

Name: Ayub Khan
ID # : 7881
SEC: B
DEPT: BE CIVIL
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Instr: Engr: Fawad
Khan
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Q no 10Given data

$$\text{Clear span} = 15 \text{ ft.}$$

Step-1Minimum thickness

$$t_{\min} = \frac{L}{28} \times 12$$

$$\Rightarrow \frac{15}{28} \times 12 = 6.428.$$

$$\text{Factored} = 0.4 + \frac{40}{100} = \boxed{0.8}$$

$$\text{Actual } t_{\min} = 6.428 \times 0.8$$

$$= 5.1424.$$

Step-2

Effective depth.

$$D = t - \text{clear cover} - \frac{1}{2} (d \text{ main bar})$$

$$= 5.5 \times 0.25 - \frac{1}{2} (4/8)$$

$$d = 4.5''$$

Step-3:

Self weight of load of slab:

$$= \frac{t}{12} \times \gamma_{\text{concrete}} \times \text{Area}$$

$$= \frac{5.5}{12} \times 150$$

$$= 68.75.$$

Step-4:

Total factor load

$$W_u = 1.2 (D.L.) + L.L.$$

$$= 1.2 (68.75) + 150.$$

$$= \underline{242.5} \text{ or } \underline{0.242 \text{ ksi}}$$

Step-5:

Ultimate moment:

$$M_u = \frac{W_u \times l^2}{8} = \frac{0.242 \times (1.5)^2}{8}$$

$$= 7.48 \times 12$$

$$29.778 \text{ k''}$$

Step-6:

Area of Steel for main bar by trial method.

Trial 01:

$$\text{Let } a = 0.2 \times \tau = 0.2 \times 5.5 = 1.1$$

$$A_s = \frac{M_u}{\phi \times f_y \times (d - \frac{a}{2})} = \frac{29.735}{0.90 \times 40 \left(4.5 - \frac{1.1}{2}\right)} = 0.631$$

Trial 02:

$$a = \frac{A_s \times f_y}{0.85 \times f'_c \times b} = \frac{0.631 \times 40}{0.25 \times 40 \times 12}$$

$$a = 0.618$$

$$A_s = \frac{29.725}{0.90 \times 40 \left(4.5 - \frac{0.61}{2}\right)} = 0.594$$

Trial 03

$$a = \frac{0.524 \times 40}{0.23 \times 4 \times 12} = 0.582$$

$$As = \frac{29.735}{0.90 \times 40 \times \left(4.5 - \frac{0.581}{2}\right)}$$

$\boxed{= 0.582}$

As 29.735

$$0.90 \times 40 \times \left(4.5 - \frac{0.582}{2}\right) = \boxed{0.599}$$

Trial 04

$$a = \frac{0.549 \times 40}{0.25 \times 4 \times 17} = 0.587$$

As = 29.735

$$0.90 \times 40 \times \left(4.5 - \frac{0.587}{2}\right) = \boxed{0.592}$$

$$\text{Trail OS} = \frac{0.592 \times 40}{0.25 \times 12} = \boxed{0.586}$$

$$AS = \frac{29.735}{0.90 \times 40 \times \left(4.5 \frac{0.580}{2}\right)} = 0.592$$

Step-7 Area of steel for distribution.

$$A_{s_{\min}} = 0.0018 \times b \times l$$

$$0.002 \times 12 \times 5.5 = 0.132 \text{ in}^2/\text{ft.}$$

Step-8 Spacing for main bars.

$$S = \frac{A_{\phi}}{A_s} \times 12 = \frac{0.2 \times 12}{0.392} = 4.05 \text{ c/c.}$$

Q. 6

Step-4: Spacing for distribution bars
4 bar.

$$S = \frac{A_b}{A_s} \times 12 = \frac{0.2}{0.132} \times 12 = 18.18 \approx 18 \text{ c/c.}$$

Step-10: Final Summary

$$f_c = 40 \text{ ksi, } f_y = 48 \text{ ksi}$$

$$C = 5.5''$$

main Steel # 4 at 4.5 c/c.

Dise Steel # 4 at 5 c/c.

Q no 2:

Given

$$\text{Width} = 16''$$

$$d_c = 22''$$

$$\text{Factored load} = 9.4 \text{ k/ft}$$

~~Q no~~

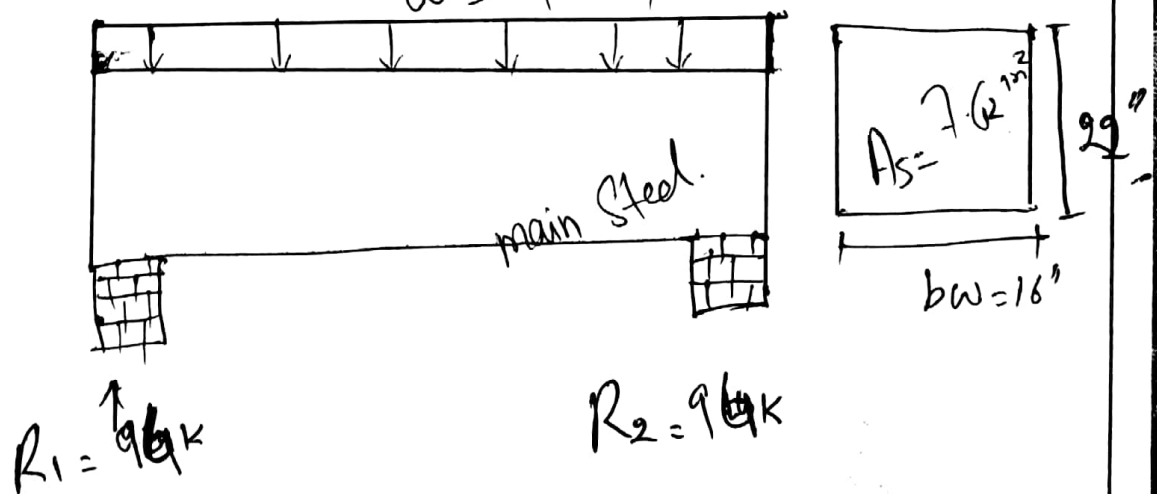
$$\text{Clear span} = 20'$$

$$\text{Tensile Steel Area} = 7.62 \text{ in}^2$$

Find self weigh

$$b \times \gamma_c = \frac{16}{12} \times 150 = 0.2 \text{ k/ft}$$

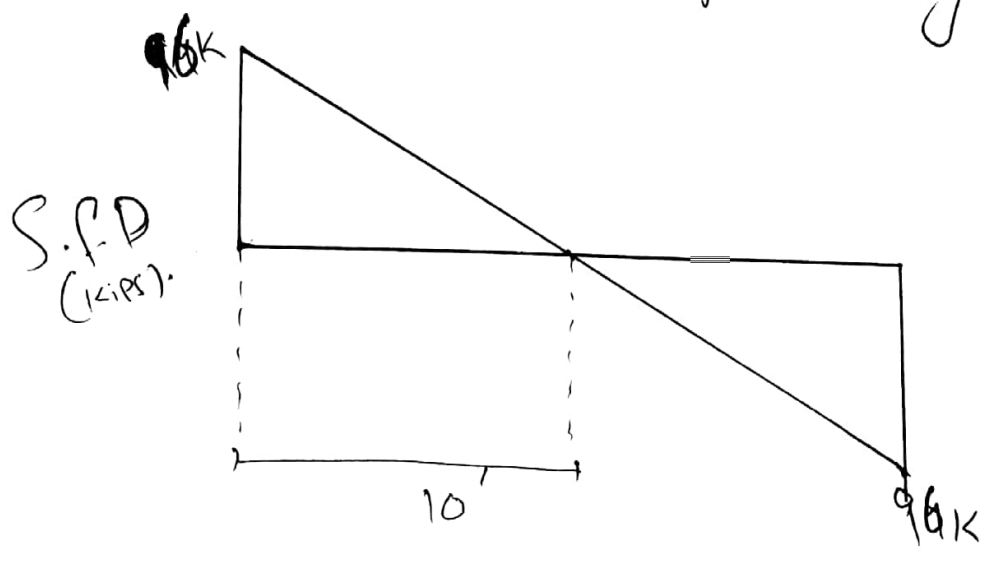
$$w = 9.6 \text{ k/ft}$$



Step-1 Find the value of R_1 & R_2 .

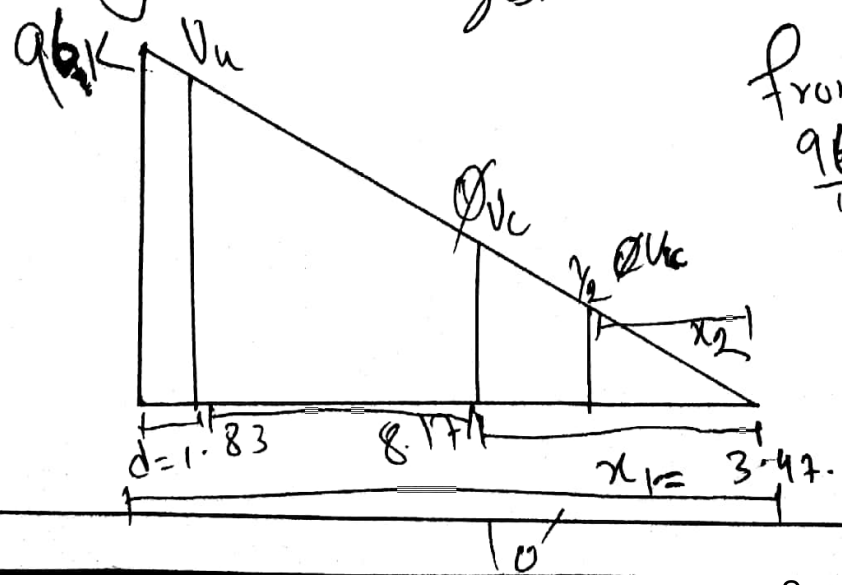
$$\text{Total load} = 9.6 \times 20 = 192 / 2 = 96$$

Step-2: Draw its Shear force diagram.



Step-3: Find the value of critical shear " V_u " and its location, As we know that, critical section is located at the distance " d " from face of support, $d = 22" = 1.83'$.

Value of Critical Shear at distance " d " by Similarity of triangles.



From Similar Δ s

$$\frac{96}{10} = \frac{V_u}{8.17}$$

$$V_u = 78.49 \text{ kips}$$

Step-4: Find the value of " ϕV_c " and $\frac{1}{2}\phi V_c$
 And also its distance from zero
 Shear to right side.

$$\phi V_c = \phi \times 2 \times \sqrt{f_c} \times b_w \times d.$$

$$= \frac{0.75 \times 2 \times \sqrt{4000} \times 16 \times 22}{1000} = 33.40 \text{ k}$$

Location of ϕV_c by similarities of Δ 's

$$\frac{96}{10} = \frac{33.40}{x_1} \Rightarrow x_1 = \frac{3.47}{\cancel{10}} \quad \cancel{10}$$

Now

$$\frac{1}{2} \phi V_c = \frac{33.40}{2} = 16.70 \text{ k.}$$

Location of $\frac{1}{2} \phi V_c \Rightarrow \frac{96}{10} = \frac{16.70}{x_2} \Rightarrow x_2 = \frac{\cancel{10}}{1.73}$

Step-5:

Value of ϕV_s . ($V_u = \phi V_s + \phi V_c$)

So,

$$\phi V_s = V_u - \phi V_c = 78.40 - 33.40 = 45.00 \text{ k.}$$

Step-6: Check on Section adequacy

$$\phi V_g + \sqrt{f'_c} * bw * d = \frac{0.75 * 8 * \sqrt{4000} * 16 * 22}{1000}$$

$$= 133.57 \text{ k.}$$

As, $\phi V_g < \phi \sqrt{f'_c} bw d \Rightarrow$ gt mean Section is adequate.

Step-07: Check on maximum Spacing for Stirrups

$$\phi * 4 * \sqrt{f'_c} * bw * d$$

$$= \frac{0.75 * 4 * \sqrt{4000} * 22 * 16}{1000} = 66.79 \text{ kip.}$$

As, $\phi 4 \sqrt{f'_c} * bw * d > \phi V_s = 43.40 \text{ k.}$

So, Max-Spacing will be Selected from following Four Conditions.

1 - $S_{max} = 24''$,

3 - $S_{max} = \frac{A_v * f_y}{0.75 * \sqrt{f'_c} * bw}$

2 - $\frac{d}{2} = \frac{22}{2} = 11$,

4 - $S_{max} = \frac{A_v * f_y}{50 * bw} = 16.50$.

From above four Condition, least value of spacing for #3, 2 legged stirrups will be selected.

So,

$$S_{max} = 11'' \text{ c/c.}$$

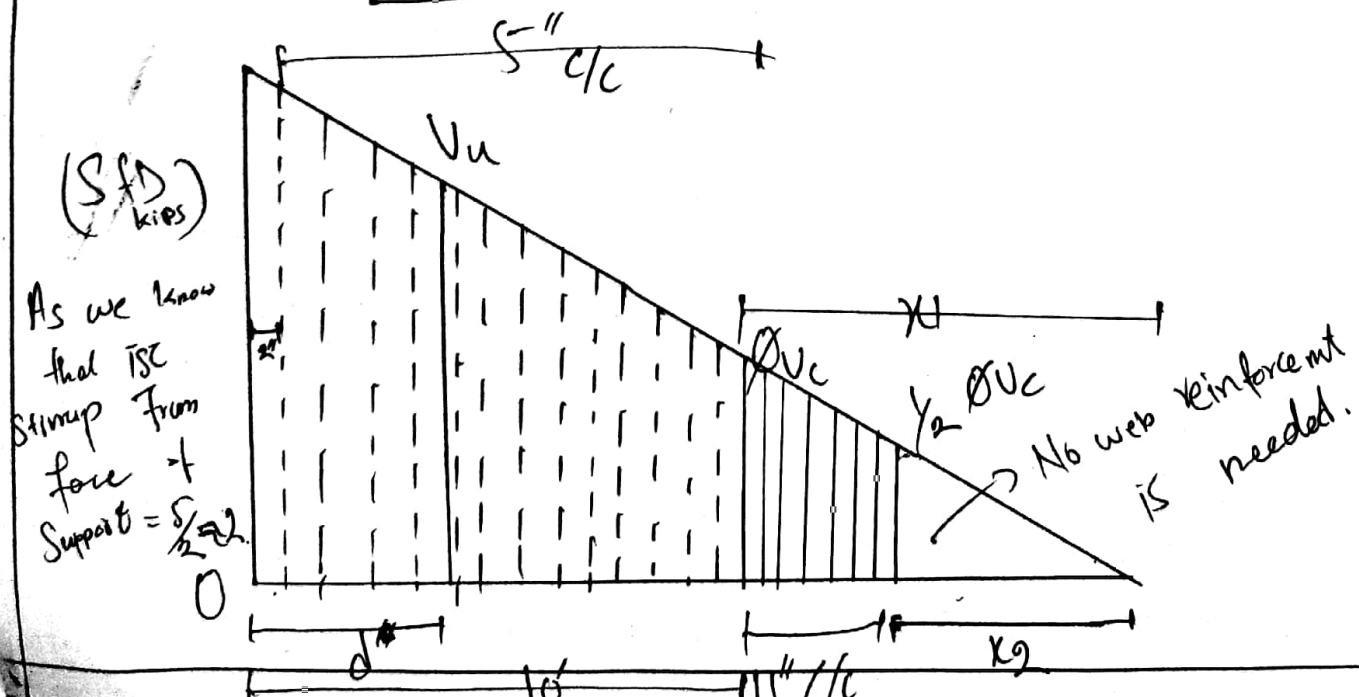
Step-8:

Spacing of stirrups from critical section.

$$S = \frac{\phi \times A_v \times f_y \times d}{V_u - \phi V_c} = \frac{0.75 \times 0.22 \times 60 \times 22}{78.42 - 33.44}$$

$$S = 4.84 \approx S = 5'' \text{ c/s}$$

Step-9: Sketch the final sketch



As we know that ISC stirrup from face of support = $\frac{S}{2} = 2.5$

Question # 03.

→ Calculate the axial ultimate load carrying capacity of a 12 inch-square tied column reinforced with 4 # 9. Ties are # 3 spaced @ 12 inches. Use $f'_c = 4000$ psi and $f_y = 60$ ksi, Also design necessary spirals.

Solution:

Given:

Step-1: Find gross area of concrete.

$A_g = b \times b$ (Since it is square tied column.)

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual).}$$

Step-2: Find the area of steel.

Since $A_s = 5\%$ of A_g .

$$= 0.05 \times 144.$$

$$A_s = 7.2 \text{ in}^2$$

Step-3: ultimate load carrying capacity.

$$P_u = \phi \times 0.80 \times (0.85 \times f'_c \times (A_g - A_s) + A_s \times f_y).$$

$$= 0.65 \times 0.80 [0.85 \times 4 (144 - 7.2) + 7.2 \times 60]$$

$$P_u = 466.50 \text{ k}$$

Step-4: Sketch and design of ties (per to distance).

From the below value we choose the

least value of all, thus;

Q3

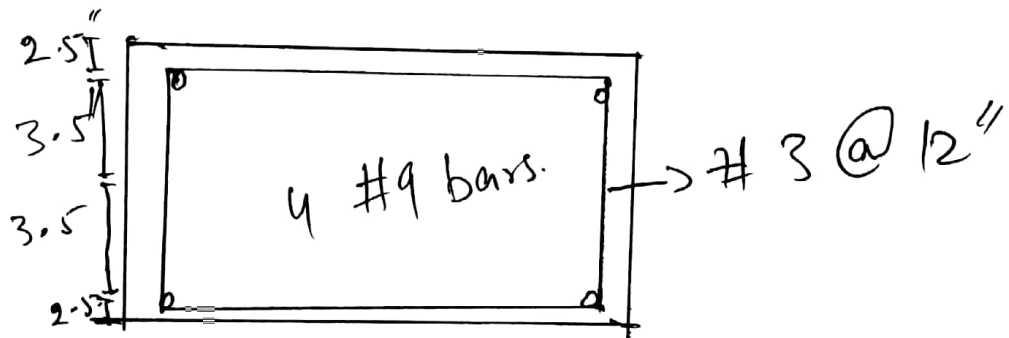
Q3 (3)

(1) 16 x dia of long bar = $16 \times \frac{9}{8}$.

(2) 48 x dia of the bar = $48 \times \text{dia of tie bar} = 48 \times \frac{3}{8}$

(3) = least column dimension = 18"

So c/c distance b/w ties = 12"



● Since it is a tied Square Column So there is no spiral stirrup ~~an~~ used, the stirrup used is of rectangular shape due to the specification of the structure thus we will use tie stirrups instead.

Q4! Design a square footing --- Sketch of your final design.

Step-1: Let $h = 24''$

Step-2: Total weight = wt of Soil + wt of Rc
 $= 3 \times 120 + 2 \times 150$
 $= 660 \text{ psf} = 0.660 \text{ ksf}$

Step-3: Effective beam Capacity

$$q_e = q_a - w$$
$$= 2.50 - 0.660$$

$$q_e = 1.84 \text{ ksf}$$

Step-4: Require Area for foundation.

$$A_{req} = \frac{\text{Service load}}{q_e} = \frac{100 + 120}{1.84}$$

$$119.57 \text{ ft}^2$$

Step-5: Since ~~forward~~ foundation is square (2)

$$A_{req} = b \times b =$$

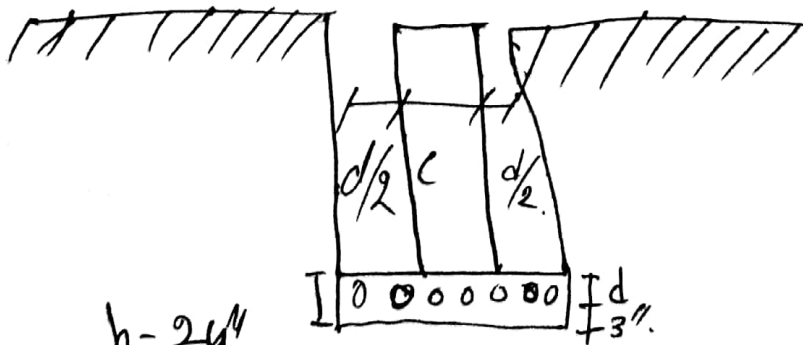
Step-6: upward bearing Capacity.

$$q_{up} = \frac{\text{factored load}}{(B)^2} = \frac{1.2 \times 100 + 1.6 \times 120}{11^2}$$

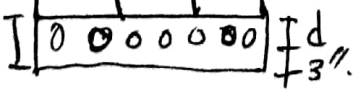
$$q_{up} = 2.58 \text{ k/ft}^2$$

Step-07: Punching Shear.

$$b_o = 4 \times (c + d)$$



$$h = 24''$$



$$d = h - c - \text{dia of bar} - \frac{1}{2} d_b$$

$$= 24 - 3 - 1 - \frac{1}{2} (1) = 19.5''$$

$$b_o = 4 \times (16 + 19.5) = 142''$$

∴ take #8 bar

dia = 8/8 = 1''

Step-8.

$$V_u = q_{up} \times \left[B^2 - (cxd)^2 \right]$$

$$= 2.58 \times \left[11^2 - \frac{(16 + 19.5)}{1.2} \right]$$

$$V_u = 289.60 \text{ k.}$$

Step-9

$$\textcircled{1} V_{up} = \frac{\phi \times 4 \times \sqrt{f'c} \times b \times d.}{1000}$$

$$= \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5}{1000}$$

$$\Rightarrow 525.38 \text{ k.}$$

Step-10.

Beam Shear / one way Shear Check.

$$V_u = q_{up} \times B \times \left[\frac{B}{2} - \frac{c}{2} - d \right]$$

$$V_u = 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{2} - \frac{19.5}{2} \right]$$

$$V_u = 90.95 \text{ k.}$$

(4)

Step-11: Self Shear Capacity.

$$\phi_{vc} = \phi \times 2 \times \sqrt{f_c} \times b \times d.$$

$$\Rightarrow \frac{0.75 \times 2 \times \sqrt{4000} \times (11 \times 12 - 16)}{1000}.$$

$$\Rightarrow 110.04 \text{ k} > V_u \Rightarrow \text{OK.}$$

Step-12: ultimate moment

$$M_o = \frac{q_{up} \times B}{8} \times (B - C)^2 = \frac{2.58 \times 11}{8} \times \left(11 - \frac{16}{12}\right)^2$$

$$M_w = 331.49 \text{ k}' = 3977.93 \text{ k}''.$$

Step-13: Area of steel for members
by trial and Repeat method.

Trial 1

(5)

$$\text{Let } a = 0.2 \times h = 0.2 \times 24 = 4.8''$$

$$A_s = \frac{M_u}{\phi \times f_y \times \left(d - \frac{a}{2}\right)} = \frac{3977.93}{0.9 \times 60 \times \left(11 - \frac{4.8}{2}\right)}$$
$$= 8.56 \text{ in}^2.$$

Trial 2:

$$a = \frac{A_s \times f_y}{0.85 \times f_c \times b} = \frac{8.56 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.53''$$

$$A_s = \frac{3977.93}{0.9 \times 60 \times \left(11 - \frac{1.53}{2}\right)} = 7.197 \text{ in}^2.$$

Trial 3:

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$A_s = \frac{3977.93}{0.9 \times 60 \times \left(11 - \frac{1.28}{2}\right)} = 7.1 \text{ in}^2.$$

So thus area = 7.1 in².

Step-14 : Check the min reinforcement by the following method.

$$A_{s_{min}} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24.$$

$$A_{s_{min}} = 8.70 \text{ in}^2.$$

$$A_{s_{min}} = \frac{20}{f_y} \times B \times d = \frac{200}{60000} \times (11 \times 12) \times 19.5.$$

$$A_{s_{min}} = \frac{3 \times \sqrt{f_c}}{f_y} \times B \times d = \frac{3 \times \sqrt{3000}}{60000} \times (11 \times 12) \times 19.5.$$

$$A_{s_{min}} = 7.05 \text{ in}^2$$

From above value greater value will be selected thus $A_{s_{min}} = 8.58 \text{ in}^2.$

Step-15: Using # 8 bar

$$A_b = 0.785 \text{ in}^2$$

$$\text{No. of bars} = \frac{A_s}{A_b} = \frac{8.58}{0.785} = 10.92$$

≈ 11 bars in each direction.