less economical than T-Beam
- ② In case of rectangular beam slab has been placed on the ~~base~~ beam and there is no connection b/w slab and beam.
- ③ It is most commonly used in office/Commercial building
- ④ Analysis is required when
  - $a \leq h_f$
  - where  $a = \text{depth}$
  - $h_f = \text{height of flange}$

## (D) Effective of strength reduction factor on flexural strength

The flexural strength of reinforced concrete (RC) beams strengthened with a carbon fiber reinforced polymer plate which fails by intermediate crack debonding is evaluated.

→ The effect is due to higher debonding resistance in the first case, ~~where~~ where the comparison of the strength reduction factor with experimental data and factors prepared for that.

## (E) Design Methods

It is a procedure techniques aids, or tool for designing.

→ They offer a number of different kinds of activities that a designer might use within an overall design process.

→ Three methods of structural design



Q No 3AnsGiven Data

$$c/c \text{ distance} = 10'$$

$$\text{Span} = 32'$$

$$\text{slab thickness} = 6''$$

$$\text{web width} = 14''$$

$$\text{Total depth}(h) = 28''$$

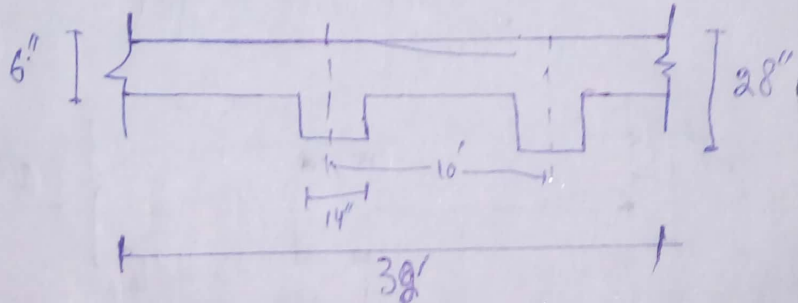
$$\text{Effective depth} = 28'' - 3'' = 25''$$

$$D.L = 50 \text{ lb/ft}^2$$

$$L.L = 225 \text{ lb/ft}^2$$

$$f_y = 60,000 \text{ psi}$$

$$f_c = 4000 \text{ psi}$$

Sol

Step #1 Ultimate factored moment  
we know that

$$M_u = \frac{w_u \times l^2}{8}$$

i Beam self wt per feet

(i) Beam self wt per foot:

$$\begin{aligned} W_t &= b \times t \times \gamma_c \\ &= \frac{14}{12} \times \frac{28}{12} \times 150 \\ &= 408.34 \text{ lb/ft} \end{aligned}$$

Total Factored Load

$$\Rightarrow 1.2(50 + 408.34) + 1.6(225)$$

$$\Rightarrow 909.99 \text{ lb/ft}$$

$$\Rightarrow 0.909 \text{ kip/ft}$$

Moment

$$\frac{wL^2}{8} = \frac{0.909 \times (32)^2}{8} \times 12 = 1396.23 \text{ kip/in}$$

Step-02 Calculate effective width "b"

$$\text{(1) } 16(h_f) + b_w = 16(6) + 14 = 110''$$

$$\text{(2) } c/c \text{ distance} = 10(12) = 120''$$

$$\text{(3) } \frac{\text{span}}{4} = \frac{32}{4} \times 12 = 96''$$

$$\text{So } \boxed{b_e = 96''}$$

Step-03 Check whether Rectangular or T Beam is

Trial #1, let  $a = h_f = 6''$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - \frac{a}{2})} = \frac{1396.23}{0.90 \times 60 \times (25 - \frac{6}{2})}$$

$$A_{st} = 1.17 \text{ in}^2$$

Trial #02

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$$a = \frac{A_{st} \times f_y}{0.85 \times f'_c \times b} = \frac{1.17 \times 60}{0.85 \times 4 \times 96} = 0.2'' < 6''$$

So Rectangular Beam design

$$A_{st} = \frac{1396.23}{0.90 \times 60 \times (25 - 0.2/2)} = \boxed{1.03 \text{ in}^2}$$

Trial #03

$$a = \frac{1.03 \times 60}{0.85 \times 4 \times 96} = 0.18''$$

$$A_{st} = \frac{1396.23}{0.90 \times 60 \left(25 - \frac{0.18}{2}\right)} = 1.03 \text{ in}^2$$

Step #04 check  $f_{max}$  and  $f_{min}$

$$\Rightarrow f_{max} = 0.85 \times 0.85 \times \frac{4}{60} \left( \frac{0.003}{0.003 + 0.005} \right)$$

$$f_{max} = 0.018$$

$$\Rightarrow f_{min} = \frac{200}{f_y} = \frac{200}{60,000} = 0.003$$

$$f = \frac{A_{st}}{b \times d} = \frac{1.03}{14 \times 25} = 0.0029$$

$$f_{min} < f < f_{max}$$

$$0.003 < 0.0029 < 0.018$$

As

(12)  
P is less than  $f_{min}$ 

So

$$P = \frac{A_{st}}{b \times d}$$

$$A_{st} = f_{min} \times b \times d = 0.003 \times 14 \times 25 = 1.05 \text{ in}^2$$

Step #05, No and section of Bar

Let use #8 bar, then

$$\text{dia} = 8/8 = 1", \text{ Area} = 0.785 \text{ in}^2$$

Now

$$\# \text{ of bars} = \frac{1.05}{0.785} = \boxed{1.3 \approx 2}$$

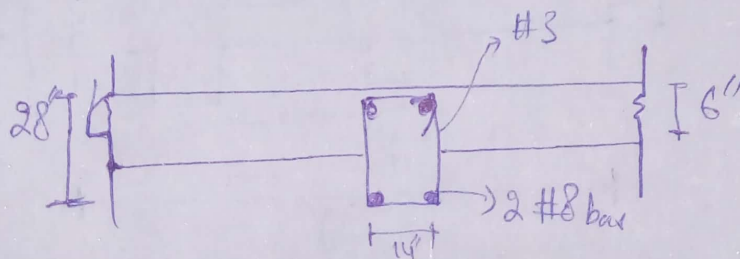
So we use 2 #8 bars

Step #06 Check on minimum width

$$b_{min} = 2(1.5) + 2\left(\frac{3}{8}\right) + 2\left(\frac{8}{8}\right) + 1\left(\frac{8}{8}\right)$$

$$= 6.75" < 14"$$

So good in one layer.

Step #07 Design moment

$$\Rightarrow M_d = \phi \times f_y \times A_{st} \times \left(d - \frac{a}{2}\right)$$

First we find Area of steel

$$\Rightarrow \text{Area of steel} = \text{Area of 1 bar} \times \text{No of bars}$$

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Put the values

$$\Rightarrow \text{Area of steel} = 0.785 \times 2 = 1.57 \text{ in}^2$$

$$\text{Area of steel} = 1.57 \text{ in}^2$$

Now

$$a = \frac{1.57 \times 60}{0.85 \times 4 \times 96}$$

$$a = 0.2$$

Then

$$\Rightarrow M_d = 0.90 \times 60 \times 1.57 \times \left(25 - \left(\frac{0.2}{2}\right)\right)$$

$$M_d = 2111.02 \text{ kip-inch}$$

$$A_s \cdot 2111.02 > 1396.23$$

Design is ok?