

Final

Name

Tauseef Ali

I-D

7701

Section

B

instructor

Eng- Adeed.

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Subjected

hydraulic structure.

## Q 1 part (a)

### Culvert:

A Culvert is a structure constructed under roadways or railways to provide cross drainage or take electrical or other cable from one side to other.

Culvert is **OR** a small bridge having length of 5m or less than 5m.

Culvert is permanent drainage.

### Cause way:

Cause way is a road paved dip which allows the floods to pass over it. It may or may not have opening or vent to allow low water to flow.

cause way can be constructed of earth masonry, wood or concrete.

A Cause way is a track, road or railway on the upper part of an embankment across a low or wet place or piece of water.

**Culvert:**  
Culvert work as bridge to pass on it.

It is normally use for natural flow of water for controlling it

Culvert having a shape of tunnel carrying a stream of water under a road or Railway

**Type of culvert**

- Arch culvert -
- slab culvert -
- Box culvert -
- pipe culvert -

**Causeway:**  
It is supported mostly by earth or stone.

And it is not a bridge because it support a roadway between piers.

A cause way is built on an embankment

**Type of cause way**

- \* flush cause way
- \* low level causeway.
- \* high level causeway.

①  $\perp$  part(B)

## Q1 part (B)

### Cross drainage works:

Cross drainage work is a suitable structure must be constructed at crossing point for the easy flow of water of the canal and drainage in the respective direction. is known as cross drainage work.

### Necessary:

- \* It is required so that water is not interrupted. to dispose of the drainage. the canal supply water remain
- \* The water of canal and the drainage get inter mixed at the crossing point. The canal drainage work are required for the design discharge of smooth running.
- \* The water of canal and drainage can not be diverted to their natural direction. So the cross drainage must be required to maintain their natural direction of flow.

# Type of cross drainage

Type I (Irrigation canal passes over the drainage)

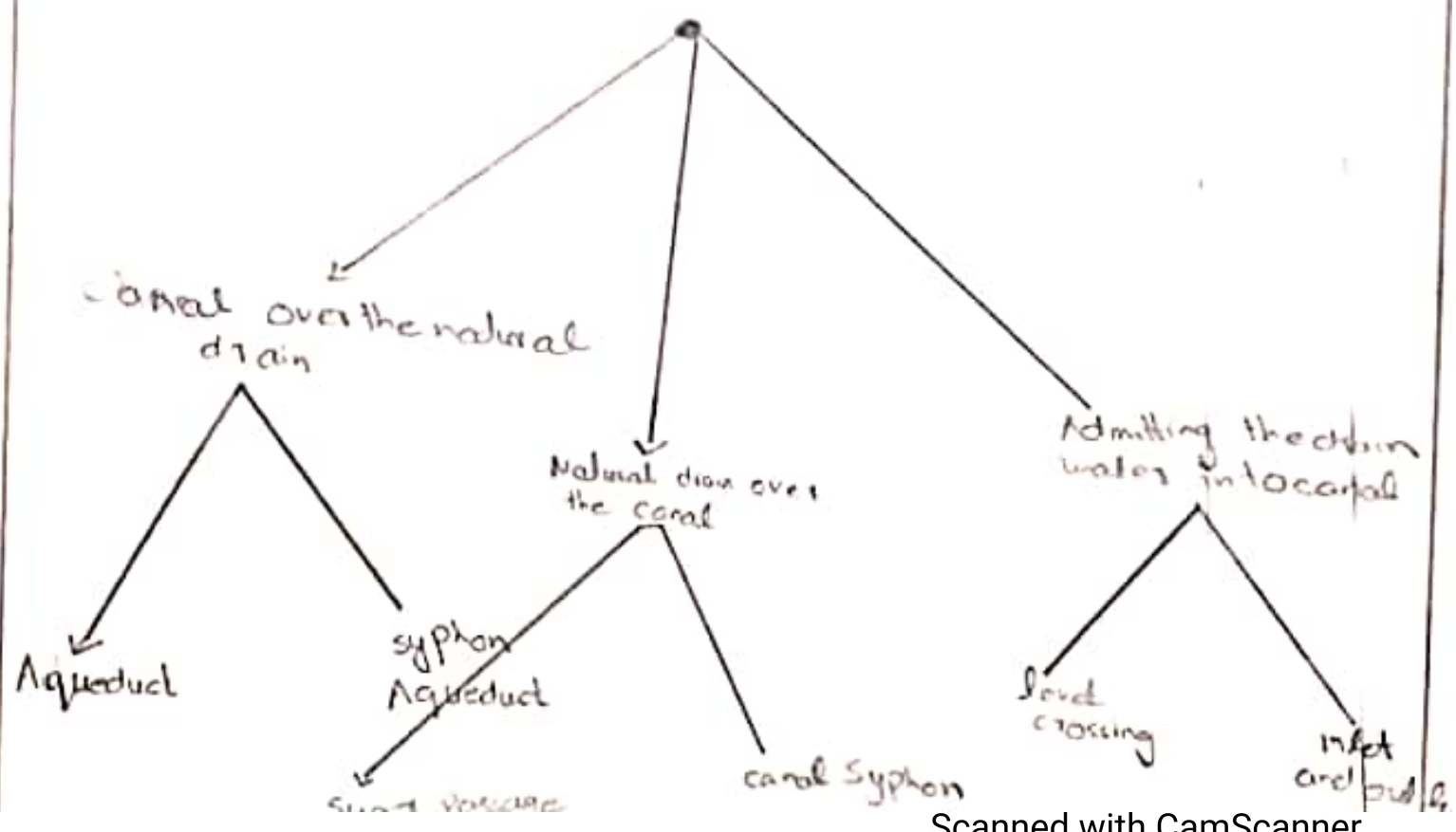
- (a) Aqueduct.
- (b) Siphon Aqueduct.

Type 2 (drainage pass over the irrigation channel)

- (a) Super passage.
- (b) Siphon super passage.

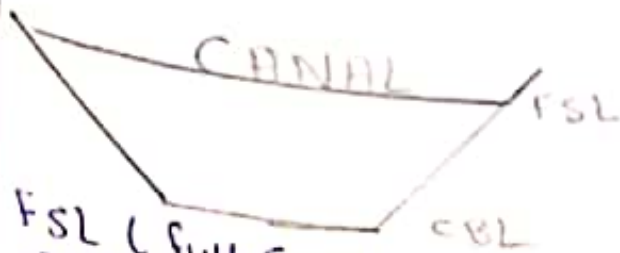
Type 3 (Drainage and channel intersection each other of the same level)

- (a) level crossing.
- (b) inlet & outlet.

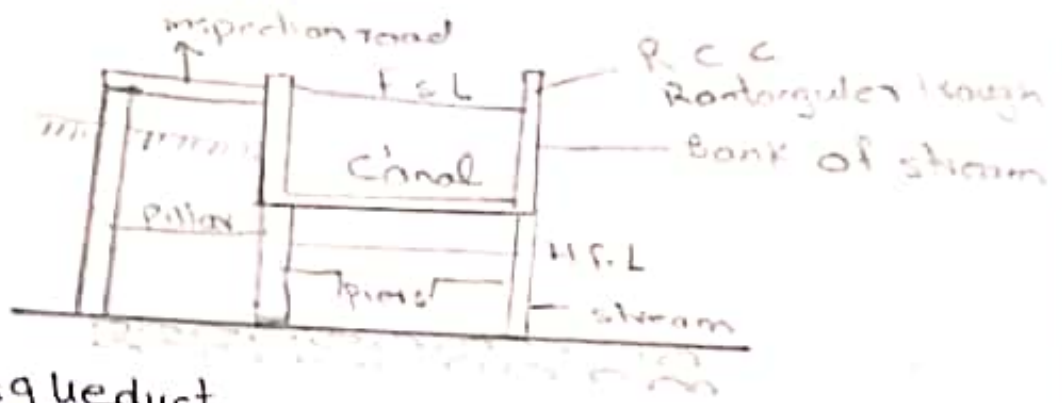


Types irrigation canal passes over the drainage.

Aqueduct: hydraulic structure in which the irrigation canal is taken over the drainage. The high flood level of drainage should remain lower than the level of the canal bed.



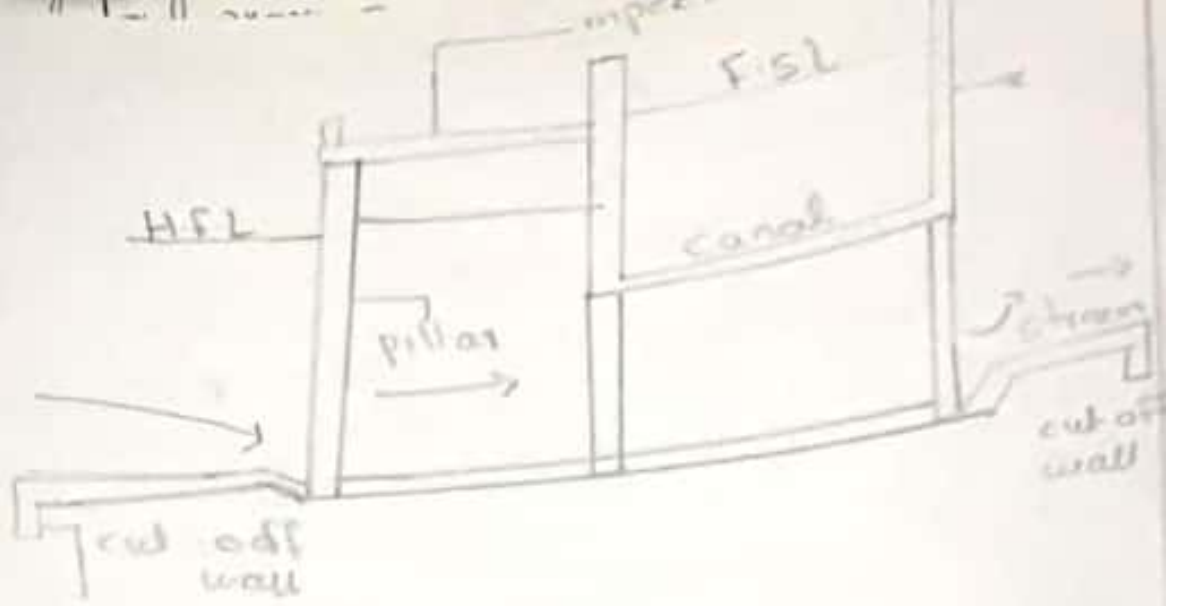
FSL (Full supply level)  
 CBL (canal bed level)  
 HFL (high flood level).  
 CBL (stream bed level).



Siphon Aqueduct

A structure where the canal is taken over the drainage but the drainage water cannot easily pass below the canal.

It is constructed where the water surface level of the drain at HFL is higher than then the canal bed.

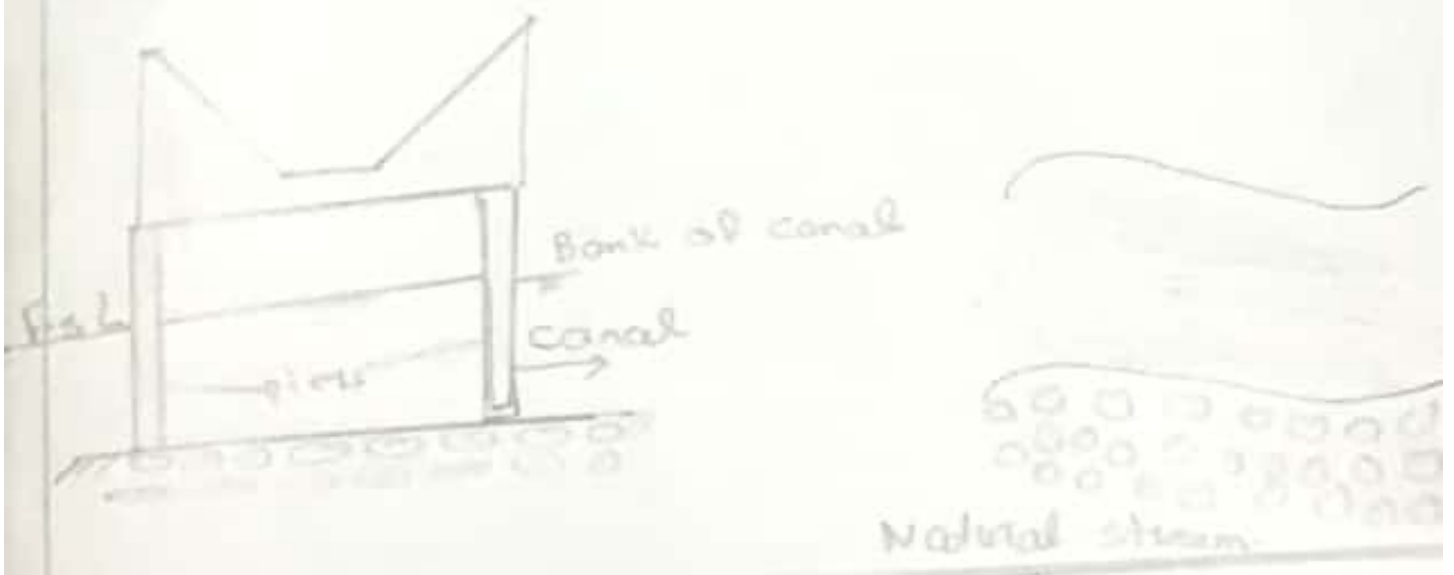


Type (2)

Super passage.

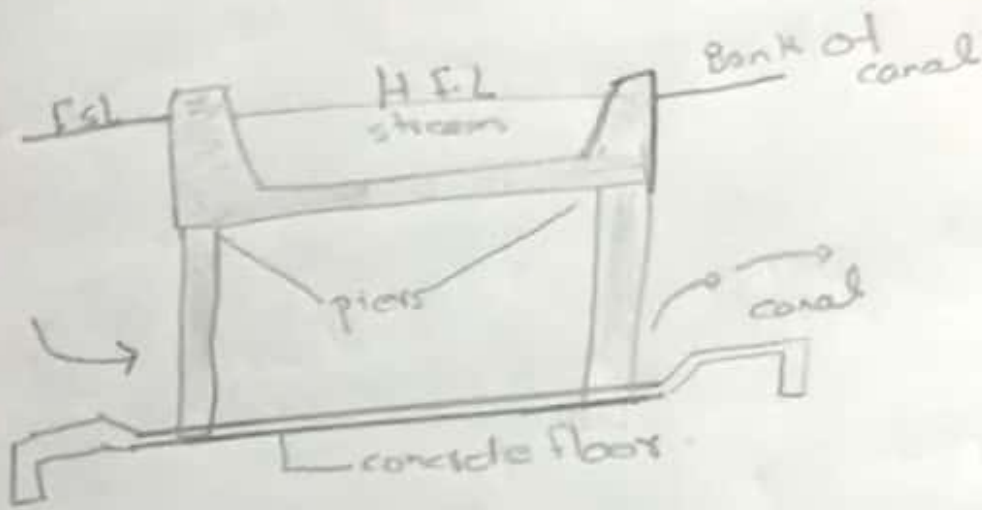
The structure in which the drainage canal is taken over the irrigation canal is known as super passage.

A super passage is reverse of Aqueduct. It is constructed where the the bed of drain is well above the canal F.S.L.



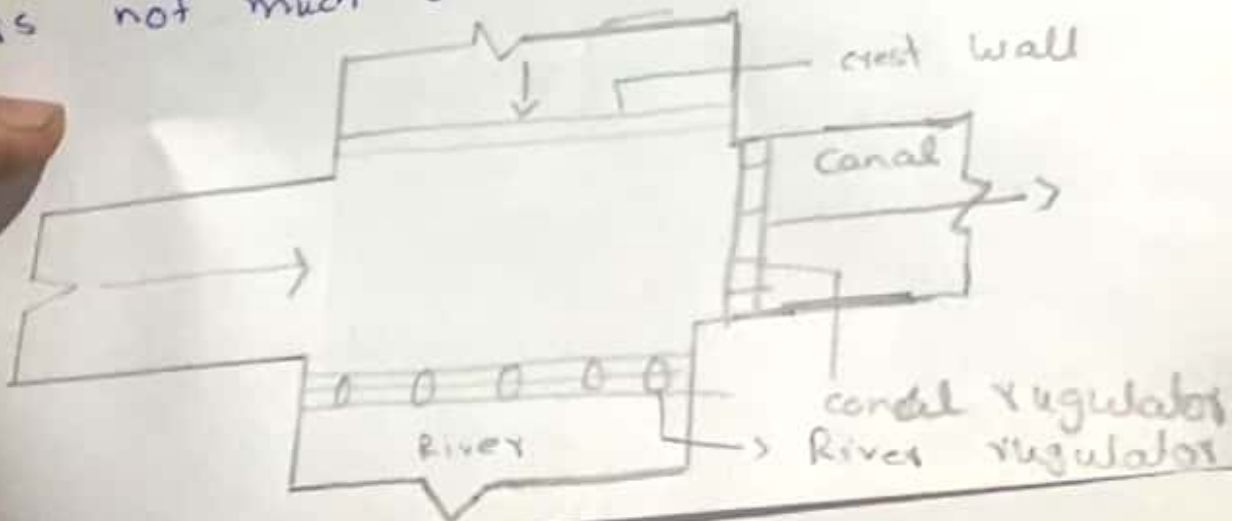
## Siphon super passage.

A structure in which the drain age is taken over the irrigation canal but the canal water passes below the drainage under siphonic action. Constructed where full supply level is higher than bed of the drain.



## Type # 3

level crossing  
When the bed level of canal and the stream are approximately the same and the quantity of water in canal and stream is not much different.





## Q #2 part (A)

**Wey:**

A low dam built across a river to raise the level of water upstream

Wey are commonly used to control the flow rate of river during period of high discharge.

Sluice gate is used to increase or decrease the volume of water going out

**Barrage:**  
A barrage is type of low head diversion dam which consist of number of large gate that can be opened or closed to control amount of water passing through.

Barrage are classified into three type.

- upstream sheet piles.
- intermediate sheet piles.
- Down stream sheet piles.

## Weir

low cost

low control on flow

gate over entire length

gate are of greater height

control on river flow

longer construction period

costly structure

## Barrages

high cost

Relatively high control on flow and water levels by operation of gate

shutter is part length.

shutter are of smaller height.

no control on river flow

shorter construction period

Relatively cheaper structure.

## Q No #2 part (b)

### Reynolds no:

It is a ratio of inertial force to viscous force is called Reynold number.

OR

The product of density time length divided by viscosity Co-efficient.

$$Re = \frac{\rho u D}{\mu} = \frac{\rho D}{\nu}$$

$\rho$  = density

$u$  = flow speed.

$D$  = Diameter.

$\mu$  = dynamic viscosity.

$\nu$  = Kinematic viscosity.

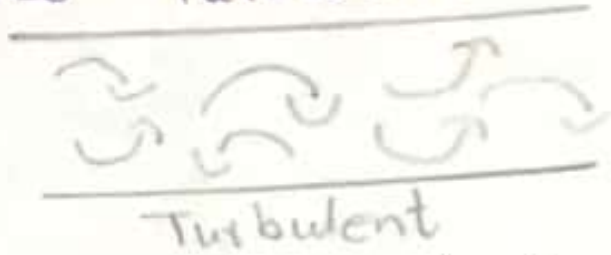
### laminar:

The flow in pipe is laminar if the Reynold number is less than 2000



laminar.

★ Turbulents: greater than 4000 then the flow is called Turbulent flow.



★ Neither laminar nor turbulent flow.  
When the Reynolds number is between 2000, and 4000, the flow is neither laminar or nor turbulent flow.

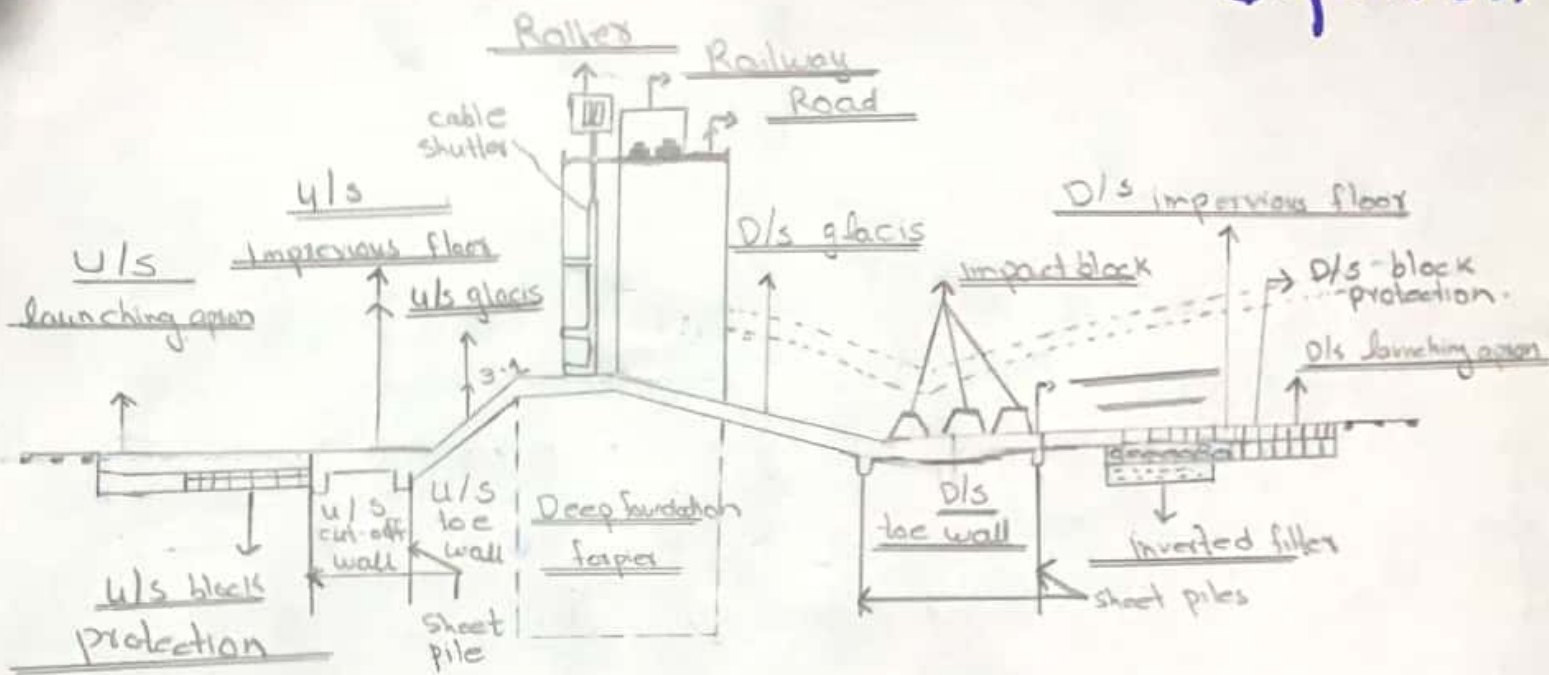
★ lower critical velocity.  
The velocity at which the flow change from laminar to transition is called lower critical velocity.

★ higher critical velocity.  
The velocity at which the flow change from transition to turbulent is called higher critical velocity.

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Q3 ≠ part A

Q3 part (A)



Component part of barrage

## Q3 part B

Several formulae based on experimental results have been proposed to predict 'maximum' or equilibrium scour depth ( $y_s$ , below general bed level) around bridge piers. In general these assume the relationship:

$$y_s/b' = \phi(y_0/b', Fr, d/b')$$

Where

$b'$  = is the pier width

$y_0$  = is the upper stream flow depth

$d$  = is the sediment size

$Fr$  = is the flow Froude number.

→ Laursen's (1962) experimental results underestimate the scour depth, compared to many Indian experiments (Ingilis 1949) which suggested the formula:

$$y_s/y_0 = 4.2(y_0/b')^{0.78} Fr^{0.52}$$

The Indian field data also suggested that the scour depth should be taken as twice regime scour depth.

In the case of live beds (a stream with bedload transport) the formula:

$$y_s/y_0 = (B/b') - 1$$

Predicts the maximum equilibrium scour depth

In a relation deep flow a first order estimate of local scour may be obtained by

$$y_s = 2.3 K_a b'$$

where  $K_a$  is angularity co-efficient which is the function of the pier alignment.

The live bed may contribute to an appreciable scour level scour distinctly layer and cover layer of thickness less than the local scour depth. The overall scouring phenomena is different.

The scour depth in the lowering layer,  $H$  is given by,

$$H = \eta (y_2 - y_1)$$

$y_1$  &  $y_2$  are uniform flow depth over a flat bed of grain toughness corresponding to the up stream surface particles ( $d_1$ ) and under lying surface fined particles ( $d_2$ ) respectively.

Co-efficient of  $\eta = 2.8$  for non rillle forming sediments. design purpose.

— The total scour depth may lead to a gross under estimate if the lower layer is of fine material.

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04

# Given data

Q4

$$L.L = 1500 \text{ lb/ft}^2$$

$$D.L = 300 \text{ lb/ft}^2$$

$$\text{thickness} = 3 \text{ ft}$$

$$\theta = 30^\circ$$

$$\text{unit of wt concrete} = 150 \text{ lb/ft}^3$$

$$F_y = 60 \text{ ksi}$$

$$\text{Section} = 15' \times 15'$$

$$\text{for 1-24 Rcc concrete} = 156 \text{ lb/ft}^3$$

## Solution:

• Self wt of slab:

$$\begin{aligned} & \text{Thickness} \times \text{unit wt of concrete} \\ & 3 \times 156 \text{ lb/ft}^3 \\ & = \boxed{468 \text{ lb/ft}^2} \end{aligned}$$

$$\begin{aligned} \bullet \text{ Total load} &= (L.L + D.L + \text{Self wt}) \\ &= 1500 + 300 + 468 \\ &= \boxed{2268 \text{ lb/ft}^2} \end{aligned}$$

• Co-efficient of earth pressure

$$\frac{1 - \sin \theta}{1 + \sin \theta} = \frac{1 - \sin 30}{1 + \sin 30} = 0.33$$



lateral pressure.

① vertical pressure at top  
(L.L + D.L)  $K_a$   
(1500 + 300) 0.33  
=  $\boxed{594 \text{ lb/ft}^2}$

② pressure of soil

$K_a \times h \times \text{unit wt of soil}$   
=  $0.33 \times 100 \times \cancel{15 + 3} (15 + 3)$   
=  $\boxed{\cancel{693 \text{ lb/ft}^2}}$  594 lb/ft<sup>2</sup>.

pressure at top =  $\boxed{594}$

pressure at bottom = top + pressure of soil

= 594 + 594  
= 1188 lb/ft<sup>2</sup>.

