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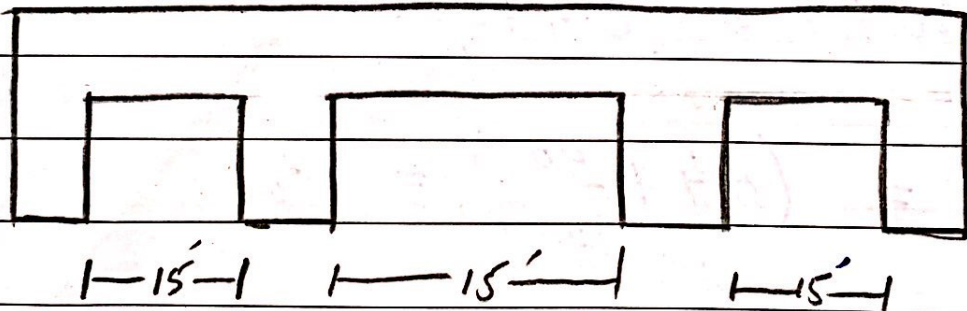
Section :- "B"

Subject :- PRED 1

Department :- Civil Engineering

Semester :- "Six"

QNO1

ANSI-Given Data:- \Rightarrow Clear Span b/w Supports = 15 ft. \Rightarrow Factored live load = 160 lb/ft². \Rightarrow FC = 4000 Psi. \Rightarrow Fy = 40 Ksi. \Rightarrow 3 equal spans Concrete Slab. \Rightarrow Service floor finish load = 20 lb/ft²Solution:-

Step #1Minimum Thickness :-By using
Formula

$$t_{\min} = \frac{L}{28} = \frac{15}{28} = 6.4$$

$$t_{\min} = \approx 6.5''$$

As $f_y \rightarrow 40 \text{ Ksi}$ So we will multiply a factor
with this thickness

$$\text{Factor} = \left(0.4 + \frac{f_y}{100} \right)$$

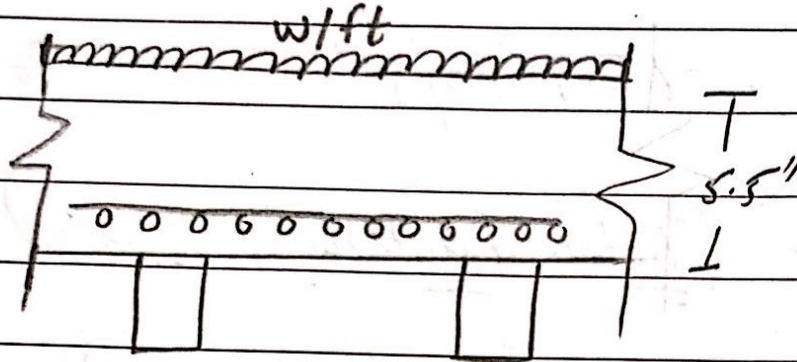
$$= \left(0.4 + \frac{40}{100} \right) = 0.8$$

$$\text{Factor} = 0.8$$

Hence the minimum thickness
will be 6.5×0.8

$$t_{\min} = 5.2 \approx 5.5''$$

Step # 2 :- (Effective Depth)



By formula

$$d = t - \text{clear cover} - \frac{1}{2}(\text{dia of main bars})$$

$$d = 5.5 - 0.75 - \frac{1}{2}\left(\frac{5}{8}\right)$$

$$d = \approx 4.5''$$

Step # 3 :- (Self wt of Slab) :-

By using formula.

$$\frac{t}{12} + \gamma_{\text{concrete}}$$

$$= \frac{5.5}{12} \times 150$$

$$= 68.75 \text{ lb/ft}^2$$

Step # 04:- (Total Factored Load)

$$\text{Factored live load} = 160 \text{ lb/ft}^2$$

So the factored Dead load will be

$$\text{D.L} = 1.2 (20 + 68.75)$$

$$\text{D.L} = 106.5 \text{ lb/ft}^2$$

$$\text{Total Factored load} = \text{D.L} + \text{L.L}$$

$$= 106.5 + 160$$

$$= 266.5 \text{ lb/ft}^2$$

$$= 0.2665 \text{ K/ft}^2$$

Step # 5 (ultimate Moment): -

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By using formula

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (15)^2 \times 12}{8}$$

$$M_u = 89.94 \text{ kip-inches}$$

Step # 6: -

Area of Steel for Main

Bars by Trial and Repeat Method: -

Trial # 01: -

Let depth of compression block

$$a = 0.2 \times L$$

$$a = 0.2 \times 5.5$$

$$a = 1.1''$$

$$A_{st} = \frac{m_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{1.1}{2})}$$

Trial #02:-

$$a = \frac{A_{st} \times f_y}{0.85 \times f'_c \times b} = \frac{0.63 \times 40}{0.85 \times 4 \times 12}$$

$$\Rightarrow 0.62 \text{ in}^2$$

$$A_{st} = \frac{m_u}{\phi \times f_y \times (d - \frac{a}{2})} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{0.6}{2})}$$

$$A_{st} = 0.59 \text{ in}^2$$

Trial #3:-

$$a = \frac{0.59 \times 40}{0.85 \times 4 \times 12} = 0.57''$$

As $f_y \rightarrow 40 \text{ ksi}$

So we will multiply a factor with this thickness

$$\text{Factor} = \left(0.4 + \frac{f_y}{100} \right)$$

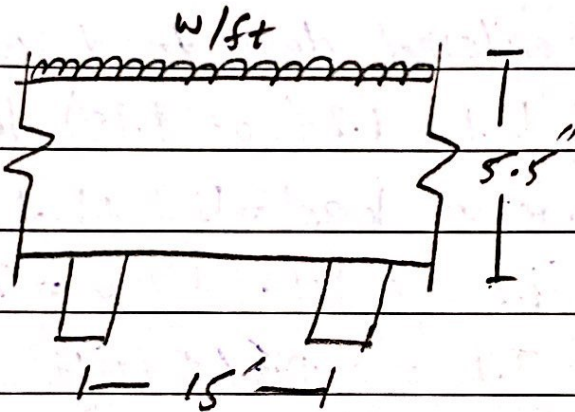
$$= \left(0.4 + \frac{40}{100} \right) = 0.8$$

Hence the minimum thickness will be 6.5×0.8

$$t_{\min} = 5.2 \text{ to } 5.5''$$

Step # 2 :-

Effective Depth :-



By formula

$$d = t - \text{Clear cover} - \frac{1}{2} (\text{dia of main bars})$$

$$= 5.5 - 0.75 - \frac{1}{2} \left(\frac{5}{8} \right)$$

$$\boxed{d = 4.5''}$$

Step # 3 :- Self weigh of Slab :-

By formula

$$\frac{t}{12} + \gamma \text{ Concrete}$$

$$= \frac{5.5 \times 150}{12}$$

$$= 68.75 \text{ lb/ft}^2$$

Step #4:-

Total Factored load:-

$$\text{Factored live load} = 160 \text{ lb/ft}^2$$

So the factored dead load will be

$$D.L = 1.2(20 + 68.75) = 106.5 \text{ lb/ft}^2$$

$$\text{Total factored load} = D.L + L.L$$

$$T.L = 106.5 + 160 = 266.5 \text{ lb/ft}^2$$

$$\cdot T.L = 0.2665 \text{ k/ft}^2$$

Step #5:-

Ultimate Moment:-

By using formula

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (13)^2 \times 12}{8}$$

$$M_u = 89.94 \text{ Kips-inches}$$

$$A_{ST} = \frac{89.94}{0.90 \times 40 \times \left(\frac{45 + 0.57}{2} \right)} = 0.59 \text{ in}^2$$

So we will use $A_{ST} = 0.59 \text{ in}^2$

Step # 6:-

Area of steel for distribution reinforcement.

By formula

$$A_{min} = 0.002 \times b \times l \rightarrow (\text{for Grade 40 steel})$$

$$= 0.002 \times 12 \times 5.5 \Rightarrow 0.132 \text{ in}^2$$

Step 7:-

Spacing for main bar.

By formula.

$$\text{Spacing} = \frac{A_b}{A_{ST}} \times 12$$

we use #6 A_{ST} bar dia = $\left(\frac{6}{8}\right)$ "

$$A_{req} = \frac{\pi}{4} \left(\frac{6}{8}\right)^2 = 0.442 \text{ in}^2$$

Step # 8 :-

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Spacing for distribution bars.

$$\text{Spacing} = \frac{A_b}{A_{ST}}$$

we use #5 bars so

$$\text{dia} = \left(\frac{5}{8}\right)'' , \text{Area} = \frac{\pi}{4} \left(\frac{5}{8}\right)^2 = 0.31 \text{ in}^2$$

$$\text{Spacing} = \frac{0.31}{0.132} \times 12 = 2.81 \approx 28''$$

Step # 10 :-Find sketch.

$$f_c = 4 \text{ ksi} , f_y = 40 \text{ ksi}$$

Main steel #6 at 9" c/c

Distribution steel #5 at 28" c/c



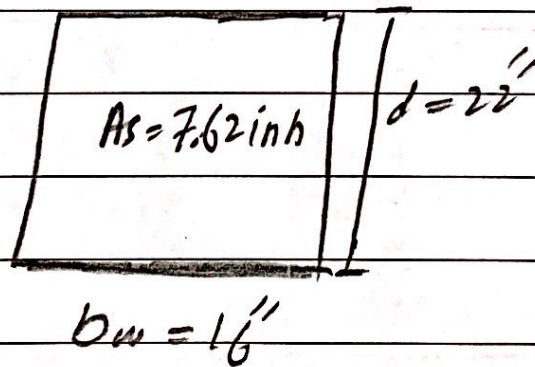
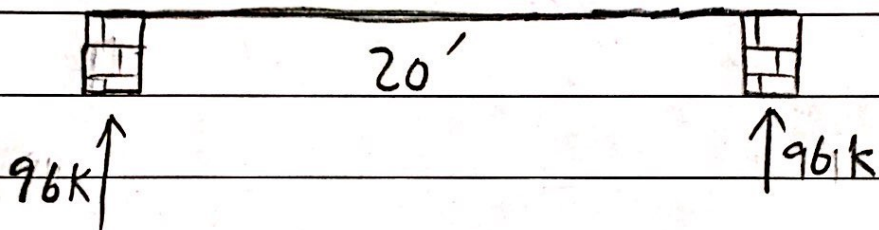
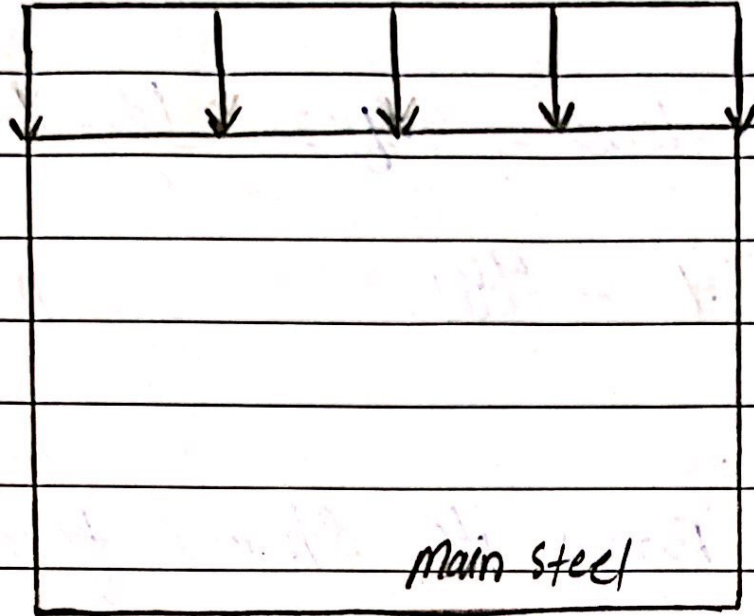
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QNO2

ANS

Solution:-

$$w = 9.4 \text{ kip/ft}$$



Step #01

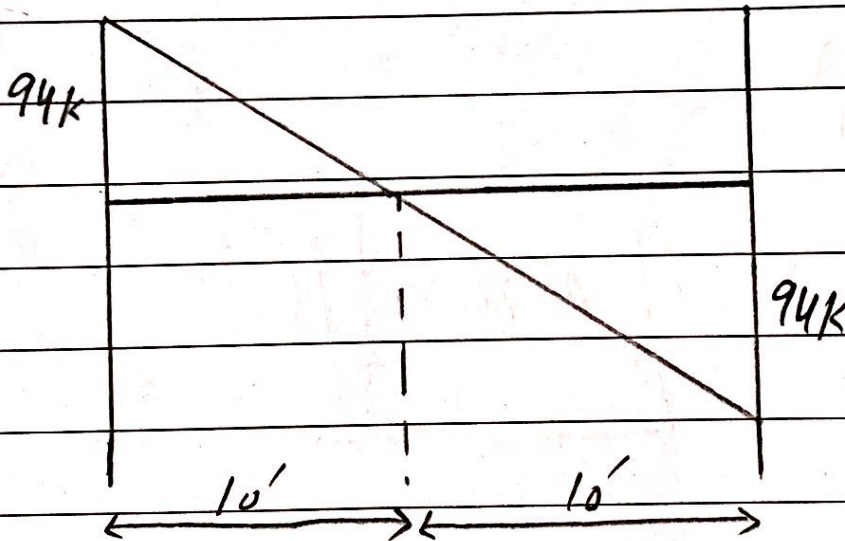
Find values of R_1 and R_2 .

$$\text{Total load} = 96 \times 20 = \frac{192}{2}$$

$$T.L = 96K$$

Step #2:

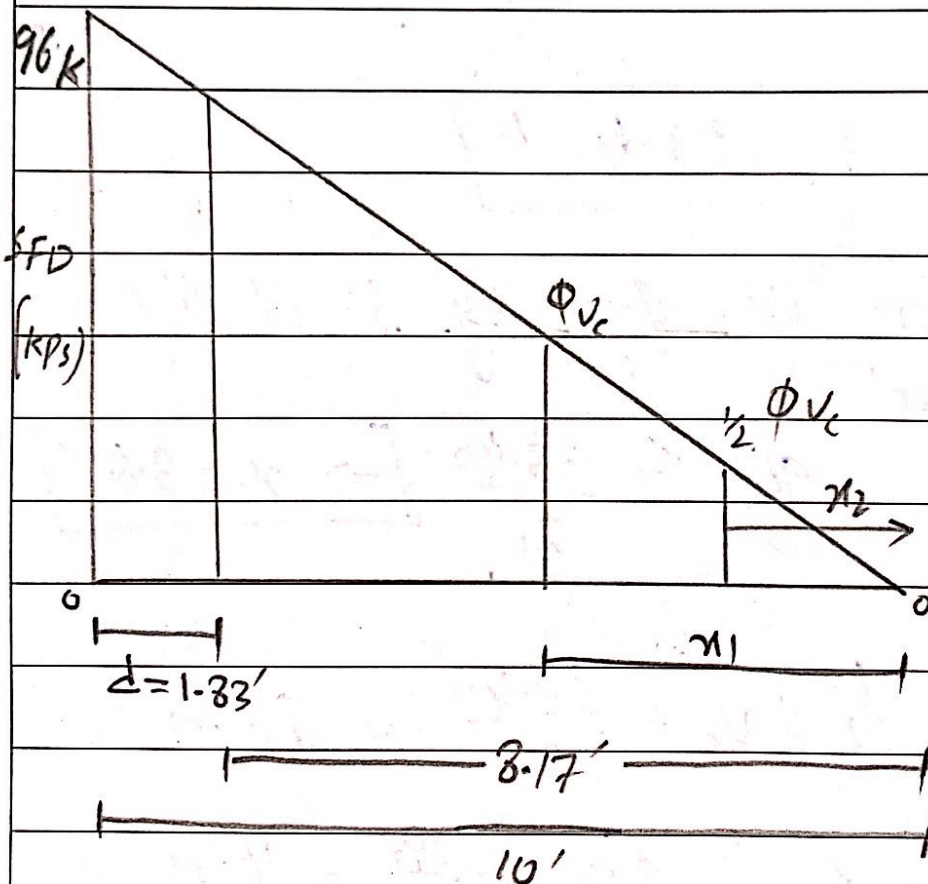
Draw its Shears force diagram.



Step #03:-

Find the value of Critical Shear " V_u " and its location.

As we know that Critical Section is located at distance " d " from Face of = $d = 22" = 1.83'$
 value of Critical Shears at distance ' d ' by Similarity of triangle



Step # 04:-

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Find the value of ' ϕV_c ' and ' $\frac{1}{2} \phi V_c$ ' and also its distance from zero shears to right side

$$\phi V_c = \phi \times 2 \times \sqrt{f'_c} \times b_w \times d$$

$$= \frac{0.75 \times 2 \sqrt{4000} \times 16 \times 22}{1000}$$

$$\boxed{\phi V_c = 33.40 \text{ k}}$$

Location of ϕV_c by similarity of " Δ_s "

$$\frac{96}{10} = \frac{33.40}{x_3} \Rightarrow \boxed{x_1 = 3.4'}$$

Now

$$\frac{1}{2} \phi V_c = \frac{33.40}{2} = 16.70 \text{ k}$$

$$\text{Location of } \frac{1}{2} \phi V_c \Rightarrow \frac{96}{10} = \frac{16.70}{x_2}$$

$$x_u = 1.74'$$

Step # 05:-

Value of ϕ_{Vc}

$$(V_u = \phi_{Vs} + \phi_{Vc})$$

So $\phi_{Vs} = V_u - \phi_{Vc} = 78.80 - 33.40$

$$\phi_{Vc} = 45.03 \text{ K}$$

Step # 06:-

Check on Section adequacy

$$\phi \cdot 8 \cdot \sqrt{f_c} \text{ bw} \cdot d = \frac{0.75 \cdot 8 \sqrt{4000}}{1000} \quad -16.22$$

$$= 133.57 \text{ K}$$

As

$$\phi_{Vs} < \phi \cdot 8 \cdot \sqrt{f_c} \text{ bw} \cdot d$$

\Rightarrow It means Section is adequate.

Step # 07:-

Check on Maximum Spacing for Stirrups

$$\phi \cdot 4 \cdot \sqrt{f_c} \cdot b_w d = \frac{0.75 \cdot 4 \sqrt{4000} \cdot 16 \cdot 22}{1000}$$

$$= 66.79 \text{ Kip}$$

As

$$\phi 4 \sqrt{f_c} b_w d > \phi V_s = 43.40 \text{ K}$$

So Max Spacing will be Selected from following four conditions:

$$(1) S_{max} = 24'' \quad (2) \frac{d}{2} = \frac{22}{2} = 11''$$

$$(3) S_{max} = \frac{0.22 \times 60000}{0.75 \sqrt{4000} \times 16} = 17.40$$

$$(4) S_{max} = \frac{0.22 \times 60,000}{50 \times 16} = 16.50''$$

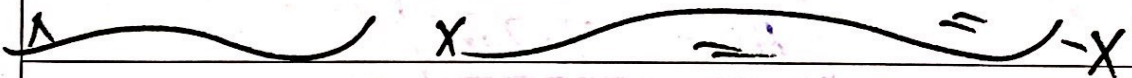
From above four conditions, Least value of spacing for # 3, 2 legged stirrup will be selected so $s_{max} = 11" c/c$

Step # 08:-

Spacing of stirrup from/at critical section.

$$s = \frac{0.75 \times 0.22 \times 60 \times 22}{76.80 - 33.44}$$

$$s = 5" c/c$$



Q No 3

Ans.

Step # 01 :-Find gross area of
Concrete $A_g = b \times b$ (since it is square tied
Column)

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual).}$$

Step # 02 :-Find the area of steel.Since $A_s = 5\%$ of A_g
 $= 0.05 \times 100$

$$A_s = 7.2 \text{ in}^2$$

Step # 3 :-Ultimate load Carrying
Capacity :-

$$P_u = \rho \times 0.80 \times [0.85 \times f'_c (A_g - A_s) + A_s \times f_y]$$

$$P_u = 0.65 \times 0.80 \left[0.85 \times 4 \left(144 - 7.2 \times 60 \right) \right]$$

$$P_u = 466.50 \text{ k}$$

Step # 4 :-

Sketch and design of Ties (c/c to distance) :-

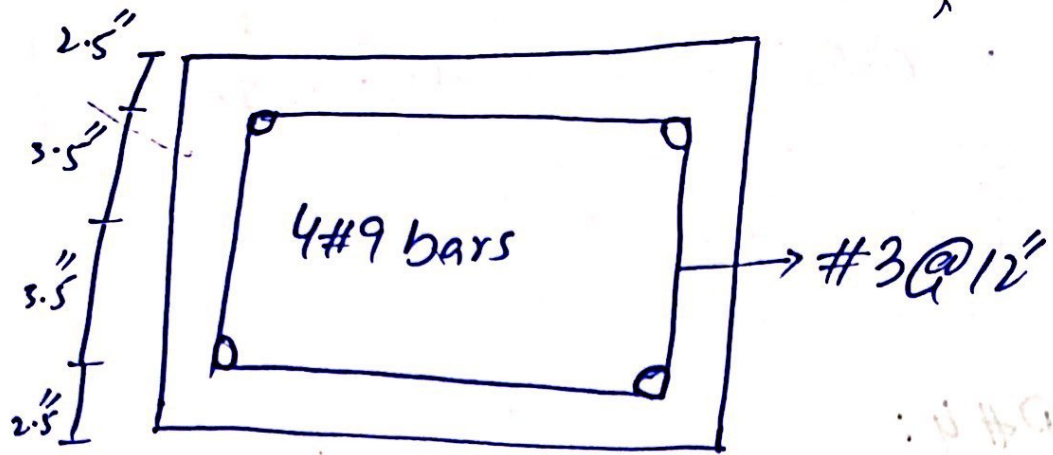
From the below value we choose the least value of all thus.

$$1) \text{ 16x dia of long bar} = 16 \times \frac{9}{8} = 18''$$

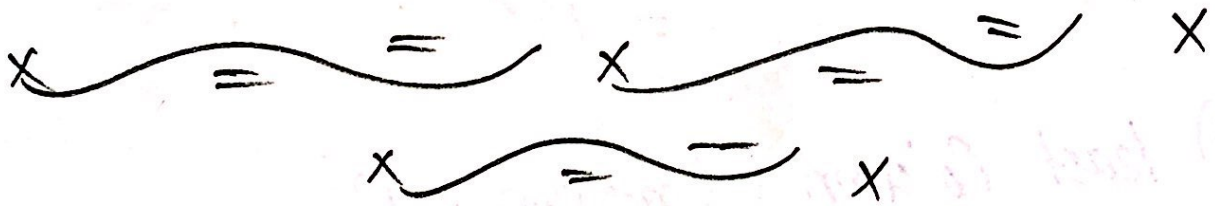
$$2) \text{ 48 x dia of the bar} = 48 \times \frac{3}{8} = 18''$$

$$3) \text{ least Column dimension} = 12''$$

So c/c distance b/w ties = 12''



* Since it is a tied Square Column
 So there is no spiral stirrup used.
 The stirrup used is of rectangular
 shape due to the specification of
 the structure thus we will use
 tie stirrups instead.



Q No 4

AnsSolution:-Step # 1:- Let $\alpha = 24^\circ$ Step # 2:- Total weight = wt of soil + wt of Rc

$$= 3 \times 120 + 2 \times 150 = 660 \text{ Psf}$$

$$= 0.660$$

Step # 03:-

Effective bearing Capacity

$$q_e = q_a - w = 2.50 - 0.660$$

$$q_e = 1.84 \text{ Ksf}$$

Step # 04:-

Required Area of Foundation

$$A_{req} = \frac{\text{Service load}}{q_e} = \frac{100 + 120}{1.84}$$

$$A_{req} = 119.56 \text{ ft}^2$$

Step #5:-

Since foundation is square

$$A_{req} = B \times B = 119.56$$

$$B \Rightarrow 119' - 56''$$

Step #6:-

$$q_{up} = \frac{\text{factored load}}{(B)^2}$$

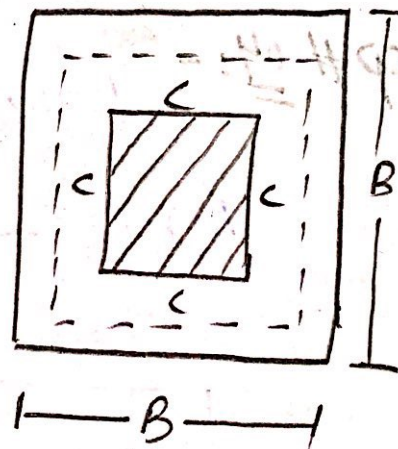
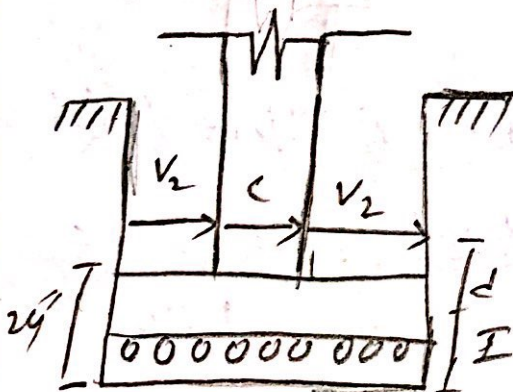
$$q_{up} = \frac{1.2 \times 100 + 1.6 \times 120}{(119.56)^2}$$

$$q_{up} = 0.021 \text{ k/ft}^2$$

Step #7:-

Punching Shear

$$b_0 = 4 + (c+d)$$



$d = h - \text{clear cover} - \text{dia of bar} - \frac{1}{2} \times d_b$

$$d = 24 - 3 - 1 - \frac{1}{2} + 1 = 19.5''$$

$$b_o = 4(16 + 19.5'') = 142''$$

Step #08:-

$$V_{r2} = q_{vp} \times \left[B^2 - (c+d)^2 \right]$$

$$= 0.021 \left[(119.56)^2 - \left(\frac{16 + 19.5}{12} \right)^2 \right]$$

$$\boxed{V_{r2} = 300}$$