

SYED JAWWAD

7386

GEOTECHNICAL ENGINEERING

Q#1

①

Define the following terms.

① PLASTIC EQUILIBRIUM:-

The Part of Soil is on verge of failure it is in state of Plastic Equilibrium. The stress strain behaviour of the soil here is rigid and with idealization of perfectly Plastic.

② ANGULAR DISTORTION:-

The structure is subjected to be angularly distorted if the two foundation support walls/columns

③ COMPRESSIVE INDEX:-

$$C_c = \frac{\Delta e}{\log_{10}(P_2/P_1)}$$

where  $\Delta e$  = Change in void Ratio

$P_1$  = Is the Pressure when the Void ratio is  $e_1$ .

$P_2$  = Is the Pressure when the void ratio is  $e_2$ .

## ULTIMATE BEARING CAPACITY

It is denoted by " $q_u$ ". It is the maximum Pressure applied on the base of footing that Cause shear failure of Soil.

## POISSON RATIO OF SOIL:-

- Poisson Ratio Represents a Change in Shape of a material while the Volume is maintained constant.
- In Soil terminology, Poisson's Ratio also known as the Coefficient of lateral expansion and is affected by the following factors.
- The Soil is a discrete and Stratified medium, mostly not elastic and anisotropic
- The Soil is not deformed linearly.

Poisson's Ratio in Soil mechanics is a rather Conditional Parameter.

(Q No 1 # Part # B)

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Q A 6m tall Cantilever wall retaining the Soil that has the following Properties.

- $c = 0$
- $\phi = 30^\circ$
- $\gamma = 19.2 \text{ kN/m}^3$

And the ground surface behind the wall is inclined at a slope of 3 horizontal and 1 vertical. The wall has moved sufficiently to develop active condition. Determine the total normal and shear forces acting on the back of this wall using Rankine's Theory.

GIVEN DATA:-

Cohesion ( $c$ ) = 0

Angle of Internal Friction ( $\phi$ ) =  $30^\circ$

Unit weight of Soil ( $\gamma$ ) =  $19.2 \text{ kN/m}^3$

Horizontal Slope = 3

Vertical Slope = 1

REQUIRED:-

Total Normal force ( $N_a/b$ ) = ?

Total shear force ( $V_a/b$ ) = ?

Sol:-

As we know that

Active force is given by

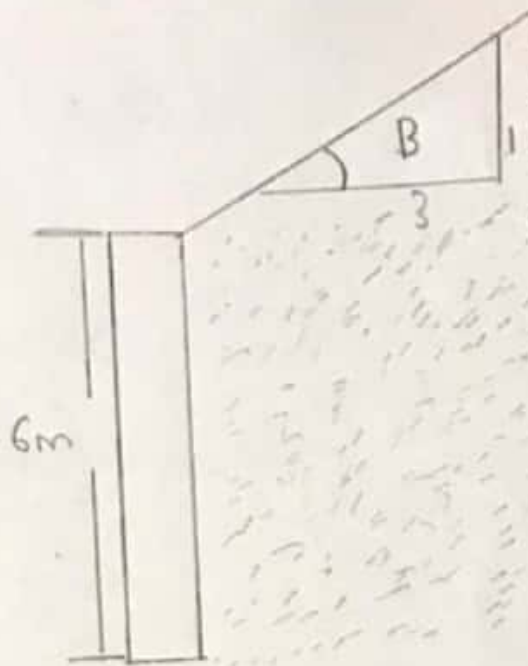
$$\frac{P_a}{b} = \frac{\gamma \cdot H^2 \cdot k_a}{2}$$

As  $\tan(B) = \frac{\text{Perpendicular}}{\text{Base}}$

$$\tan(B) = 1/3$$

$$B = \tan^{-1}(1/3)$$

$$B = 18^\circ$$



Also  $k_a$  is given by,

$$k_a = \cos B \times \frac{\cos B - \sqrt{\cos^2 B - \cos^2 \phi}}{\cos B + \sqrt{\cos^2 B - \cos^2 \phi}}$$

$$= \cos(18) \times \frac{\cos(18) - \sqrt{\cos^2(18) - \cos^2(30)}}{\cos(18) + \sqrt{\cos^2(18) - \cos^2(30)}}$$

$$= 0.951 \times \frac{0.951 - \sqrt{0.904 - 0.75}}{0.951 + \sqrt{0.904 - 0.75}}$$

$$k_a = 0.3948$$

$$k_a = 0.395$$

Now By formula

$$\text{Active force } P_a/b = \frac{\gamma H^2 \cdot k_a}{2}$$

$$= \frac{19.2 \times (6)^2 \times 0.395}{2}$$

$$\frac{P_a}{b} = 136.512 \text{ kN/m}$$

$$P_a/b = 136.52 \text{ kN/m}$$

As the Normal force is,

$$\frac{N_g}{b} = \frac{P_g}{b} \cdot \cos \beta$$
$$= 136.52 \times \cos(18)$$

$$\frac{N_g}{b} = 129.83 \text{ kN/m}$$

Also the shear force is

$$\frac{V_g}{b} = \frac{P_g}{b} \cdot \sin \beta$$
$$= 136.52 \times \sin(18)$$

$$\frac{V_g}{b} = 42.18 \text{ kN/m}$$

# FACTOR AFFECTING BEARING CAPACITY

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## ① RELATIVE DENSITY:-

If the Density of Soil is greater, the value of angle of Internal friction " $\phi$ " will be higher. The higher the value of " $\phi$ ", higher the value of Terzaghi's Bearing factors ( $N_s$ ,  $N_c$  and  $N_e$ ). Bearing Capacity will be higher if values of  $N_a$ ,  $N_r$  and  $N_q$  are greater. Hence Enough Bearing Capacity of Soil will have enough Relative Density.

## ② DEPTH OF FOOTING:-

The bearing Capacity of Soil is directly Proportional to the Depth of footing. Increase in this will have Maximum effect on dense soil as compared to loose Sand.

## ③ BREADTH OF FOOTING

The Unit weight of Soil is known as Breadth of footing.

~~④ UNIT WEIGHT OF SOIL~~

## BEARING CAPACITY:-

Applying resistance to the load is known as Bearing Capacity. It's also known as Internal strength of Soil, which is denoted by " $q_v$ ".

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## (PART-B)

Q what is the maximum safe load which can be supported by a rectangular footing  $2m \times 3m$  with a safety factor of 3. The base of the footing is at  $1.6m$  below the ground surface. The unit weight of soil is  $18kN/m^3$ . The angle of shear resistance  $(\phi) = 20^\circ$ . ( $N_c = 14.8$ ) ( $N_q = 6.4$ ;  $N_r = 2.9$ ). Unit Cohesion  $C_u = 20kN/m^2$ . Use Meyerhoff Analysis.

Given Data:-

Footing Dimensions:  $2m \times 3m$  ( $b = 3, h = 2$ )

Factor of Safety = 3

Depth of foundation (DF) =  $1.6m$

Unit weight of soil ( $\gamma$ ) =  $18kN/m^3$

Angle of shear resistance  $(\phi) = 20^\circ$

Unit Cohesion ( $C_u$ ) =  $20kN/m^2$

$N_c = 14.8$

$N_q = 6.4$

$N_r = 2.9$

Required:-

Maximum Safe Load ( $Q_{s}$ ):?



Solution:-

According to Meyerhoff's Analysis,

$$q_u = c \cdot N_c \cdot S_c \cdot d_c + \gamma \cdot N_q \cdot S_q \cdot d_q + \frac{1}{2} \gamma \cdot B \cdot N_r \cdot S_r \cdot d_r$$

→ For Shape factors:- (S<sub>c</sub>, S<sub>q</sub>, S<sub>r</sub>)

$$S_c = 1 + 0.2 (B/L) \tan^2 \alpha$$

$$\Rightarrow \alpha = (45 + \phi/2)$$

$$= 45 + \frac{20}{2}$$

$$\alpha = 55^\circ$$

$$S_c = 1 + 0.2 (2/3) \tan^2 (55)$$

$$S_c = 1.27$$

As  $\phi > 10^\circ$ , So

$$S_q = S_r = 1 + 0.1 (B/L) \tan^2 \alpha$$

$$= 1 + 0.1 (2/3) \tan^2 (55)$$

$$S_q = S_r = 1.135$$

→ For Depth Factors:- (d<sub>c</sub>, d<sub>q</sub>, d<sub>r</sub>)

$$d_c = 1 + 0.2 \left(\frac{D_f}{B}\right) \tan \alpha$$

$$= 1 + 0.2 (1.6/2) \tan (55)$$

$$d_c = 1.22$$

Also  $\phi > 10^\circ$ , So

$$d_q = d_r = 1 + 0.1 (D/B) \tan \alpha$$

$$d_q = d_r = 1 + 0.1 \frac{(1.6)}{2} \tan(55)$$

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$$d_q = d_r = 1.11$$

INCLINATION FACTORS:-

For  $\alpha = 0^\circ$

$$i_c = i_q = i_r = 1$$

By formula

$$q_u = C N_c \cdot s_c \cdot d_c + q N_q \cdot s_q \cdot d_q + \frac{1}{2} \gamma B N_r \cdot d_r \cdot s_r$$

$$= (20)(14.8)(1.27)(1.22) + [(1.6 \times 18)](6.4)(1.135)(1.11) + \frac{1}{2}(18)$$

$$(2)(2.9)(1.11)(1.135)$$

$$q_u = 762.1 \text{ kN/m}^2$$

As Net Ultimate Bearing Capacity is

$$q_{n.u} = q_u - \bar{\sigma}$$

$$q_{n.u} = 733.2 \text{ kN/m}^2$$

Net Safe Bearing Capacity is

$$q_{n.s} = \frac{q_{n.u}}{F.O.S} = \frac{733.2}{3} = 244.4 \text{ kN/m}^2$$

Safe Bearing Capacity is

$$q_s = q_{n.s} + \bar{\sigma}$$

$$= 244.4 + (1.6 \times 18)$$

$$= 244.4 + (1.6 \times 18)$$

$$q_s = 273.2 \text{ kN/m}^2$$

This Safe Bearing Capacity.

$$\Rightarrow A \times q_s = 273.2 (6m^2)$$

$$= \boxed{1639.2 \text{ kN}}$$

## Q #3 Part-A

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### SETTLEMENT:-

Load is applied on the ground surface

Causing stress which lead to vertical strain.

This vertical strain causes movement in downward direction as settlement.

### TYPES:-

#### ① TOTAL SETTLEMENT:-

Also known as uniform settlement because of the fact that each part of the structure is settled equally. Failure is rare in this case as structure is tend to be rigid ~~the~~ utility services such as water supply, electricity is provided in order to keep the structure firm and sound.

#### ② LIMITATION SETTLEMENT:-

① The soil should have right bearing capacity to resist the load applied

② The load has to cover the large area.

### DIFFERENTIAL:-

Here the structure is not uniform as the settlement is done in different parts of structure it's more dangerous than uniform or total settlement.

TYPES:-

① TILT:-

The entire structure is rotated and leads to un-equal Settlement.

② ANGULAR DISTORTION:-

The structure is subjected to be Angularly distorted if the two foundation supports walls/Columns.

Q: A Soil has Compressive Index ( $cc = 0.31$ ). At a Stress of  $130 \text{ kN/m}^2$ , the void ratio was 1.02. Calculate.

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- 1- The void ratio if the stress on the soil is increased to  $170 \text{ kN/m}^2$
- 2- The total Settlement of the stratum of 5m thickness

Given Data:-

Compressive Index of soil ( $cc$ ) = 0.31

Initial Stress / Pressure ( $P_1$ ) =  $130 \text{ kN/m}^2$

Initial Void Ratio ( $e_0$ ) = 1.02

Increased or final Stress / Pressure ( $P_2$ ) =  $170 \text{ kN/m}^2$

Stratum thickness ( $H$ ) = 5m

Required:-

Final void ratio due to increased stress ( $e_1$ ) = ?

Total (Consolidation) Settlement ( $S_c$ ) = ?

Solution:-

As Compressive Index is given by,

$$cc = \frac{\Delta e}{\log_{10}(P_2/P_1)} = \frac{e_0 - e_1}{\log_{10}(P_2/P_1)}$$

$$0.31 = \frac{1.02 - e_1}{\log_{10}(170/130)} \Rightarrow 0.31 \times 0.1163 = 1.02 - e_1$$

$$\boxed{e_1 = 0.984}$$

By formula

~~Consolidation~~  
Consolidation Settlement is

$$S_c = \frac{H}{1+e_0} \times C_c (\log_{10}) (P_2/P_1)$$

$$= \frac{5}{1+1.02} \times 0.31 \times \log_{10} (170/130)$$

$$= 0.0893m \times 1000mm$$

$S_c = 89.3m$