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SUBJECT = Advanced Mechanics of Materials

PROGRAMME = M.S (S.E)

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ANSWER SHEET :

QUESTION NO : 01

Q1: Solution (1)

Moment of section - A is

$$M = 14951 \times 0.2$$

$$= 3068 \text{ Nm}$$

and the torque on the shaft is

$$T = 14951 \times 0.15$$

$$= 2301 \text{ Nm}$$

The normal stress due to M at A is

$$\sigma = \frac{64Md}{2\pi d^4} = \frac{-32M}{\pi d^3}$$

and The max Shear stress due to T at A is

$$\tau = \frac{32Td}{2\pi d^4} = \frac{16T}{\pi d^3}$$

The Shear stress due to the shear force F is zero at A.

$$\sigma_{1,3} = \frac{1}{2} \sigma \pm \frac{1}{2} (\sigma^2 + 4\tau^2)^{1/2},$$
$$\sigma_2 = 0$$

Max Shear Stress Theory

$$\tau_{max} = \frac{1}{2} (\sigma_1 - \sigma_3)$$

$$= \frac{1}{2} (\sigma_2 + 4\sigma_c^2)^{1/2}$$

$$= \frac{1}{2} \left(\frac{32}{\pi d^3} \right) (M^2 + T^2)^{1/2}$$

$$= \frac{16}{\pi d^3} (3068^2 + 2301^2)^{1/2}$$

$$= \frac{19531.5}{d^3} \text{ Pa}$$

With FOS $N = 15$ The value of τ_{max} becomes

$$N \tau_{max} = \frac{292972.5}{d^3} \text{ Pa}$$

This should not exceed the max shear stress value at yielding in the uniaxial Tension Test

Thus,

$$\frac{1}{d^3} (29297.5) = \frac{\sigma_y}{2} = \frac{207 \times 10^6}{2}$$

$$d^3 \times \frac{1}{d^3} (29297.5) = 103.5 \times 10^6 \times d^3$$

$$\frac{29297.5}{103.5 \times 10^6} = d^3$$

$$d^3 = 2.83 \times 10^{-4} \text{ m}^3$$

$$\text{or } d = 65.65 \times 10^{-3} \text{ m}$$

$$d = 6.565 \text{ cm}$$

(ii) Octahedral shear stress theory

$$\tau_{oct} = \frac{1}{3} \left[(\sigma_1 - \sigma_2)^2 + (\sigma_1 - \sigma_3)^2 + (\sigma_2 - \sigma_3)^2 \right]^{1/2}$$

with $\sigma_2 = 0$

$$\tau_{oct} = \frac{1}{3} \left[2\sigma_1^2 + 2\sigma_3^2 - 2\sigma_1\sigma_3 \right]^{1/2}$$

Substituting for σ_1 & σ_3 & Simplifying

$$\tau_{oct} = \frac{\sqrt{2}}{3} (\sigma^2 + 3\tau^2)^{1/2}$$

$$= \frac{\sqrt{2}}{3\pi d^3} \left[(32M)^2 + 3(16T)^2 \right]^{1/2}$$

$$= \frac{16\sqrt{2}}{3\pi d^3} (4M^2 + 3T^2)^{1/2}$$

$$= \frac{16\sqrt{2}}{3\pi d^3} \left[4 \left(\frac{3088}{\pi} \right)^2 + 3(2301)^2 \right]^{1/2}$$

or

$$= \frac{16\sqrt{2}}{3\pi d^3} \times 7316.7$$

Pa

$$= \frac{\sqrt{2}}{3\pi d^3} \times 117067$$

Equating this

$$\frac{\sqrt{2}}{3\pi d^3} \times 15 \times 117067 = \frac{\sqrt{2}}{3} \sigma_y$$

or

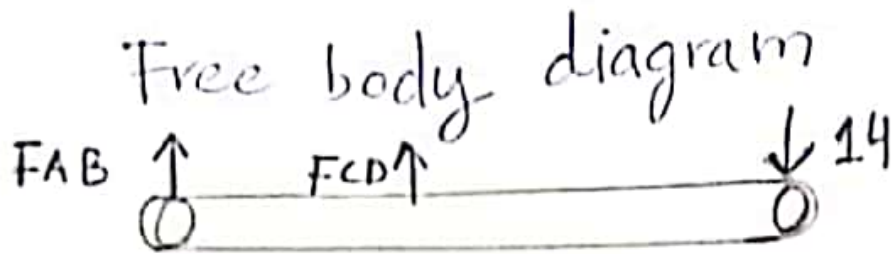
$$2 \times 117067 = \pi d^3 \quad \sigma_y = \pi d^3 \times 207 \times 10^6$$

$$\therefore d^3 = 10.56 \times 10^{-4}$$

$$d = 10.18 \text{ cm}$$

QUESTION NO : 02

Q2 ANSWER :-



$$\sum M_B = 0$$

$$0 = -(14 \text{ kN} \times 0.6 \text{ m}) + F_{CD} \times 0.2 \text{ m}$$

$$= \frac{16 \text{ kN} \times 0.6}{0.2} = \frac{F_{CD} \times 0.2}{0.2}$$

$$F_{CD} = 48 \text{ kN Tension}$$

$$\sum M_D = 0$$

$$0 = 14 \text{ kN} \times 0.4 - F_{AB} \times 0.2$$

$$\frac{F_{AB} \times 0.2}{0.2} = \frac{-14 \text{ kN} \times 0.4}{0.2}$$

$$F_{AB} = -30 \text{ kN Compression}$$

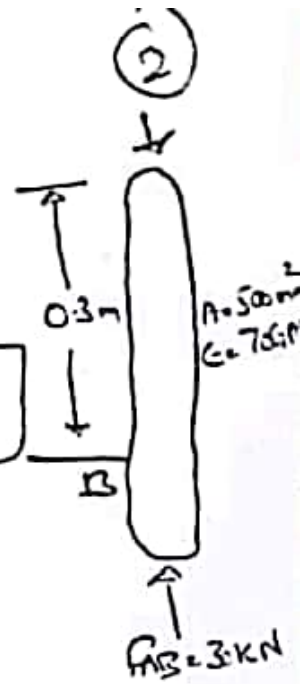
$$\delta_B = \frac{PL}{AE}$$

Displacement of B:

$$= \frac{(-30 \times 10^3 \text{ N})(0.3 \text{ m})}{(500 \times 10^{-6} \text{ m}^2)(70 \times 10^9 \text{ Pa})}$$

$$= -257 \times 10^{-6} \text{ m}$$

$$\Rightarrow \delta_B = 0.257 \text{ mm} \uparrow$$

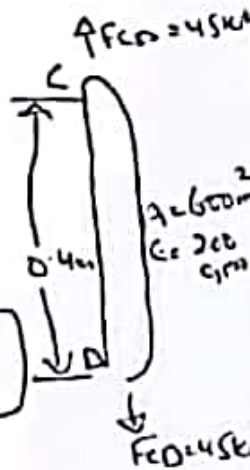


Displacement of D:

$$\delta_D = \frac{PL}{AE}$$

$$= \frac{(45 \times 10^3 \text{ N})(0.4 \text{ m})}{(600 \times 10^{-6} \text{ m}^2)(200 \times 10^9 \text{ Pa})}$$

$$= 150 \times 10^{-6} \text{ m} \Rightarrow 0.150 \text{ mm} \downarrow$$



Displacement of D

$$\frac{BB'}{DD'} = \frac{BH}{HD} = \frac{0.257}{0.150} = \frac{(200 \text{ mm}) - x}{x}$$

$$x = 36.85 \text{ mm}$$

$$\frac{EE'}{DD'} = \frac{HE}{HD}$$

~~$$\frac{\delta_E}{0.300 \text{ m}} = \frac{(400 + 73.7) \text{ mm}}{73.7 \text{ mm}}$$~~

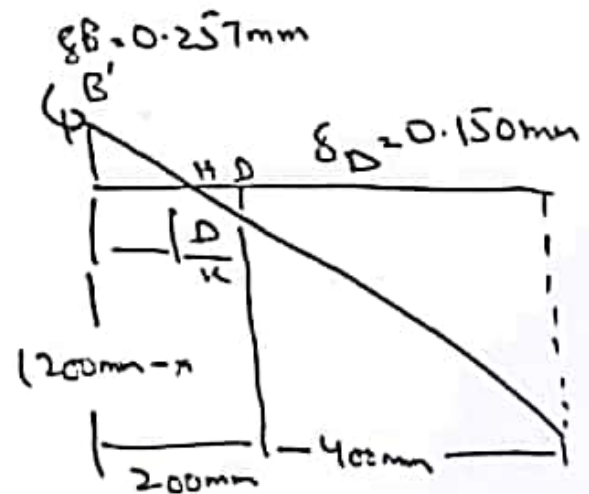
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$$\frac{EE'}{DD'} = \frac{HE}{HD}$$

$$\frac{\delta E}{0.150 \text{ mm}} = \frac{(400 + 36.85)}{36.85}$$

$$\delta E = \frac{400 + 36.85}{36.85} \times 0.150$$

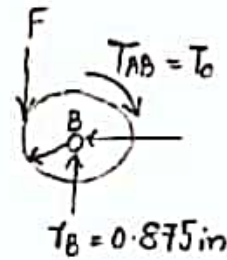
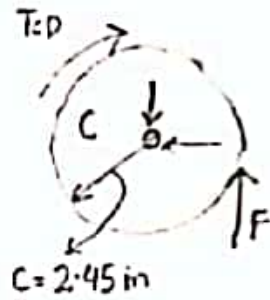
$$\delta E = 0.964 \text{ mm} \downarrow$$



QUESTION. NO: D3

Solution :

- Apply a static equilibrium analysis on the two shafts to find a relationship b/w T_{CD} and T_o
- Apply a kinematic analysis to relate the angular relation of the gears.
- find the maximum allowable torque on each shaft - choose the smallest.
- find the corresponding angle of twist for each shaft and the net angular rotation of end A.
- Apply a static equilibrium analysis on the two shafts to find a relationship b/w T_{cp} and T_o

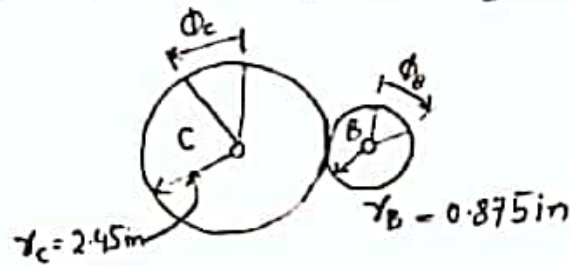


$$\sum M_B = 0 = F(0.875 \text{ in}) - T_0$$

$$\sum M_C = 0 = F(2.45 \text{ in}) - T_{CD}$$

$$T_{CD} = 2.8 T_0$$

→ Apply a kinematic analysis to relate the angular rotation of the gears.

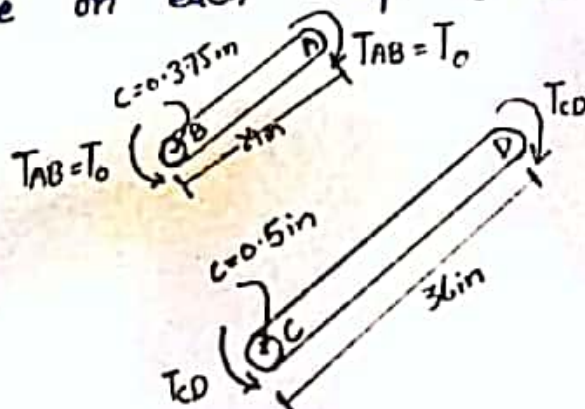


$$r_B \phi_B = r_C \phi_C$$

$$\phi_B = \frac{r_C}{r_B} \phi_C = \frac{2.45 \text{ in.}}{0.875 \text{ in.}} \phi_C$$

$$\phi_B = 2.8 \phi_C$$

→ Find the T_0 for the maximum allowable torque on each shaft choose the smallest



$$\tau_{\max} = \frac{T_{AB}c}{J_{AB}} \Rightarrow 10,000 \text{ psi} = \frac{T_0(0.375 \text{ in.})}{\frac{\pi}{2}(0.375 \text{ in.})^4}$$

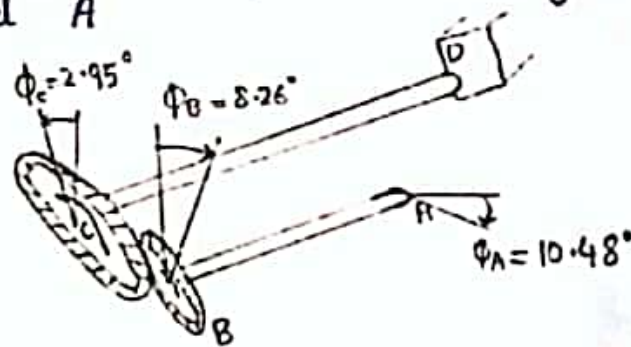
$$= 10,000 \text{ psi} = \frac{T_0(0.375 \text{ in.})}{0.0310 \text{ in}^4}$$

$$= 10,000 \text{ psi} * 0.0310 \text{ in}^4 = T_0(0.375 \text{ in.})$$

$$= 310 \text{ lb.in}^2 = T_0 0.375 \text{ in.}$$

$$= T_0 = \frac{310 \text{ in}^2 \cdot \text{lb}}{0.375 \text{ in.}} \Rightarrow \boxed{T_0 = 826 \text{ lb.in}}$$

- Find the corresponding angle of twist for each shaft and the net angular rotation of end A



$$\phi_{A/B} = \frac{T_{AB}L}{J_{AB}G} = \frac{(826 \text{ lb.in})(24 \text{ in})}{\frac{\pi}{2}(0.375)^4(15 \times 10^6 \text{ psi})} = 0.0425 \text{ rad} =$$

$$= 0.0425 \text{ rad} = 2.43^\circ$$

$$\phi_{C/D} = \frac{T_{CD}L}{J_{CD}G} = \frac{2.8(826 \text{ lb.in})(24 \text{ in})}{\frac{\pi}{2}(0.5 \text{ in})^4(15 \times 10^6 \text{ psi})}$$

$$= 0.0376 \text{ rad} = \boxed{2.15^\circ}$$

$$\phi_B = 2.8 \phi_C = 2.8(2.15) = 6.02^\circ$$

$$\phi_A = \phi_B + \phi_{A/B} = 6.02^\circ + 2.43^\circ = \boxed{\phi_A = 8.45^\circ}$$

QUESTION NO : 04

(1)

$$I D = 14951$$

$$So, V = 14 + 3 = 17 \text{ kips}$$

⇒ Shear stresses in the flange

$$\tau = \frac{VQ}{It} = \frac{V}{I} (S) \frac{h}{2} = \frac{Vh}{2I} S$$

$$\tau_B = \frac{Vhb}{2 \left(\frac{1}{12} th^2 \right) (6b+h)} = \frac{6vb}{th(6b+h)}$$

$$\tau_B = \frac{6 (17 \text{ kips}) (4 \text{ in})}{(0.15 \text{ in}) (6 \text{ in}) (6 \times 4 \text{ in} + 6)}$$

$$\tau_B = 16 \text{ kips}$$

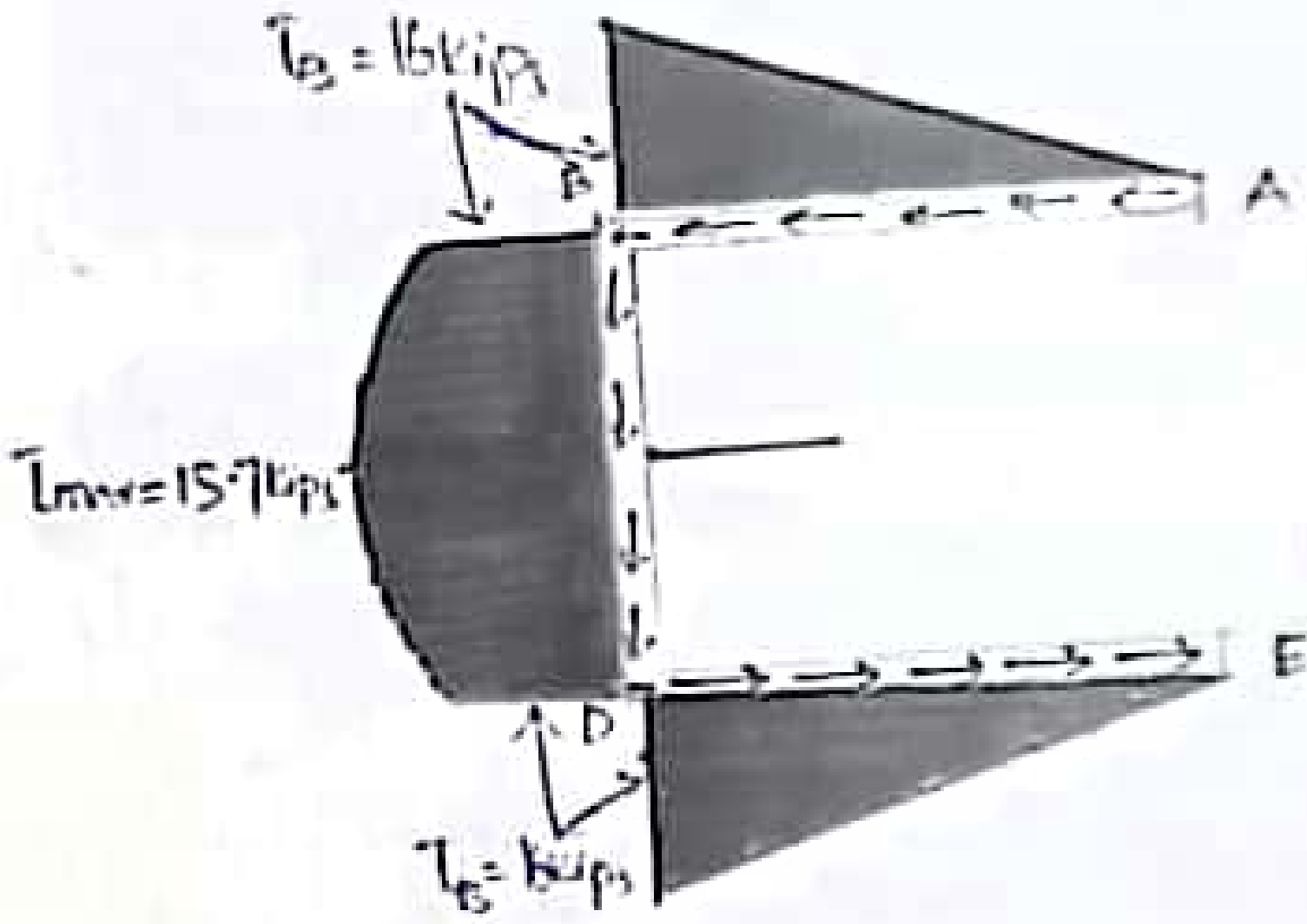
⇒ Shear stress In the Web,

$$\tau_{max} = \frac{VQ}{It} = \frac{V \left(\frac{1}{8} ht \right) (4b+h)}{\frac{1}{12} th^2 (6b+h) t}$$

$$= \frac{3v(4b+h)}{2th(6b+h)} \quad (2)$$

$$\bar{I}_{max} = \frac{3(17 \text{ Kips})(4 \times 4 \text{ in} + 6 \text{ in})}{2(0.15 \text{ in})(6 \text{ in})(6 \times 6 \text{ in} + 6 \text{ in})}$$

$$\bar{I}_{max} = 15.71 \text{ Kips}$$



QUESTION NO : 05

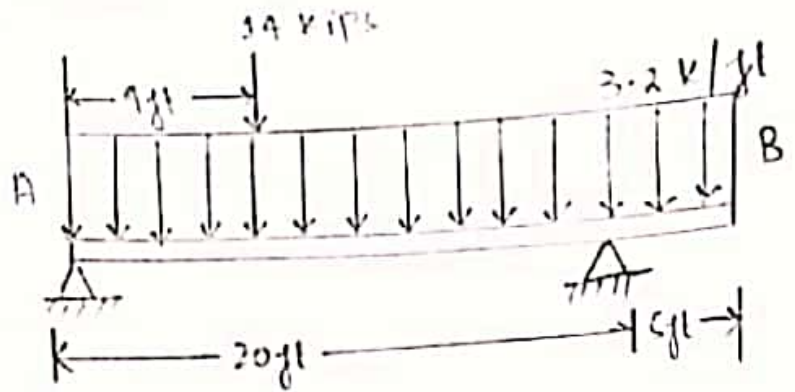
Q.05 SOLUTION: (1)

Given Data:

$$\delta = 14 + 4 = 18$$

and

$$\tau = 14 + 1 = 15$$



(i) Determine Reaction at A and D.

$$\sum M_A = 0$$

$$-14 \times 9 - 80 \times 12.5 + R_D \times 20 = 0$$

$$\Rightarrow -135 - 1000 + 20R_D = 0$$

$$\Rightarrow -1135 + 20R_D = 0$$

$$\Rightarrow 20R_D = 1135$$

$$\Rightarrow R_D = \frac{1135}{20}$$

$$\Rightarrow \boxed{R_D = 56.75 \text{ kips}} \rightarrow \text{Eq (*)}$$

Now

$$\sum F_y = 0$$

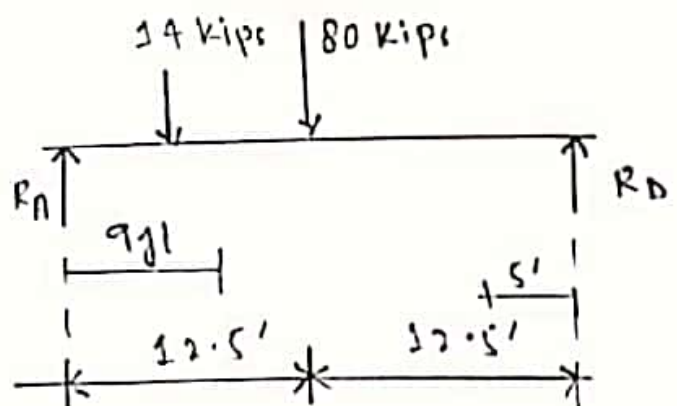
$$R_A + R_D - 14 \text{ kips} - 80 \text{ kips} = 0$$

$$R_A + R_D - 95 \text{ kips} = 0$$

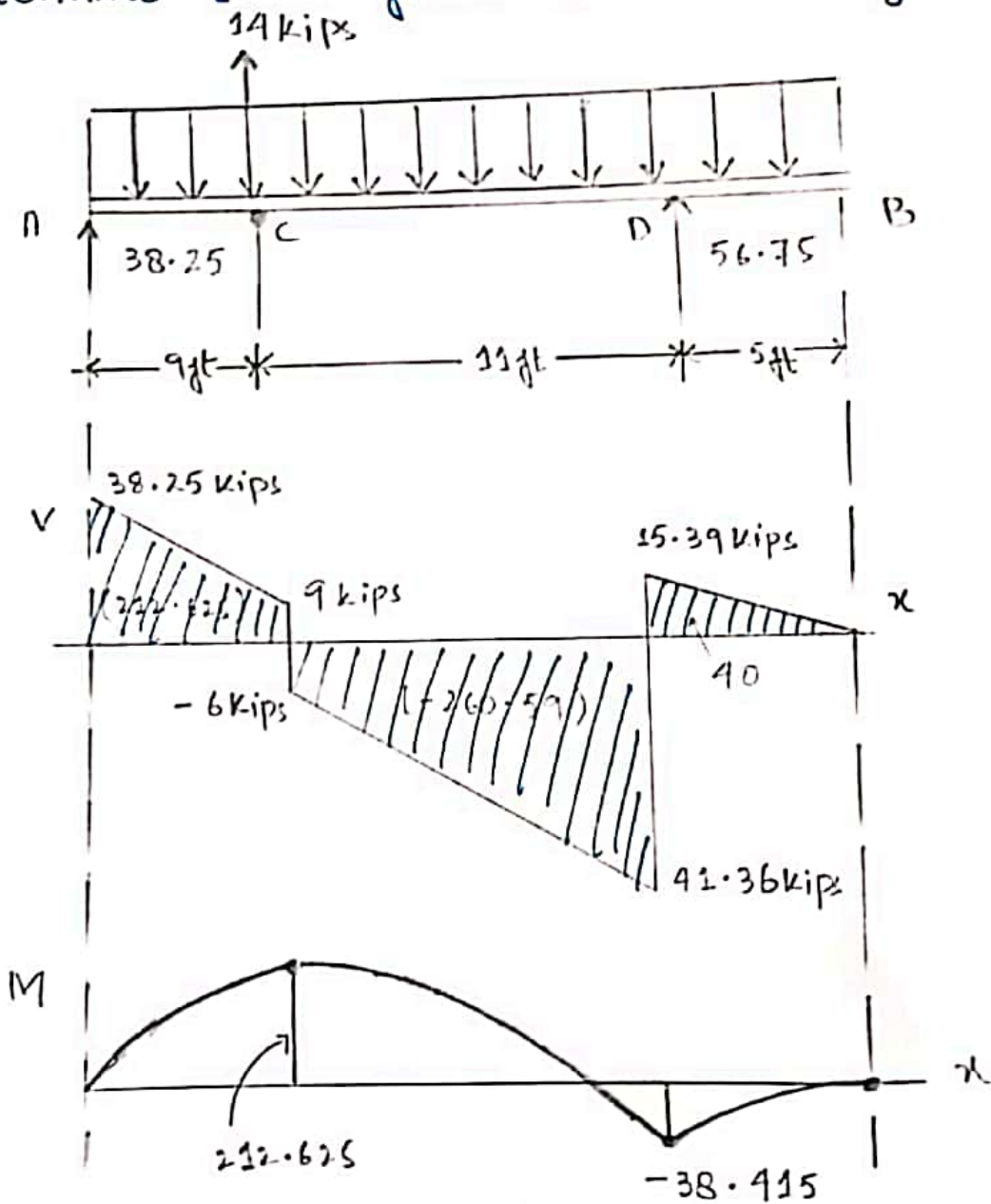
$$\boxed{R_A + R_D = 95 \text{ kips}} \rightarrow \text{Eq (#)}$$

Put Eq (*) in Eq (#)

$$R_A = 38.25 \text{ kips}$$



(2)
 (ii) To determine shear force and Bending.



$$|M| = 239.4 \text{ kip-in with } V = 9 \text{ kips}$$

$$|V|_{\max} = 41.36 \text{ kips}$$

(3)

Calculate required section modulus and select appropriate beam section.

$$S_{\min} = \frac{|M|_{\max}}{\sigma_{\text{all}}} = \frac{24 \text{ kips} \cdot \text{in}}{24 \text{ ksi}} = 119.7 \text{ in}^3$$

Select W₂₁ x 62 beam section

* Find maximum shearing stress, Assuming uniform shearing stress in web,

$$\tau_{\max} = \frac{V_{\max}}{A_{\text{web}}} = \frac{41.36 \text{ kips}}{8.40 \text{ in}^2} = 5.12 \text{ ksi} < 14.5 \text{ ksi}$$

* Find maximum normal stress

$$\sigma_a = \frac{M_{\max}}{S} = 2873 \frac{60 \text{ kip} \cdot \text{in}}{127 \text{ in}^3} = 22.6 \text{ ksi}$$

$$\sigma_b = \sigma_a \frac{Y_b}{c} = (22.6 \text{ ksi}) \frac{9.88}{10.5} = 21.3 \text{ ksi}$$

$$\tau_b = \frac{V}{A_{\text{web}}} = \frac{12.2 \text{ kips}}{8.40 \text{ in}^2} = 1.45 \text{ ksi}$$

$$\sigma_{\max} = \frac{21.3 \text{ ksi}}{2} + \sqrt{\left(\frac{21.3 \text{ ksi}}{2}\right)^2 + (1.45 \text{ ksi})^2}$$

$$\sigma_{\max} = 21.4 \text{ ksi} < 24 \text{ ksi}$$