

Name

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M. Usama

ID

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14150

Subject

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Power System Analysis

Semester

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6<sup>TH</sup>

Submitted to

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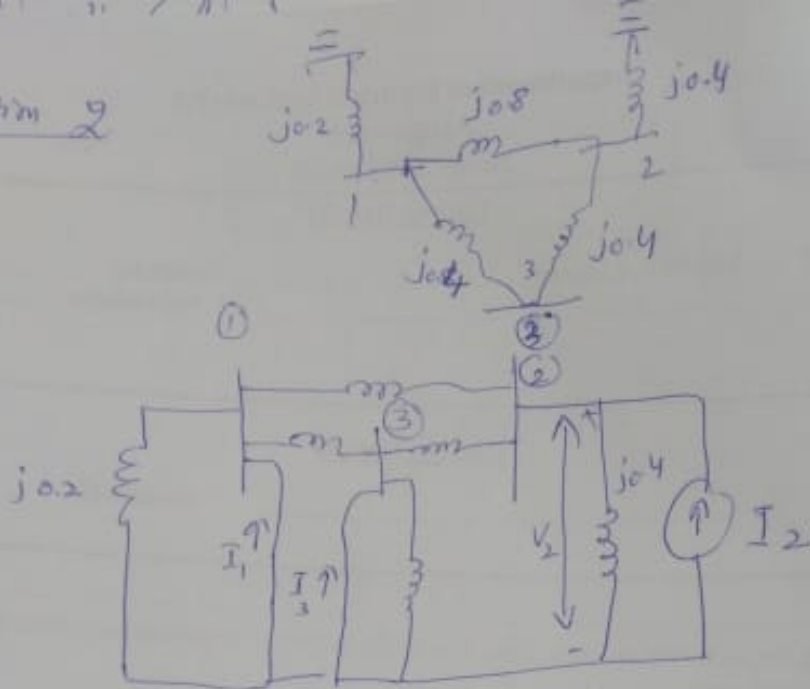
Engr: Amir Aman.

Date

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23/01/2020.

Question 2



$$Z_{bus} = \begin{bmatrix} Z_{11} & Z_{12} & Z_{13} \\ Z_{21} & Z_{22} & Z_{23} \\ Z_{31} & Z_{32} & Z_{33} \end{bmatrix}, I = Y_{bus} V \text{ (A)}$$

Diagonal element:

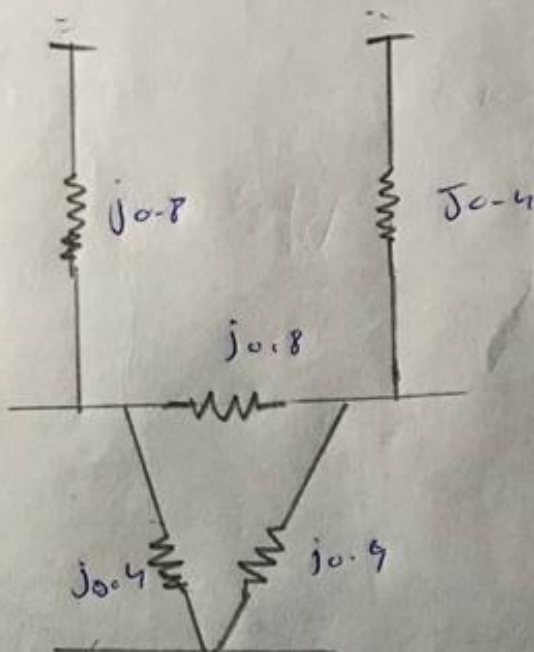
$Z_{11}, Z_{22}, Z_{33}$  are driving point impedances of nodes

while transfer impedances are  $Z_{12}=Z_{21}, Z_{13}=Z_{31}, Z_{23}=Z_{32}$ .

$$Z_{bus} = \begin{bmatrix} j(0.2+0.8+0.4) & -j0.8 & -j0.4 \\ -j0.8 & j(0.4+0.8+0.4) & -j0.4 \\ -j0.4 & -j0.4 & j(0.4+0.4) \end{bmatrix}$$

$Q = 2$

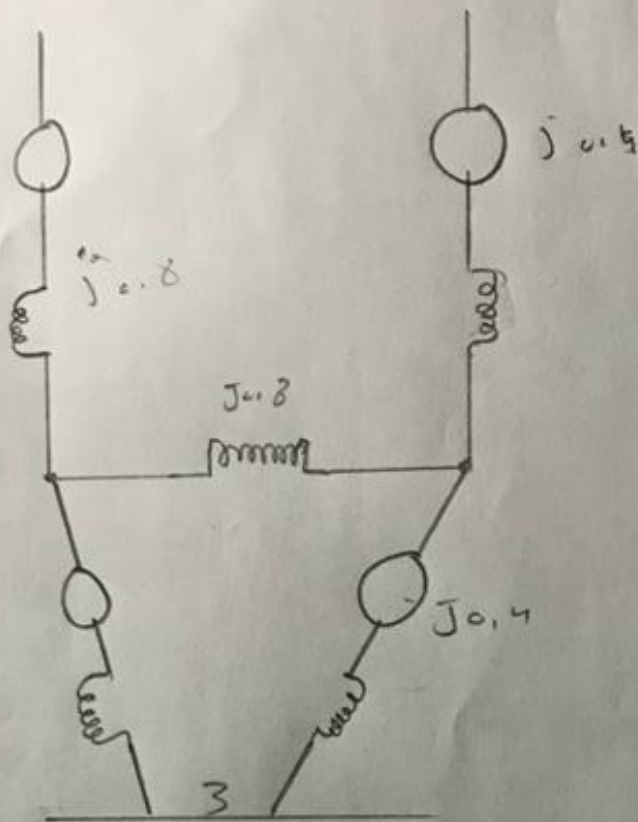
Ans



$Z_{base} = Y_{base}$

$Z_{base}$

$Z_{11}$	$Z_{12}$	$Z_{13}$
$Z_{21}$	$Z_{22}$	$Z_{23}$
$Z_{31}$	$Z_{32}$	$Z_{33}$



$$\begin{bmatrix} V_1 \\ V_2 \\ V_3 \end{bmatrix} = \begin{bmatrix} Z_{11} & Z_{12} & Z_{13} \\ Z_{21} & Z_{22} & Z_{23} \\ Z_{31} & Z_{32} & Z_{33} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

$$V_1 = Z_{11} I_1 + Z_{12} I_2 + Z_{13} I_3 \quad \dots \quad (1)$$

$$V_2 = Z_{21} I_1 + Z_{22} I_2 + Z_{23} I_3 \quad \dots \quad (2)$$

$$V_3 = Z_{31} I_1 + Z_{32} I_2 + Z_{33} I_3 \quad \dots \quad (3)$$

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$Q = 3$

Ans A 10kW generator is connected which injects  $P_{Gk}, Q_{Gk}$  to the "11kV" Busbar. A 90kW Load is connected which takes  $P_{Lk}, Q_{Lk}$  from the 11kV Busbar. This 11kV Busbar is connected to other Busbar i.e. to bus  $i$  and on through lines. The ~~voltage~~<sup>voltage</sup> at 11kV Busbar is  $V_c$ . Where  $L_k$  is equal to the magnitude  $V_k$  and the angle  $\delta_k$ .

$\Rightarrow$  one thing we see that injects  $P_{Gk}$  &  $Q_{Gk}$  while Load takes  $P_{Lk}$  &  $Q_{Lk}$  from the Busbar then we can take the algebraic sum of generation, and Load, i.e. subtraction the Loads from the generation

$$i.e. = P_k = P_{Gk} - P_{Lk} \therefore \text{Real Power injection}$$

From the diagram we see that we have three lines one going to 11kV busbar, 2nd to  $i$ , and the third one to  $m$ . These lines will carry the power  $P_{ki}, Q_{ki}$  to bus  $i$ ,  $P_{kj}, Q_{kj}$  to bus  $m$  and  ~~$P_{km}, Q_{km}$  to bus  $m$~~

$\Rightarrow$  Some of these power may be in the reverse direction i.e bus  $k$ , in that case The value of  $P_{ic}$ ,  $Q_{ic}$  will be negative.

$$\text{So, } P_{ic} = P_{ici} + P_{ikj} + P_{icm}$$

$$Q_{ic} = Q_{icki} + Q_{ikj} + Q_{ickm}$$

$\therefore$  Real and Reactive power is equal to the algebraic sum  $P, Q$  &  $Q$  power going out.

Power flow equation  $\Rightarrow$  we showed that, Power flow equation are coming from the network equation.

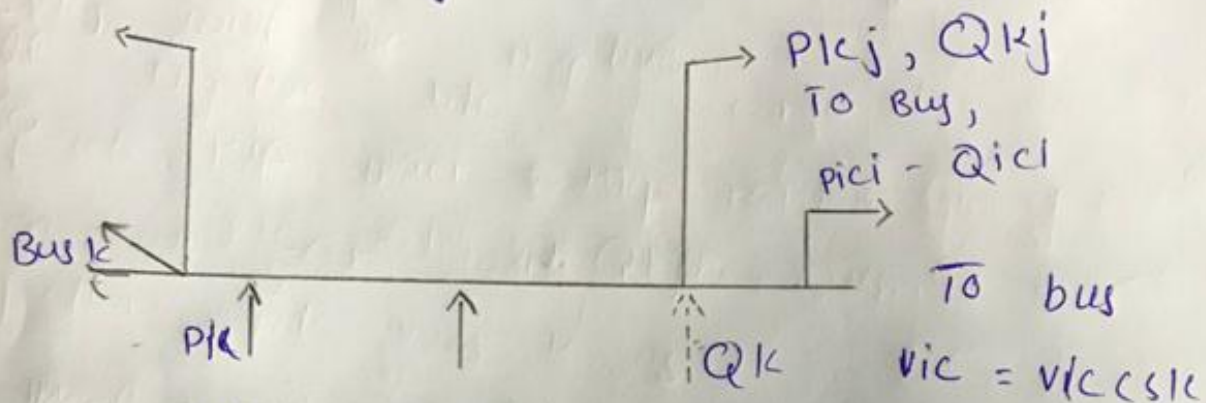
$$\text{i.e. } I_{Bus} = Y_{Bus} U_{Bus} \quad \text{--- (1)}$$

when  $I_{Bus}$  is the vector of

Similarly reactive power injection is

$$Q_k = Q_{Gik} = Q_{Lk}$$

Then the diagram became as



⇒ Now will say the injection into the 11 kV busbar. Rather saying the generation and loads. If a particular generation input in only load is connected then the injection to that 11 kV busbar will be ∴

$$P_k = 0 - P_{Lk}$$

$$P_k = P_{Lk}$$

$$\text{∴ } Q_k = 0 - Q_{Lk}$$

$$Q_k = - Q_{Lk}$$

So, Load can be considered as negative injection.

$$R_k + jQ_k = V_k \sum_{n=1}^N y_{kn} V_n e^{i(\delta_k - \delta_n - \theta_{kn})}$$

∴ All angles  $\delta_k$  with  $V_k$   $\delta_n$  with  $V_n$   
 $\theta_{kn}$  with  $y_{kn}$

all Negative b/c of conjugates we can separate out the real & imaginary parts. Then we can write the real power injection into Bus  $k$  as

$$P_k = V_k \sum_{n=1}^N y_{kn} V_n \cos(\delta_k - \delta_n - \theta_{kn}) \quad \text{eq (4)}$$

Similarly the reactive power injective

$$Q_k = V_k \sum_{n=1}^N y_{kn} V_n \sin(\delta_k - \delta_n - \theta_{kn}) \quad \text{(5)}$$

So, we can see that these injection is related to the voltage magnitude and angle at remain bus bars

Eq (4) and (5) is said as, the power flow equation for the power Network.



Current injection into the bus bars  $y_{Bus}$  is the  $n \times n$  matrix of  $x$ . admittance and  $V_{Bus}$  in the voltage phases at the busbar of  $k$  power system

$\Rightarrow$  For a particular bus  $k$ , we can write the equation as,  $I_k = \sum_{n=1}^N y_{kn} V_n \rightarrow (2)$

where  $N =$  no of bus bar.

$y_{kn} =$  admittance of the  $kn$  element

$V_n =$  voltage phases at busbar  $k$  is

$$S_k = P_k + jQ_k = V_k I_k \rightarrow (3)$$

Now we know the value of  $I_k$

from eq (2) substituting  $I_k$  in eq (3)

$$P_k + jQ_k = V_k \left[ \sum_{n=1}^N y_{kn} \right] V_n$$

where  $k = 1, 2, N$

$V_n$  is a phasor, which has a magnitude and an angles  $V_n = V_n e^{j-\delta_n}$

and  $y_{kn} = y_{kn} e^{j\theta_{kn}}$ ,  $k, n = 1, 2, N$

substituting  $V_n$  and  $y_{kn}$  values in eq (b)

Q = 4

M. Usama

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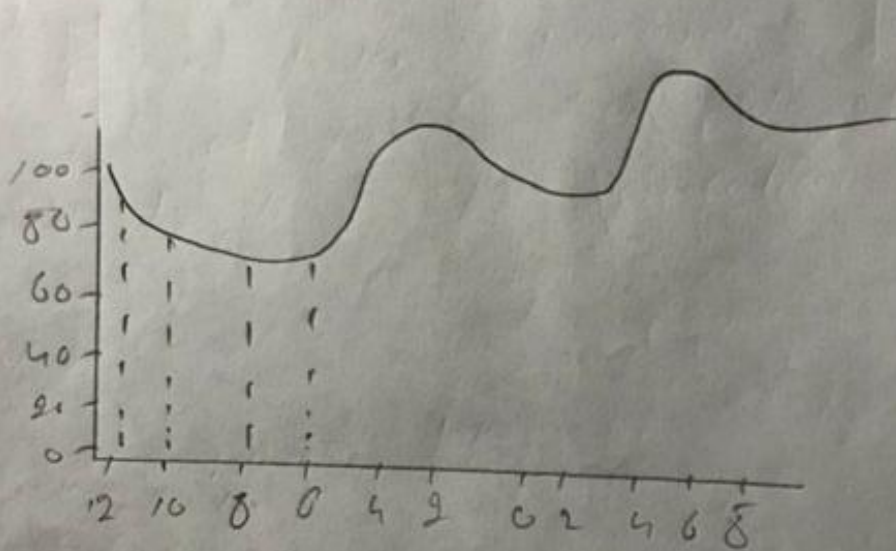
Ans There is one problem in doing power flow solution that we cannot know all the generations. All the loads are known to us but generations are in our control and one can say that all generations known to us. But there is one problem. The problem is still all the generations are available we don't know what is the loss in the system. sure we cannot know the loss in the system. we cannot know how much generation because the sum of load and the no of losses must be equal to the total generation.

Solution  $\Rightarrow$

To overcome this we chose one bus as a reference bus which takes up all these losses which can find after solution. So at one bus we cannot specify the generation. Generally this is a bus which have very large generation available.

So that there will be no problem for it to take a loss. This bus is power system terminology is called slack bus.

Load curves :-



$$\underline{Q = S}$$

(Ans)

This is the fixed iterative method  
find-out the power flow equation for  
these method we again start with the  
basic of network equation.

$$\text{i.e. } I_{\text{Bus}} = Y_{\text{Bus}} - V_{\text{Bus}}$$

and for any particular Bus is

$$I_k = \sum_{n=1}^N Y_{kn} \cdot V_n$$

The complex power  $P_k + jQ_k = V_k I_k$

$$P_k + jQ_k = V_k \left[ \sum_{n=1}^N Y_{kn} V_n \right]$$

$$\text{Where } k = [1, 2, \dots, N]$$

from complex power.

$$I_k = \frac{P_k - jQ_k}{V_k}$$

$$\text{Also } I_k = \sum_{n=1}^N Y_{kn} V_n \text{ or}$$

$$I_k = Y_{k1} V_1 + Y_{k2} V_2 + Y_{kN} V_k + Y_{kn} - V_n$$

From the above eqn:

$$V_k = \frac{1}{Y_{kk}} \left[ I_k - \left( \sum_{n=1}^{k-1} Y_{kn} V_n + \sum_{n=k+1}^N Y_{kn} V_n \right) \right]$$

OR

$$V_k = \frac{1}{Y_{kk}} \left[ \frac{P_k - j\omega k}{V_k} - \left( \sum_{n=1}^{k-1} Y_{kn} V_n + \sum_{n=k+1}^N Y_{kn} V_n \right) \right]$$

Where  $k = [1, 2, \dots, N]$

P. T. O

④ Flow chart of Gauss-Seidel.

