

Q No: 1 Part 'A'

a:- Hydraulic gradient:

The difference between two hydraulic heads taken from the soil specimen over the distance of flow in the soil specimen when measured is called hydraulic gradient.

The expression to compute hydraulic gradient is given below

$$i = \frac{\Delta h}{\Delta L}$$

b:-

The description of how easily a liquid will move through a soil is called coefficient of permeability of soil and it is also called hydraulic conductivity of soil.

c:-

Liquidity index of soil Liquidity index is defined to understand the consistency of soil particles and it is represented by LI. It is defined as the ratio of the difference b/w the natural water content of the soil and its plastic limit to its plasticity index.

d:-

Soil porosity" refers to the amount of pores or open space between soil particles. These spaces may be formed due to the movement of roots, worms and insects; expanding gases trapped within these spaces by ground water; and/or the dissolution of the soil parent material.

e:-

The degree of saturation is the ratio of the volume of water to the volume of voids. It is denoted by 'S'. $S = V_w / V_v$. The degree of saturation generally expressed as a percentage. It is equal to zero when the soil is absolutely dry and 100% when the soil is fully saturated.

Q No: 1 Part 2

Q: A sample of wet soil has a volume of 0.0192 m^3 and a mass of 32 kg . After drying the samples in an oven its mass reduces to 28.5 kg . Determine i) Bulk density ii) water content iii) Dry density iv) Saturated density v) Void ratio vi) Porosity vii) Degree of saturation.

Take Sp-Gravity of soil solid as 2.65

Given data:- $W = 32 \text{ kg}$, $V = 0.0192 \text{ m}^3$, $W_s = 28.5 \text{ kg}$
 $G_s = 2.65$

Required:- $\gamma_b = ?$, $w = ?$, $\gamma_d = ?$, $\gamma_{sat} = ?$
 $e = ?$, $n = ?$, $s = ?$

Solution:-

$$W_w = W - W_s = 32 - 28.5 = 3.5 \text{ kg}$$

$$w = \frac{W_w}{W_s} \times 100 = \frac{3.5}{28.5} \times 100 = 12.3 \%$$

$$\gamma_b = \frac{W}{V} = \frac{32}{0.0192} = 1666.67 \text{ kg/m}^3$$

$$\gamma_d = \frac{W_s}{V} = \frac{28.5}{0.0192} = 1484.37 \text{ kg/m}^3$$

$$\gamma_d = \frac{G_s \times \gamma_w}{1+e} \Rightarrow e = \frac{G_s \times \gamma_w}{\gamma_d} - 1 = \frac{2.65 \times 10000}{1484.37} - 1$$

$$\gamma_{sat} = \frac{(G_s + e) \gamma_w}{1+e} = \frac{(2.65 + 0.785) \times 10000}{1 + 0.785} = 1924.31 \text{ kg/m}^3$$

QNo: 2 'A'

Prove that $e = \frac{r_s \cdot r_w (1 + w_c)}{r_b} - 1$

$$r_b = \frac{W}{V} = \frac{W_s + W_v}{V_s + V_v} = \frac{W_s (W_s + W_v)}{V_s (V_s + V_v)}$$

$$r_b = \frac{W_s \left(\frac{W_s}{V_s} + \frac{W_v}{V_v} \right)}{V_s \left(\frac{V_s}{V_s} + \frac{V_v}{V_v} \right)} = \frac{W_s \left(1 + \frac{W_v}{W_s} \right)}{V_s \left(1 + \frac{V_v}{V_s} \right)}$$

$$r_s = \frac{W_s}{V_s} = w_c = \frac{W_v}{W_s}, \quad e = \frac{V_v}{V_s}$$

$$r_b = \frac{r_s (1 + w_c)}{1 + e}$$

$$\therefore r_s = \frac{r_b}{r_w}$$

$$r_s = r_b r_w$$

$$r_b = \frac{r_s \cdot r_w (1 + w_c)}{1 + e}$$

$$1 + e = \frac{r_s \cdot r_w (1 + w_c)}{r_b}$$

$$e = \frac{r_s \cdot r_w (1 + w_c)}{r_b} - 1$$

Hence proved.

Q No 2 'B'

i - Grain size Classification / Particle Size Classification

i - US - Bureau of Soil Classification

Clay	Silt	Sand				Gravel	
		Very fine sand	Fine sand	Medium sand	Coarse sand	Fine gravel	Coarse gravel
		0.075 mm	0.075 mm	0.25 mm	0.5 mm	4.75 mm	20 mm

ii - ASTM soil classification System

American Society of Testing and Material

Clay	Colloidal or colloidal clay	Silt	Sand		Gravel
			Fine sand	Coarse sand	
			0.075 mm	0.25 mm	2.0 mm

iii - MIT Soil classification System

Massachusetts

Clay			Silt			Sand			Gravel
Fine clay	Medium clay	Coarse clay	Fine Silt	Medium Silt	Coarse Silt	Fine Sand	Medium Sand	Coarse sand	
0.002 mm	0.006 mm	0.02 mm	0.002 mm	0.006 mm	0.02 mm	0.06 mm	0.2 mm	0.6 mm	2.00 mm

Q No: 3'A'

Quick sand:- When the seepage pressure due to upward flow of water in sand/sandy soil balance the downward force of gravity (weight of material) a condition of instability rises in sand. Sand in this state is called quick sand.

* Seepage flow of water under gravitational forces in a permeable medium.

Critical hydraulic gradient:-

At the bottom surface.

i.e. at x-x.

$$\text{upward force} = (h-L)\gamma_w \cdot A \rightarrow (1)$$

$$\text{Downward force} = \gamma_w \times \frac{(G_s + e)}{(1+e)} \times V$$

$$\text{Since } \gamma_B = \frac{W}{V} \Rightarrow W = \gamma_w \frac{(G_s + e)}{1+e} \times V$$

$$W = \gamma_w \times \frac{(G_s + e)}{(1+e)} \times A \times L \rightarrow (2) \quad \text{where } V = A \times L$$

The soil is literally behaving like a liquid rather than solid.

$$\text{At balance ; Upward force} = \text{Downward force}$$
$$(h+L)\gamma_w \cdot A = \gamma_w \times \frac{(G_s + e)}{1+e} \times A \times L$$

$$\frac{h+L}{L} = \frac{G_s + e}{1+e} \times \frac{L}{L}$$

$$\frac{h}{L} + 1 = \frac{g_s + e}{1 + e}$$

$$\therefore \frac{h}{L} = \frac{g_s + e}{1 + e} - 1$$

$$\dot{i}_c = \frac{g_s + e - 1}{1 + e} - \cancel{e}$$

$$\dot{i}_c = \frac{g_s - 1}{1 + e}$$

Q No: 3 Part 'B'

Given data:-

$$V = 65 \text{ ml} = 0.000065 \text{ m}^3 \quad \text{As } 1 \text{ ml} = 10^{-6} \text{ m}^3$$

$$W = 0.96 \text{ N} \quad \text{and } W_d = 0.785 \text{ N}$$

$$G_s = 2.65$$

Required: $S = ?$

Solution: $\gamma_B = \frac{\gamma_w \times (G_s + e)}{(1+e)} \quad \text{--- (1)}$

$$\gamma_B = \frac{W}{V} = \frac{0.96}{0.000065} = 14769 \text{ N/m}^3$$

$$\gamma_w = 9800 \text{ N/m}^3$$

$$\frac{W_d}{V_d} = \frac{V_v}{V_s}$$

$$V_s = 0.000065 \text{ m}^3$$

$$\text{As } \frac{W_d}{V_d} = \frac{U_s}{V_s}$$

$$U_s = \frac{W_d}{\gamma_s} = \frac{0.785}{25970}$$

$$e = 0.000035$$

$$0.000030$$

$$e = 1.167$$

Also;

$$V = V_v + V_s$$

$$V_v = V - V_s$$

$$V_v = 0.000065 - 0.000030$$

$$V_v = 0.000035 \text{ m}^3$$

$$V_s = 0.000035 \text{ m}^3$$

But $G_s = \frac{\gamma_s}{\gamma_w}$

$$\gamma_s = G_s \times \gamma_w$$

$$\gamma_s = 2.65 \times 9800$$

$$\gamma_s = 25970 \text{ N/m}^3$$

Putting the values in (1)

Eq. Solve it for S

$$S = 0.527 \text{ or } 52.7 \%$$