

ID: 7379

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Subject: PRCD - I

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FINAL TERM.

Q1: A reinforced concrete slab is built integrally with its support and consists - - - - -

Draw sketch of your final design.

Given Data:

⇒ 3 equal spans concrete slab.

⇒ Clear span b/w supports = 15 ft.

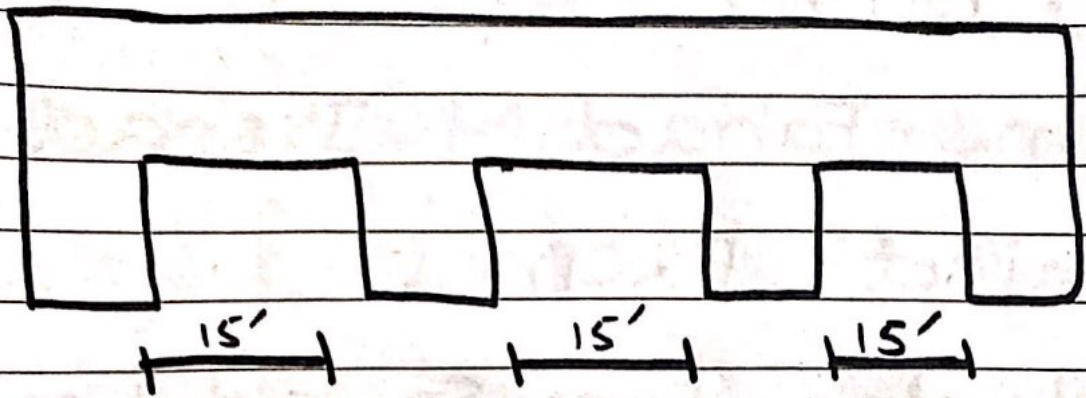
⇒ factored live load = 160 lb/ft^2

⇒ service floor finish load = 20 lb/ft^2

⇒ $f'_c = 4000 \text{ psi}$

⇒ $f_y = 40 \text{ ksi}$

Solution:.



STEP #1 (Minimum Thickness)

By using formula

$$t_{\min} = \frac{L}{28} = \frac{15'}{28} = 6.4 \approx 6.5''$$

As $f_y \rightarrow 40 \text{ ksi}$

So we will multiply a factor with this thickness.

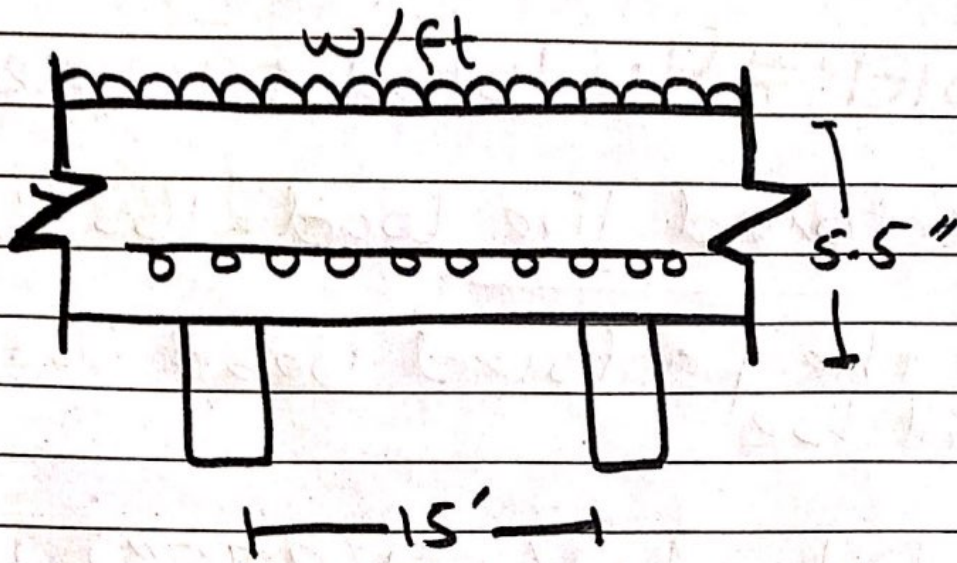
$$\text{factor} = \left(0.4 + \frac{f_y}{100} \right)$$

$$= \left(0.4 + \frac{40}{100} \right) = 0.8$$

Hence the minimum thickness will be 6.5×0.8 .

$$t_{\min} = 5.2 \approx 5.5''$$

STEP # 2: (Effective Depth)



By formula

$$d = t - \text{clear cover} - \frac{1}{2} (\text{dia of}$$

main bars)

$$= 5.5 - 0.75 - \frac{1}{2} \left(\frac{5}{8} \right)$$

$$d \cong 4.5''$$

STEP # 3 (Self wt. of slab)

By formula

$$\frac{t}{12} + \gamma_{\text{concrete}}$$

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$$= \frac{5.5 \times 150}{12} = 68.75 \text{ Lb/ft}^2$$

STEP #4: (Total Factored load)

factored live load = 160 Lb/ft²

So the factored Dead load will be

$$D.L = 1.2(20 + 68.75) = 106.5 \text{ Lb/ft}^2$$

Total factored load = D.L + L.L

$$= 106.5 + 160$$

$$= 266.5 \text{ Lb/ft}^2$$

$$= 0.2665 \text{ K/ft}^2$$

STEP #5: (Ultimate Moment)

By using formula

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (15)^2 \times 12}{8}$$

$$= 89.94 \text{ Kip-inches}$$

STEP #6: Area of steel for main Bar By Trial and Repeat Method.

Trial #1:

Let depth of compression block

$$a = 0.2 \times t \\ = 0.2 \times 5.5 = 1.1''$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 -$$

$$A_{st} = 0.63 \text{ in}^2$$

Trial #2:

$$a = \frac{A_{st} \times f_y}{0.85 \times f'_c \times b} = \frac{0.63 \times 40}{0.85 \times 4 \times 12}$$

$$= 0.62 \text{ in}^2$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - 0.6/2)}$$

$$A_{st} = 0.59 \text{ in}^2$$

Trial # 3:

$$a = \frac{0.59 \times 40}{0.85 \times 4 \times 12} = 0.57''$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times (4.5 - 0.57)} = 0.59 \text{ in}^2$$

So we will be $A_{st} = 0.59 \text{ in}^2$

STEP # 7: Area of steel for distribution reinforcement

$$A_{min} = 0.002 \times b \times \ell \rightarrow$$

(For Grade 40 steel)

$$= 0.002 \times 12 \times 5.5$$

$$= 0.132 \text{ in}^2$$

STEP: 8: Spacing for main bar

By formula

$$\text{Spacing} = \frac{A_b \times 12}{A_{st}}$$

We use # 6 bar dia = $\left(\frac{6}{8}\right)^4$

$$\text{Area} = \frac{\pi}{4} \left(\frac{6}{8}\right)^2 = 0.442 \text{ in}^2$$

STEP #9: Spacing for distribution bars.

$$\text{Spacing} = \frac{A_b}{A_{st}}$$

We use #5 bars so

$$\text{dia} = \left(\frac{5}{8}\right)'' , \text{Area} = \frac{\pi}{4} \left(\frac{5}{8}\right)^2 = 0.31 \text{ in}^2$$

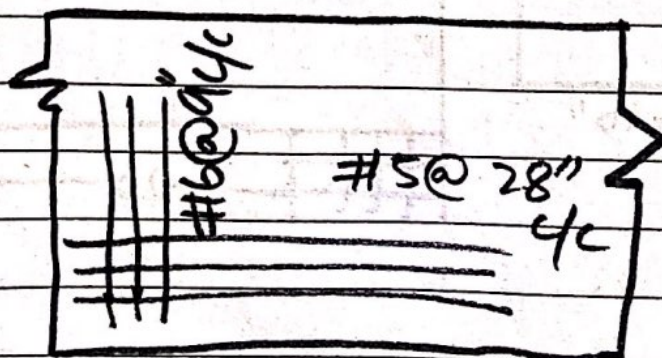
$$\text{spacing} = \frac{0.31 \times 12}{0.132} = 28.1'' \approx 28$$

STEP #10: Find Sketch.

$$f_c' = 4 \text{ ksi} , f_y = 40 \text{ ksi}$$

main steel #6 at 9" c/c

Distribution steel #5 at 28" c/c



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A simply supported rectangular beam 16" wide
Draw a sketch of your final diagram.

Solution:

First of all find the unit load of beam

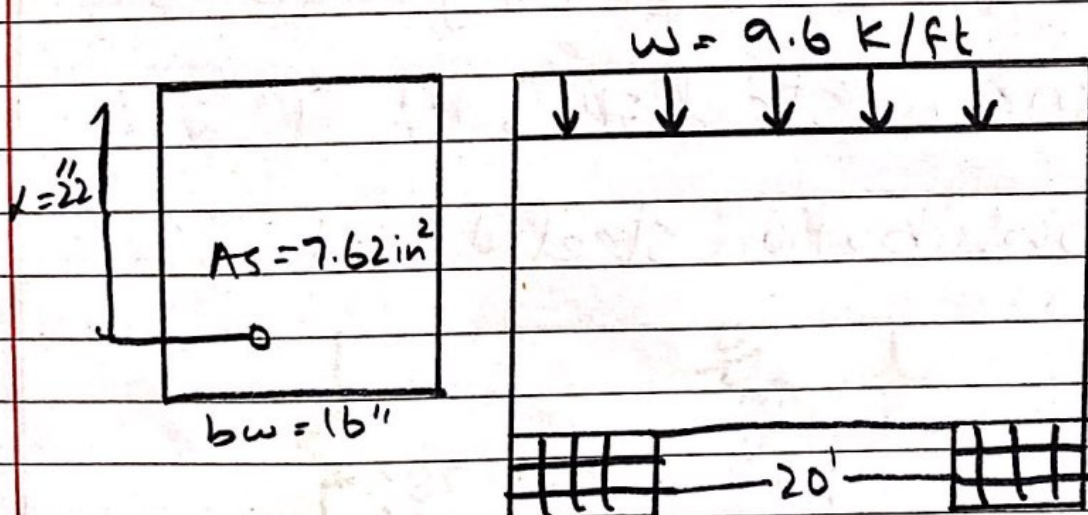
$$so \quad b \times h$$

$$= \frac{16}{12} \times 150 \Rightarrow 200 \text{ lb/ft} =$$

$$0.2 \text{ K/ft}$$

So total factored load = $9.4 + 0.2$

$$= 9.6 \text{ K/ft}$$



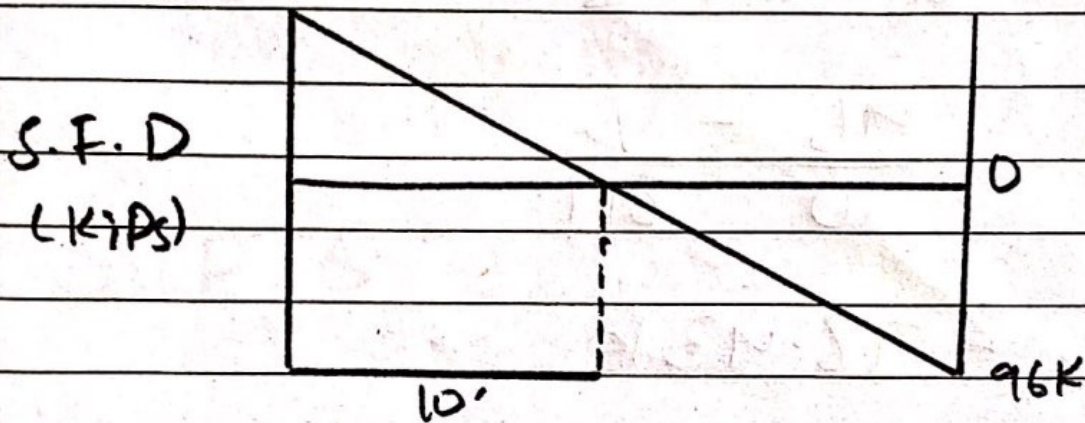
STEP #1

find the value of R_1 & R_2

$$\text{Total load} = 9.6 \times \frac{20}{2} = 96 \text{ k.}$$

STEP #2

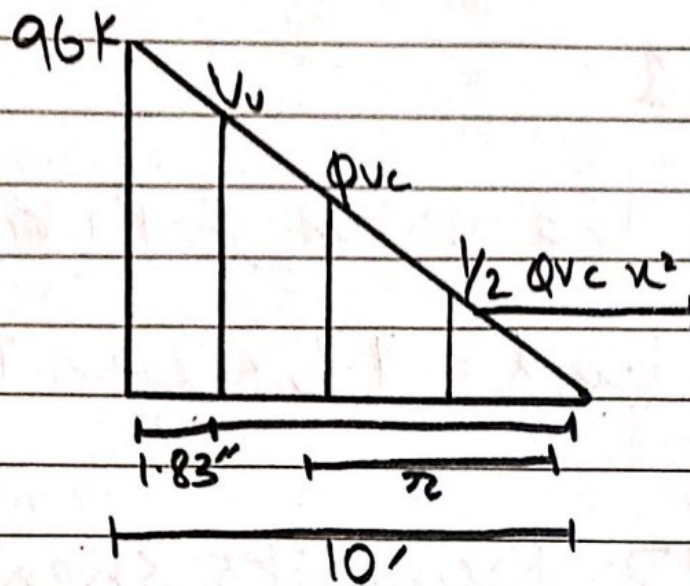
Draw its shear force diagram.



STEP #3:

find the value of critical stress " v_u " and its location.

As we know that critical reaction is located at distance " d " from face of support $\alpha = 22" = 1.83$ value of critical shear at distance " d " by similarity of triangles.



from similar Δ 's

$$\frac{96}{10} = \frac{V_u}{8.17}$$

$$V_u = 78.43k$$

STEP: 4: Find the value of ϕ_{vc} $\left\{ \frac{1}{2} \phi_{vc} \right\}$ Also its distance from zero shear of right side.

$$\phi_{vc} = (\phi \times 2 \times \sqrt{f_c' \times b_w \times d}) \Rightarrow$$

$$0.75 \times 2 \times \frac{\sqrt{4000 \times 16 \times 2}}{1000}$$

$$\phi_{vc} = 33.40k$$

Location of ϕ_{vc} by similarity of Δ 's

$$\frac{96}{10} = \frac{33.40}{n_1}$$

$$n_1 = 3.48'$$

$$\text{Now } \frac{1}{2} \phi_{vc} = \frac{33.40}{2} = 16.70 \text{ k}$$

$$\text{Location of } \frac{1}{2} \phi_{vc} \Rightarrow \frac{96}{10} = \frac{16.70}{n_2}$$

$$n_2 = 1.74'$$

STEP: 5: Value of ϕ_{vs} ($v_u = \phi_{vs} + \phi_{vc}$)

$$\text{So } \phi_{vs} = v_u - \phi_{vc}$$

$$\phi_{vs} = 78.43 - 33.40$$

$$\phi_{vs} = 45.03 \text{ k}$$

STEP: 6: Check on section
Adequacy.

$$\Rightarrow \phi \times 8 \times \sqrt{f'_c} \times b_w \times d =$$

$$\frac{0.75 \times 8 \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$= 133.57k$$

As $\phi \times 8 \sqrt{f_c} \times b \times d > \phi V_s \rightarrow$

It means section is adequate.

STEP: 7: check on min spacing for stirrups.

$$\phi \times 4 \times \sqrt{f_c} \times b \times d =$$

$$\frac{0.75 \times \sqrt{4000} \times 16 \times 22}{1000} = 66.79k$$

$$\text{As } \phi 4 \sqrt{f_c} \times b \times d > \phi V_s = 45.03k$$

Thus max spacing will be selected from the following four condition.

1) $s_{max} = 24"$

2) $\frac{2}{2} = \frac{22}{2} = 11"$

3) $s_{max} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c} \times b}$

$$A_v = \frac{\pi}{4} \left(\frac{3}{8} \right)^2 = 0.22 \times 60000 \quad A_v = 0.11 \times 2$$

$$0.75 \times \sqrt{4000} \times 16 \quad A_v = 0.22$$

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$$4) \rho = \frac{A_u \times f_y}{50 \times b_w}$$

$$= \frac{0.22 \times 60000}{50 \times 16}$$

$$= 1.650$$

From the above four conditions, least value of spacing from #3, v shaped will be selected

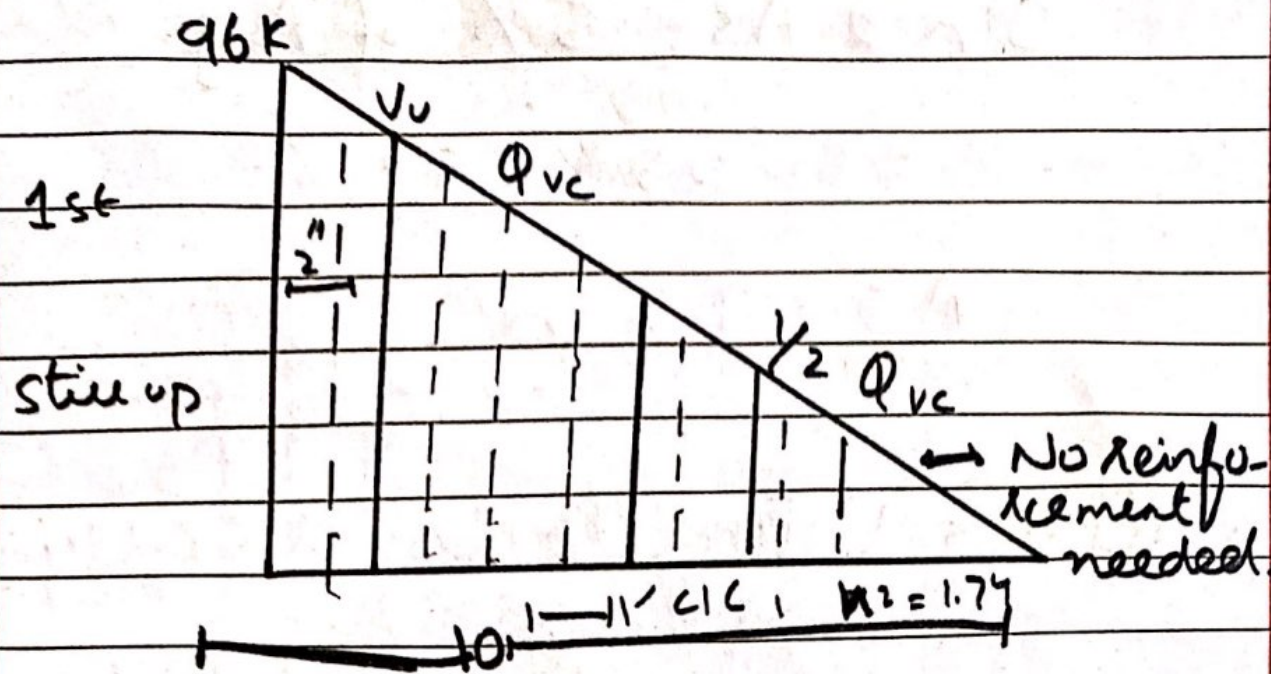
$$s_o \quad s_{max} = 1.1" c/c$$

STEP # 8: Spacing of stirr UP from / at critical section.

$$s = \frac{\phi \times A_u \times f_y \times d}{V_u - \phi V_c} = \frac{\phi \times A_u \times f_y \times d}{V_u - \phi V_c}$$

$$= \frac{0.75 \times 0.22 \times 60 \times 22}{78.43 - 33.46}$$

STEP # 9: Find sketch. $= 48.4" \approx 5" c/c$



As we know that first stirrup from face of support.

$$\Rightarrow \frac{s}{2} = 2.5 \approx 2''$$

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Q3: Calculate the axial ultimate design necessary spins.

STEP: 1. Find gross area of concrete.

$A_g = b \times b$ (since it is square tied column)

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

STEP: 2 Find the area of steel

$$\text{Since } A_s = 5\% \text{ of } A_g$$

$$= 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

STEP: 3 Ultimate load carrying capacity.

$$P_u = \phi \times 0.80 \times [0.85 \times f'_c \times (A_g - A_s) + A_s \times f_y]$$

$$= 0.65 \times 0.80 [0.85 \times 4 (144 - 7.2) + 7.2 \times 60]$$

$$P_u = 466.50 \text{ k}$$

STEP: 4 Sketch & design of Ties

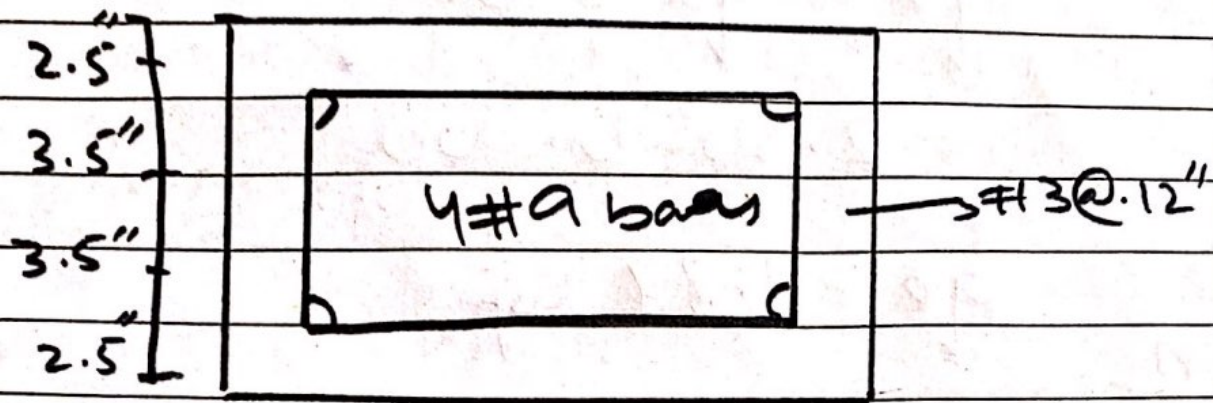
From the below value we choose the least value of all these

1) $16 \times \text{dia of long bar} = 16 \times \frac{9}{8} = 18''$

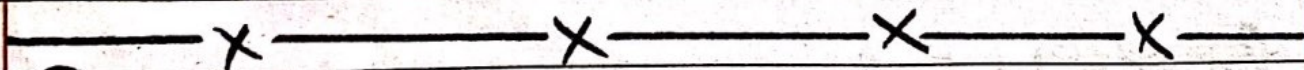
2) $48 \times \text{dia of Tie bar} = 48 \times \frac{3}{8} = 18''$

3) least column dimension = 12"

so c/c distance b/w ties = 12"



Since it is a tied square column so there is no spiral stirrup used, the stirrup used is of rectangular shape due to the specification of the structure thus we will use the stirrup instead.



Q4:

Design a square footing
 ----- sketch of your final design.

STEP: 1.

Let $h = 24"$

STEP: 2. Effective bearing capacity

$$q_e = q_a - w$$
$$= 2.50 - 0.660$$

$$q_e = 1.84 \text{ Ksf}$$

STEP: 3 Required Area for foundation.

$$\text{Area} = \frac{\text{Service load}}{q_e} = \frac{100 + 120}{1.84}$$
$$= 119.57 \text{ ft}^2$$

STEP: 4 Since foundation is square.

$$\text{Area} = b + b = 119.57 \Rightarrow B \approx 11'$$

STEP: 5 Upward bearing capacity of soil.

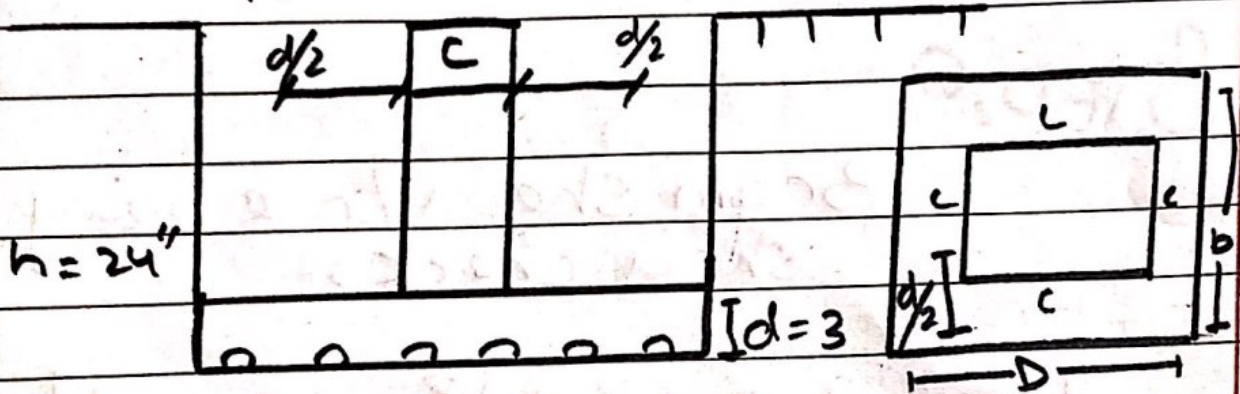
$$q_{up} = \frac{\text{factored load}}{(B)^2}$$

$$= \frac{1.2 \times 100 + 1.6 \times 120}{112}$$

$$q_{up} = 2.58 \text{ k/ft}^2$$

STEP: 6 Punching shear

$$b_o = 4 \times (c + d)$$



$$d = h - c - \frac{c - \text{dia of bar}}{2} \quad \text{db}$$

\therefore Take #8
bar dia =

$$= 24 - 3 - \frac{1}{2}(1) = 19.5'' \quad \frac{8''}{8} = 1''$$

$$b_o = 4 \times (16 + 9.5) = 142''$$

STEP: 7

$$V_{u2} = q_{up} \times \left[B^2 - \frac{(c+d)^2}{2} \right]$$

$$= 2.58 \times \left[11^2 - \frac{(16+19.5)^2}{2} \right]$$

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$$V_{u2} = 289.60 \text{ k}$$

STEP: 8

$$\phi V_{up} = \phi \times 4 \times \sqrt{f_c} \times b \times d$$

$$= \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5}{1000}$$

$$\phi_{up} = 525.38 \text{ k}$$

STEP: 9

Beam shear / one way shear check :-

$$V_{u1} = q_{up} \times B \times \left[\frac{B}{2} - \frac{c}{2} - d \right]$$

$$V_{u1} = 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{2} - \frac{19.5}{2} \right]$$

$$V_{u1} = 90.95 \text{ k}$$

"Self shear capacity".

$$\phi_{vc} = \phi \times 2 \times \sqrt{f_c} \times b \times d$$

$$= \frac{0.75 \times 2 \times \sqrt{4000} \times (11 \times 12 - 16)}{1000}$$

$$= 110.04k > v_{u1} \Rightarrow O.K$$

STEP: 12 - Ultimate moment

$$m_u = \frac{q_{up} \times B \times (B - c)^2}{8} = \frac{2.58 \times 11}{8}$$

$$m_w = 331.49k' = 3977.93k''$$

STEP: 12

Area of steel for main bars by trial & Repeat method.

trial # 1

$$\text{let } a = 0.2 \times h = 0.2 \times 24 = 48''$$

$$A_s = m_u = 3977.93$$

$$\phi \times f_y \times \left(\frac{d - a}{2} \right) = 0.9 \times 60 \times \left(\frac{11 - 4.8}{2} \right)$$

$$A_s = 8.56 \text{ in}^2$$

trial #2

$$a = \frac{A_s \times f_y}{0.85 \times f_c \times b} = \frac{8.56 \times 60}{0.85 \times 3 \times 11 \times 12}$$
$$= 1.53''$$

$$A_s = \frac{3977.93}{0.90 \times 60 \times \frac{(11 - 1.53)}{2}} = 7.197 \text{ in}^2$$

trial #3

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$A_s = \frac{3977.93}{0.90 \times 60 \times \frac{(11 - 1.28)}{2}} = 7.1 \text{ in}^2$$

So, thus (area) = 7.1 in²

Step # 14.

Check the min reinforcement by the following as method,

$$A_{s \min} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24$$

$$A_{s \min} = 5.70 \text{ in}^2$$

$$A_{s \min} = \frac{200}{f_y} \times B \times d = \frac{200}{60000} \times (11 \times 12) \times 19.5$$
$$= 8.58 \text{ in}^2$$

$$A_{s \min} = \frac{3 \times \sqrt{f'_c}}{f_y} \times B \times d$$

$$= \frac{3 \times \sqrt{3000}}{60000} \times (11 \times 12) \times 19.5$$

$$= 7.05 \text{ in}^2$$

From the above values greater value will be selected thus $A_{s \min} = 8.58 \text{ in}^2$

STEP: 15

Using # 8 bars.

$$A_b = 0.785 \text{ in}^2$$

$$\text{No. of bars} = \frac{A_s}{A_b} = \frac{8.58}{0.785} = 10.92$$

≈ 11 bars in each

direction.

THE END.