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Department: Civil Engineering

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Assignment # 01

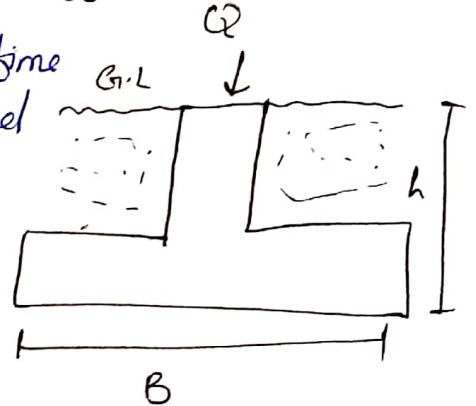
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Q 1

Part A:

1. Ultimate bearing capacity:

It is the maximum gross pressure at the base of footing with no shear failure in soil is called ultimate bearing capacity it is denoted by q_u



2. Angular distortion:

When the wall and edum are supported by two footing then the unequal settlement in this case is called Angular distortion

3. Plastic Equilibrium:

The transition from the state of plastic equilibrium to the state of plastic flow represents the failure of the mass. Since the weight of the mass assists in producing an expansion in a horizontal direction, the subsequent failure is called active failure.

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4. Compression index:
~~2x2x2x2~~

The Compression index is used to find the settlement in the normally consolidated clay. The total stress applied is larger than the stress in the field, to which the soil sample has been undergone in the past.

This kind of clayey soil is said to be normally consolidated clay.

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Q 1:-

Part B

Problem:

A 6 meter tall cantilever that has the following properties $c=0$, $\phi'=30^\circ$, $\gamma=19.2 \text{ KN/m}^3$ in the ground surface behind the wall is inclined at a slope 3 horizontal and 1 vertical. The wall has moved sufficiently to develop active condition. Determine the total normal and shear forces acting on the back of this wall using Rankine theory

Solution:

$$c=0$$

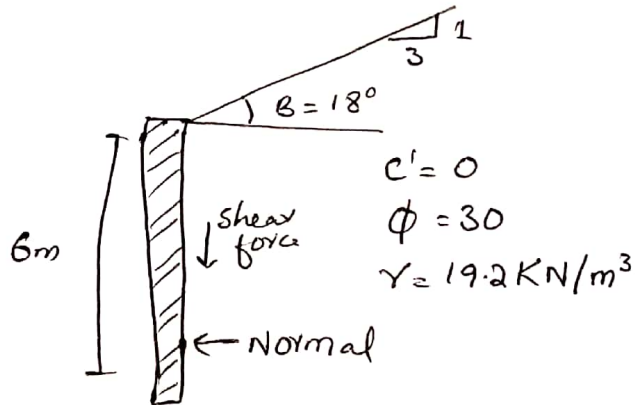
$$H=6\text{m}$$

$$\phi=30^\circ$$

$$\gamma=19.2 \text{ KN/m}^3$$

Slope

$$(H=3, V=1)$$



Required:

$$\text{Normal force} = ? \quad \frac{N_a}{b} = \frac{P_a}{b} \cos \beta$$

$$\text{Shear force} = ? \quad \frac{V_a}{b} = \frac{P_a}{b} \sin \beta$$

$$\therefore \beta = \tan^{-1} \left(\frac{1}{3} \right)$$

$$\beta = 18^\circ$$

$$\frac{N_a}{b} = \frac{\gamma H^2 K_a \cos \beta}{2}$$

where
$$K_a = \frac{\cos \beta (\cos \beta - \sqrt{\cos^2 \beta - \cos^2 \phi'})}{\cos \beta + \sqrt{\cos^2 \beta - \cos^2 \phi'}}$$

$$K_a = \frac{\cos(18^\circ) (\cos(18^\circ) - \sqrt{\cos^2(18^\circ) - \cos^2(30^\circ)})}{\cos(18^\circ) + \sqrt{\cos^2(18^\circ) - \cos^2(30^\circ)}}$$

$K_a = 0.395$

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$$\frac{N_a}{b} = \frac{\gamma H^2 K_a \cos \beta}{2}$$
$$= \frac{19.2 (6)^2 (0.395) \cos(18^\circ)}{2}$$

$$\boxed{\frac{N_a}{b} = 130 \text{ KN/m}^3}$$

$$\frac{V_a}{b} = \frac{\gamma H^2 K_a \sin \beta}{2} \quad \therefore \frac{P_a}{b} = \frac{\gamma H^2 K_a}{2}$$

$$\frac{V_a}{b} = \frac{(19.2)(6)^2(0.395)}{2} \times \sin(18^\circ)$$

$$\boxed{\frac{V_a}{b} = 42 \text{ KN/m}}$$

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Q 2

Part A :-

Bearing Capacity:

In Geotechnical engineering the bearing capacity is defined as the ability of soil to support the applied load is called bearing capacity of soil.

In other words the internal strength of the soil is called bearing capacity.

It is denoted by q .

Factor effecting bearing capacity:

Relative density: More the relative density of the soil more will be its angle friction ϕ

This will be more in case of dense soil as compared with medium and loose sand.

With increase of relative density, N_q & N_r

N_r will increase.

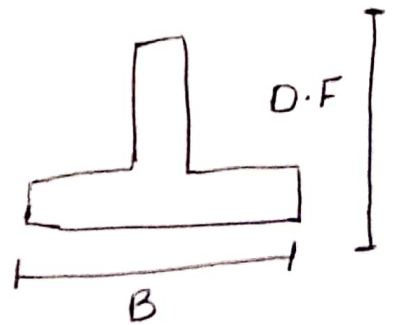
This increase in N_q & N_r will cause increase in the bearing capacity.

N_q & N_r these are Terzaghi's bearing capacity factors.

Depth of footing:

The bearing capacity of soil will increase with increase of depth of the footing.

This increasing will be more in case of dense soil as compared with medium and loose sand.



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unit weight of the soil:

with the increase of unit weight of the soil more than unit weight of the soil will be its bearing capacity. dense soil increase will be more as compared with medium and loose.

Width of the footing:

increase with the increase of width of the footing. More the width more will be the bearing capacity. This will be more in case of dense soil as compared with loose & medium.

Location of water table:

Bearing Capacity decrease as the water table comes near in location with footing.

Q2 Part B:-

Problem:

What is the maximum safe load which can be supported by a rectangular footing 2m by 3m with a safety factor of 3? The base of the footing is of 1.6m below this group surface. The unit weight of soil is 18 KN/m^3 .

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The angle of shearing resistance ϕ is 20° and the unit cohesion c_u is 20 kN/m^2 use the Meyerhof's analysis

Given data:

$$\begin{aligned} \phi &= 20^\circ & D &= 1.6 \text{ m} \\ L &= 3 \text{ m} & \gamma &= 18 \text{ kN/m}^3 \\ B &= 2 \text{ m} & F.O.S &= 3 \\ C &= 20 \text{ kN/m}^2 \end{aligned}$$

From table

$$\phi = 20^\circ \\ (N_c = 14.8, N_q = 2.9, N_\gamma = 6.4)$$

$$\alpha = \left(45 + \frac{\phi}{2}\right)$$

$$\alpha = \left(45 + \frac{20}{2}\right)$$

$$\boxed{\alpha = 55^\circ}$$

$$\begin{aligned} S_c &= 1 + 0.2 \left(\frac{B}{L}\right) \tan^2 \alpha \\ &= 1 + 0.2 \left(\frac{2}{3}\right) \tan^2 (55^\circ) \end{aligned}$$

$$\boxed{S_c = 1.2}$$

$$S_q = S_\gamma = 1 + 0.1 \left(\frac{B}{L}\right) \tan^2 \alpha$$

$$S_q = S_\gamma = 1 + 0.1 \left(\frac{2}{3}\right) \tan^2 (55^\circ)$$

$$\boxed{S_q = S_\gamma = 1.09}$$

$$d_c = 1 + 0.2 \left(\frac{D}{B}\right) \tan \alpha$$

$$d_c = 1 + 0.2 \left(\frac{1.6}{2}\right) \tan (55^\circ)$$

$$\boxed{d_c = 1.2}$$

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$$d_{qv} = d_{rz} \left(1 + 0.1 \left(\frac{D}{B} \right) \tan \alpha \right)$$

$$d_{qv} = d_{rz} \left(1 + 0.1 \left(\frac{1.6}{2} \right) \tan (55^\circ) \right)$$

$$d_{qv} = d_{rz} = 1.1$$

$$q_u = c N_c S_c d_c + q N_v S_q d_{qv} + \frac{1}{2} \gamma_B N_\gamma S_\gamma d_z$$

$$= (20 \times 14.8 \times 1.2 \times 1.272) + (1.6 \times 18 \times 6.4 \times 1.09 \times 1.1) + \frac{1}{2} (18 \times 2 \times 2.9 \times 1.09 \times 1.1)$$

$$q_u = 462 + 234 + 66$$

$$q_u = 762 \text{ KN/m}^2$$

$$q_{n.u} = q_u - \gamma \times D_f \quad \delta'$$

$$= 762 - (18 \times 1.6)$$

$$q_{n.u} = 733.2 \text{ KN/m}^2$$

$$q_{n.s} = \frac{733.2}{3} = 244.4 \text{ KN/m}^2$$

$$q_s = q_{n.s} + \gamma \times D_f$$

$$q_s = 244.4 + 18 \times 1.6$$

$$q_s = 273.2 \text{ KN/m}^2$$

q_s on the hole area of the footing

$$= A \times q_s$$
$$= (2 \times 3) \times (273.2)$$

$$\text{hole area} = 1639 \text{ KN}$$

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Q 3

Part A

Settlement.

When load is applied on the ground surface effective stresses will be produced due to these effective strain will be produced due to as result change in volume will take place and soil particles will move in the downward direction this downward movement is called Settlement.

Types of Settlement

① Total settlement

② Differential settlement

① Total settlement/ uniform settlement,

It is also called uniform settlement in this type of settlement every part of the structure settles equally. In this type of settlement the structure remains in its sound form.

Total settlement take place in structure which is supported by rigid footing.

Due to uniform settlement the utility service of the building can be decrease such as water supply, electricity, sewage service, telephone etc.

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Limitation of total settlement:

- ① To transfer the load of the structure to the soil which have enough bearing capacity
- ② To distribute the load over a large area.

② Differential settlements

is the same structure is called differential settlement. It is more undesirable as compared to total settlement because it is more dangerous than total settlement.

Q 3

Part B

A soil has compressive index $C_c = 0.31$ At a stress 130 KN/m^2 , the void ratio was 1.02 Calculate

1. The void ratio if the stress on the soil is increased to 170 KN/m^2
2. the total settlement of the stratum of 5 m thickness.

Given data:

$C_c = 0.28$

$e_1 = 1.02$

$P_1 = 130 \text{ KN/m}^2$

$P_2 = 170 \text{ KN/m}^2$

$H = 6 \text{ m}$

Required: $e_2 = ?$ $S_c = ?$

Solution:

$$C_c = \frac{e_2 - e_1}{\log \frac{P_2}{P_1}}$$

$$\Rightarrow 0.28 = \frac{e_2 - 1.02}{\log \left(\frac{170}{130} \right)}$$

$$\Rightarrow 0.28 = \frac{e_2 - 1.02}{0.1165}$$

$$\Rightarrow 0.28 \times 0.1165 = e_2 - 1.02$$

$$\Rightarrow 0.03262 + 1.02 = e_2$$

$$\Rightarrow \boxed{e_2 = 1.05}$$

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$$\textcircled{b} \quad s_c = \frac{H}{1+e_1} \times C_c \log \left(\frac{P_2}{P_1} \right)$$

$$= \left(\frac{5}{1+1.02} \right) \times 0.28 \times \log \left(\frac{170}{130} \right)$$

$$= 0.080 \text{ m}$$

$$s_c = 80 \text{ mm}$$