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Subject :- MOSII - Theory

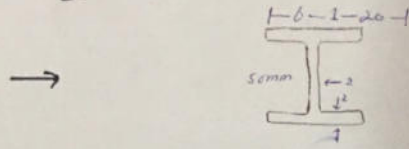
Program :- (REC)

Exam :- Final Terms

Date :- 23 June 2020.

→ Question #01 Page #1

→ Part # (a)



→ Required location of share center.

→ Solⁿ As we know that

$$e = \frac{I_x h^2 b^2}{4I}$$

and

$$I = 2 \left(\frac{bh^3}{12} + Ay^2 \right) + \left(\frac{bh^3}{12} + Ay^2 \right)$$

$$= 2 \left[\frac{26(20)^3}{12} + (20 \times 2)(25)^2 \right] + \left[\frac{2(26)^3}{12} + 0 \right]$$

$$I = 50034.66 + 20833$$

$$I = 70867.99 \text{ mm}^4$$

$$e = \frac{2(26)^2(25)^2}{4(70867.99)} = 11.02 \text{ mm}$$

→ So share center $e = 11.02 \text{ mm}$.

(2)

Question = 1

Part = (b)

* Data:-

$$\Rightarrow H = 26 \text{ ft}$$

\Rightarrow I assume diameter

$$D = 22 \text{ ft}$$

$$\Rightarrow \text{Tangential stress} \\ = 600 \text{ lb/ft}^2$$

$$\Rightarrow \text{Specific weight of} \\ \text{water tank} = 62.4 \text{ lb/ft}^3$$

we have to find
the thickness = ?

③
* Solution:-

The pressure
developed by water

$$= p = \gamma h$$

$$bt = \frac{PD}{2t} \Rightarrow \frac{\gamma h D}{2t}$$

$$2t \times bt = \gamma h D$$

$$2t = \frac{\gamma h D}{bt}$$

$$t = \frac{\gamma h D}{bt \times 2}$$

$$t = \frac{\left(\frac{62.4}{12}\right) \times (26 \times 12) \times (22 \times 12)}{6000 \times 2}$$

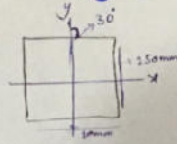
$$t = 0.24$$

(4)

⊛ Question # Q2

⊛ Part # (a)

⊛ Diagram :-



⊛ Momout of Inertia:-

$$I_z = \frac{bh^3}{12} = \frac{0.15 (2.1)^3}{12} = I_z = 2.8125 \times 10^{-5}$$

$$\text{Now } I_y = \frac{bh^3}{12} = \frac{0.15 (2.1)^3}{12}$$

$$I_y = 1.25 \times 10^{-5}$$

$$I = \frac{M_x y}{I_z} + \frac{M_y z}{I_y}$$

$$I = \frac{m \cos \theta}{I_z} + \frac{m \sin \theta}{I_y}$$

where

$$m = \cos \theta = P \cos \theta = m_z$$

$$= 12 \cos 30 = m_z$$

$$m_z = 10.392$$

$$m \sin \theta = P \sin \theta = m_y$$

$$m_y = 12 \sin 30$$

$$m_y = 6$$

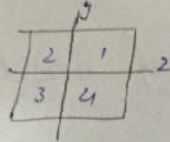
(5)

②

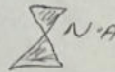
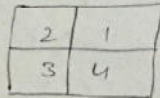
$$G = \left(\frac{mz}{I_x} \right) + \left(\frac{my}{I_y} \right)$$

$$G = \frac{1.857}{2.812 \times 10^{-6}} + \left(\frac{-11.8563}{1.25 \times 10^{-5}} \right) = \frac{882078}{Nm^2}$$

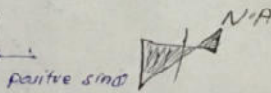
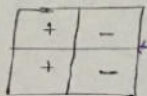
Sign Convention



→ If we take compression as negative and tension as a positive and the beam is a simply supported plate.



Quadrant 1, 2 -ve.
Quadrant 3, 4 +ve



Quadrant 1, 4 -ve
Quadrant 2, 3 +ve

(6)

→ was of an symmetrical loading the neutral axis is at an angle of θ to the principal axis and the algebraic sum of stress at N.A is zero.

$$\sigma = \frac{m \cos \theta y}{I_x} + \frac{m \sin \theta z}{I_y} \rightarrow (1)$$

→ in this case, N.A passes through 2, 4, 30

$$\sigma = \frac{m \cos \theta y}{I} + \frac{m \sin \theta z}{I_y}$$

→ let consider a point A on N.A lies in quadrant 3, where
• Bending stress due to p case is compresses

(6)

(7)

→ (8) Bending stress due to $P \sin \theta$ is tensile

$$\text{eq (i)} \Rightarrow 0 = -\frac{m \cos \theta y_A}{I_z} + \frac{m \sin \theta z_A}{I_y}$$

$$\rightarrow 0 = \frac{-m \cos \theta y_A}{I_z} + \frac{m \sin \theta z_A}{I_y}$$

$$\rightarrow 0 = \frac{m \cos \theta y_A}{I_z} + \frac{m \sin \theta z_A}{I_y}$$

$$\Rightarrow \frac{y_A}{z_A} = \frac{I_z}{I_y} \frac{\sin \theta}{\cos \theta} \Rightarrow \tan \alpha = \frac{I_z}{I_y} \tan \theta$$

(9) ↓

Now put values of I_z , I_y and θ in eq (9)

$$\tan \alpha = \frac{I_z}{I_y} \tan 30^\circ$$

$$\Rightarrow \tan \alpha = \frac{3.8125 \times 10^5}{12.5 \times 10^5} \tan 30^\circ$$

(8)

⑥

$$\rightarrow \tan \alpha = -14.4129$$

$$\alpha = \tan^{-1}(-14.4129)$$

$$\alpha = 1.5^\circ$$

$$\alpha = 1^{\circ}38'5''$$

Q #02
part B

(9)

Ans:

Given data:

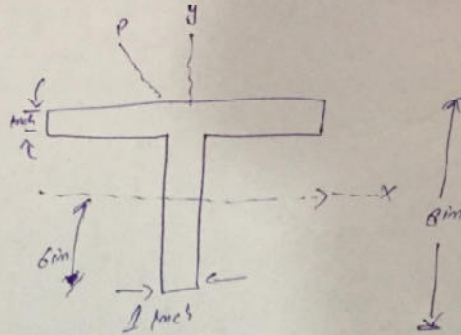
$$L = 167t$$

$$I_x = 110.6 \text{ in}^4$$

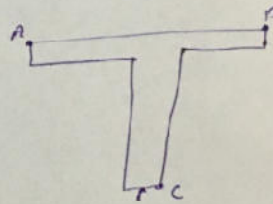
$$I_y = 18.7 \text{ in}^4$$

$$\sigma_c = 12000 \text{ psi}$$

$$\sigma_t = 8000 \text{ psi}$$



Sol: By looking to the figure we can see that maximum compression would occur at A and maximum tension at pt c. There will be tension as well as compression which will cancel the effect of each other so we will calculate stresses.
At A & c



$$\sigma_A = \frac{m \times y}{I_x} + \frac{m \times x}{I_y} \quad (\text{Comp})$$

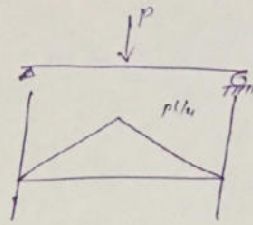
$$\sigma_c = \frac{m \times y}{I_x} + \frac{m \times x}{I_y} \quad (\text{Tension})$$

Now m_x & m_y

(b)

so
$$m_x = \frac{P \cos 60^\circ (16 \times 12)}{4}$$

$$m_x = 48 P \cos 60^\circ$$



$$m_y = \frac{P \sin 60^\circ (16 \times 12)}{4}$$

$$m_y = 48 P \sin 60^\circ$$

Now

$$\sigma_A = \frac{m_x y}{I_x} + \frac{m_y x}{I_y}$$

$$= 12000 = \frac{48 P \cos 60^\circ \times 3.07}{112.6} + \frac{48 P \sin 60^\circ \times 9}{18.7}$$

Solving the equation

$$\Rightarrow P = 1638.6 \text{ kN}$$

Now

$$\sigma_C = \frac{m_x y}{I_x} + \frac{m_y x}{I_y}$$

$$5000 = \frac{48 P \cos 60^\circ \times (5.93)}{112.6} + \frac{48 P \sin 60^\circ \times 0.5}{18.7}$$

Solving the equation

$$P = 2104.9 \text{ kN}$$

So the maximum load P applied should be 1638.6 kN

Q #03

(11)

Ans:

Given data:

$$\text{Length } L = 10\text{ft}$$

As both side are hinged

$$L_0 = L_e = L$$

$$E = 10.8 \times 10^6$$

Factor of safety = 2

$$b = 0.75 \text{ inch}$$

$$h = 2 \text{ inch}$$

Res: determine safe load. ?

Sol: As

$$P_{cr} = \frac{\pi^2 EI}{L_e^2}$$

As we know that

$$E = A\alpha^2$$

$$\alpha = \sqrt{E/A}$$

$$\alpha = \frac{\sqrt{hb^3}}{12/bh} = \sqrt{b^2/12}$$

$$\alpha = \frac{b}{2\sqrt{3}} = \frac{0.75}{2\sqrt{3}}$$

$$\alpha = 0.216 \text{ inch}$$

$$P(\alpha) = \frac{\pi^2 EA}{(le/\alpha)^2}$$

$$= \frac{(3.14)^2 (10.3 \times 10^6) (1.5)}{(10/0.216)^2}$$

$$P(\alpha) = 853.8343$$

$$\text{Safe load} = \frac{\text{Crippling load}}{\text{Factor of safety}}$$

$$\Rightarrow \frac{853.8343}{2}$$

$$\text{Safe load} = 426.917$$

* For fixed ended column

$$le = l/2 = 10/2$$

$$le = 5 \text{ ft}$$

$$P(\alpha) = \frac{\pi^2 EA}{(le/\alpha)^2} = \frac{(3.14)^2 \times (10.3 \times 10^6) (1.5)}{10/(0.216)^2}$$

$$\boxed{PCR = 1974.207}$$

(13)

$$\text{safe load} = \frac{PCR}{\text{factor of safety}}$$

$$= \frac{1974.207}{2}$$

$$\boxed{= 987.103}$$