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Sec # B

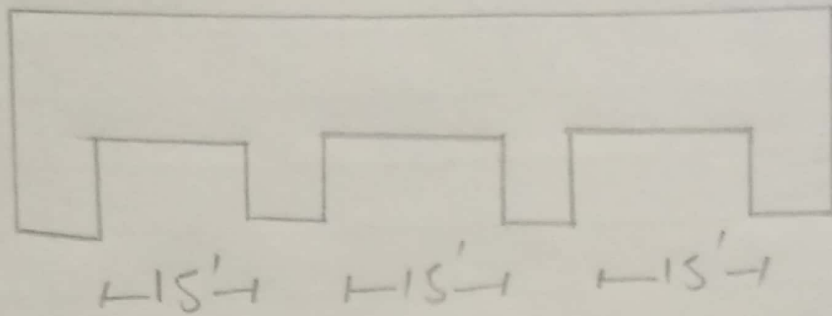
Sub # PRC

Ans:

Q:- 1

Pg# 1

Sol:-



Step # 1: (Minimum Thickness)

By using formula

$$t_{min} = L/28 = 15/28 = 6.4 \\ \approx 6.5''$$

As $F_y \rightarrow 40 \text{ ksi}$

So we will multiply

a factor with thin thickness

$$\text{factor} = \left(0.4 + \frac{F_y}{100} \right)$$

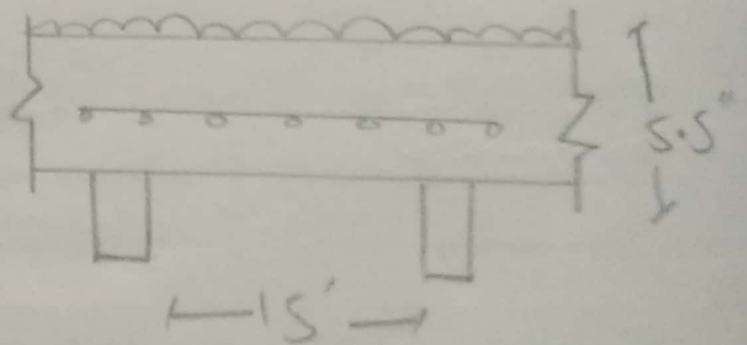
$$= \left(0.4 + \frac{40}{100} \right) = 0.8$$

Hence the minimum thickness will be

$$6.5 \times 0.8$$

$$t_{\min} = 5.2 \approx 5.5''$$

Step: 2: (effective depth)
 w/t/t



By formula

$$d = t - \text{clear cover} - \frac{1}{2} (\text{dia of main bar})$$

$$= 5.5 - 0.75 = \frac{1}{2} (5/8)$$

$$d \approx 4.5''$$

(3)

Step #3: (Self wt of Slab)

By formula

$$t/12 + \gamma \text{ concrete}$$

$$= \frac{5.5}{12} \times 150 = 68.75 \text{ lb/ft}^2$$

Step #4: (Total factored load)

Factored live load = 160 lb/ft^2

So the factored Dead

load will be

$$D.L = 1.2(20 + 68.75) = 106.5 \text{ lb/ft}^2$$

Total factored load = D.L + L.L

$$= 106.5 + 160$$

$$= 266.5 \text{ lb/ft}^2 = 0.2665 \text{ k/ft}^2$$

Step #5 (ultimate moment) (4)

By using formula

$$M_u = \frac{w_u \times L^2}{8} = \frac{0.2665 \times (15)^2}{8} \times 12$$

$$= 89.94 \text{ kip-inch}$$

Step #6: Area of Steel
for Main Bars By Trial
and Repeat method.

Trial #1: let depth of compression block

$$a = 0.2 \times t$$

$$= 0.2 \times 5.5 = 1.1''$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)}$$

$$= \frac{89.94}{0.90 \times 40 \left(4.5 - \frac{1.1}{2}\right)}$$

(5)

Trial #2: $A_{st} = 0.63 \text{ in}^2$

$$\bar{a} = \frac{A_{st} \times f_y}{0.55 \times f_c' \times b} = \frac{0.63 \times 40}{0.85 \times 4 \times 12} \Rightarrow 0.62 \text{ in}$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times \left(4.5 - \frac{0.6}{2}\right)}$$

$$A_{st} = 0.59 \text{ in}^2$$

Trial #3:

$$a = \frac{0.59 \times 40}{0.85 \times 4 \times 12} = 0.57 \text{ in}$$

$$A_{st} = 89.94$$

(b)

$$0.90 \times 40 \left(4.5 - \frac{5.7}{2} \right)$$

$$= 0.59 \text{ in}^2$$

So we will use $A_{st} = 0.59 \text{ in}^2$

Step #7: Area of steel for distribution reinforcement

$$A_{min} = 0.002 \times b \times t \rightarrow \text{(for Grade 40 steel)}$$

$$= 0.002 \times 12 \times 5.5 = 0.132 \text{ in}^2$$

$$= 0.132 \text{ in}^2$$

Step # 8: Spacing for main bar

By formula

$$\text{Spacing} = \frac{Ab}{As} \times 12$$

We use # 6 bar $d = \left(\frac{6}{8}\right)$ "

$$\text{Area} = \frac{\pi}{4} \left(\frac{6}{8}\right)^2 = 0.442 \text{ in}^2$$

Step # 9: Spacing for distribution bar

$$\text{Spacing} = \frac{Ab}{As}$$

We use # 5 bar so

$$d_{ia} = \left(\frac{5}{8}\right)^2, \text{ Area} = \frac{\pi}{4} \left(\frac{5}{8}\right)^2$$

$$= 0.31 \text{ in}^2$$

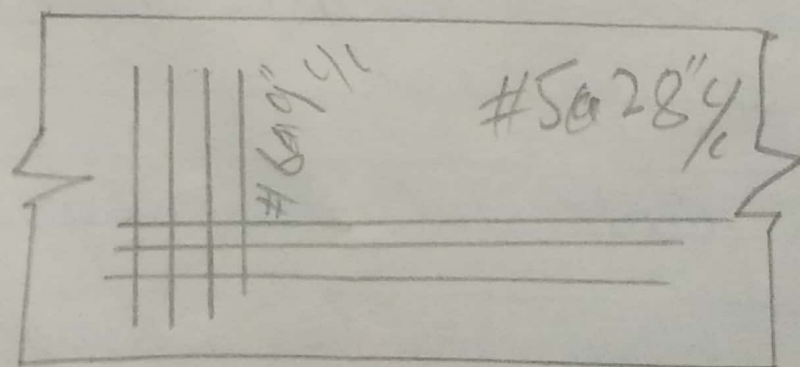
$$\text{Spacing} = \frac{0.31}{0.132} \times 12 = 2.81 \approx 28''$$

Step #10: find sketch.

$$f_c' = 4 \text{ Ksi}, f_y = 40 \text{ Ksi}$$

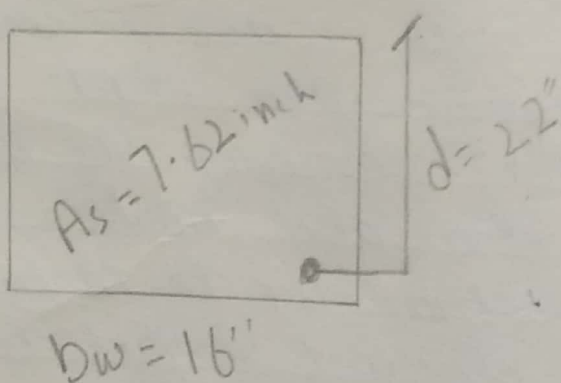
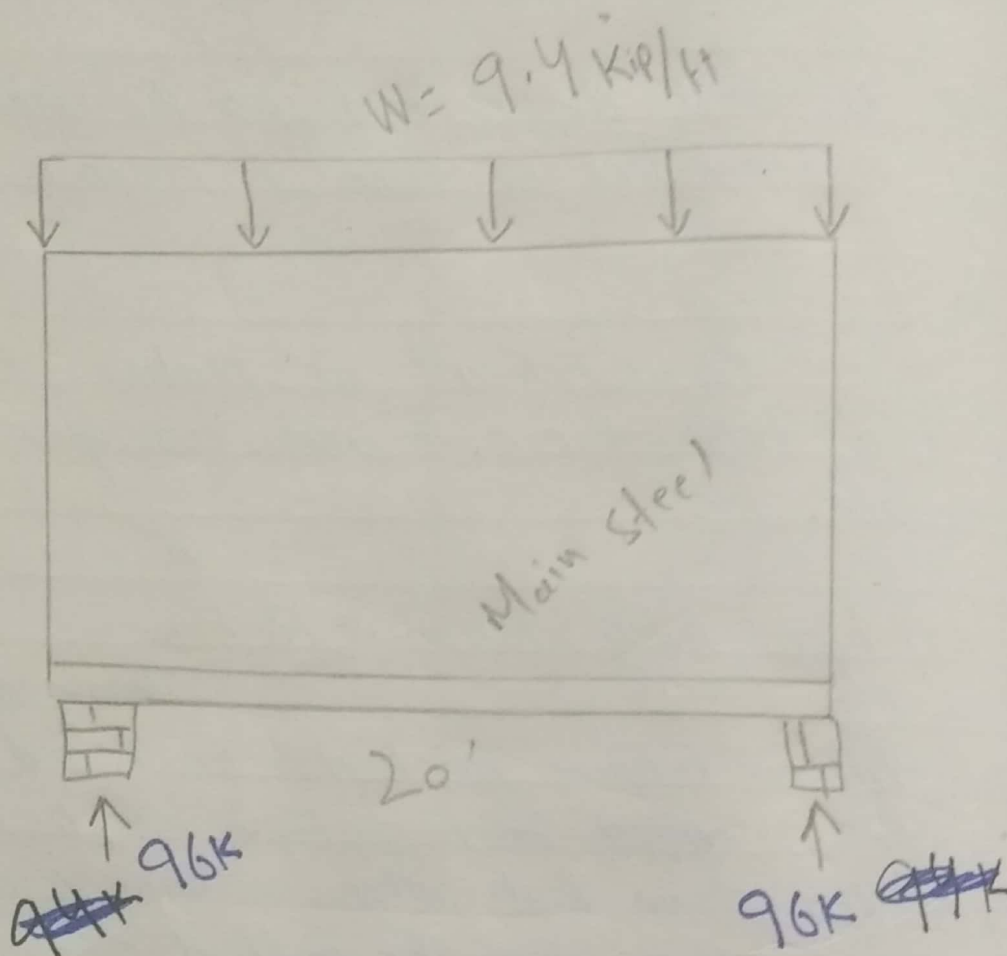
Main Steel #6 at 9" c/c

Distribution Steel #5 at 28" c/c



Q: 2

Sol:-

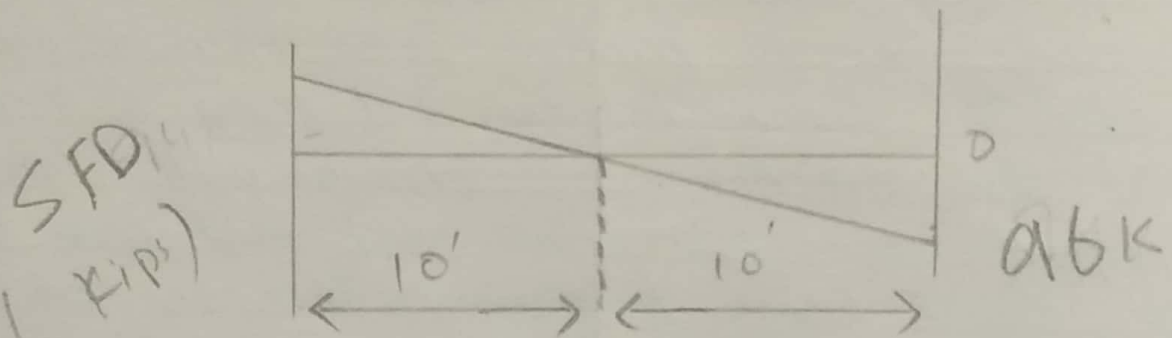


Step #1: find values of R_1
and R_2

$$\text{Total load} = 9.6 \times 20 = \frac{192}{2} = 96 \text{ k}$$

$$\text{unit load} = w \times x_c = \frac{16}{12} \times 150 = 200 = 0.2 \text{ k/ft}$$

Step #2: Draw Shear force Diagram



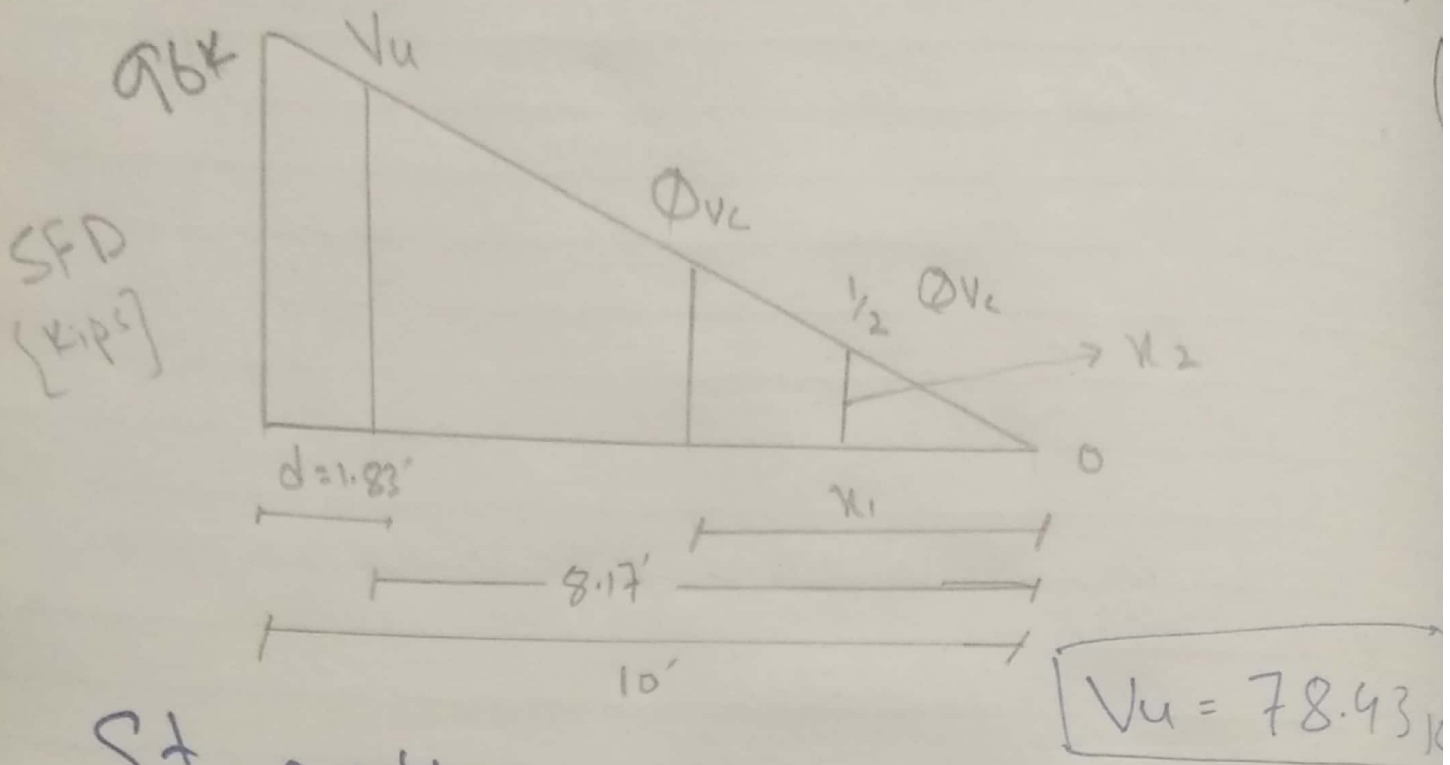
Step #3:

Find the value of Critical Shear ' V_u ' and its location.

As we know that critical section is located at distance

$$d \text{ from face of } = d = 22'' = 1.83'$$

Value of Critical Shears at distance 'd' by Similarity of triangles.



Step #4:

Find the value of ' ΦV_c ' and $\frac{1}{2} \Phi V_c$ ' and also its distance from zero shear to right side

$$\Phi V_c = \Phi \times \rho \times \sqrt{f_c'} \times b_w \times d$$

$$= \frac{0.75 \times \rho \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$\Phi V_c = 33.40k$$

location of Φ_{Vc} by Similarity
of D_s

$$\frac{96}{10} = \frac{3340}{X_1} \Rightarrow \boxed{X_1 = 3.4}$$

Now

$$\frac{1}{2} \Phi_{Vc} = \frac{33.40}{2} = 16.70 \text{ K}$$

location of $\frac{1}{2} \Phi_{Vc} \Rightarrow \frac{94}{10} = \frac{16.70}{X_2}$

$$\boxed{X_2 = 1.74}$$

Step # 5: Value of Φ_{Vs}

$$\left(\cancel{\Phi_{Vs}} \right) (V_0 = \Phi_{Vs} + \Phi_{Vc})$$

$$\text{So } \Phi_{Vs} = V_0 - \Phi_{Vc} = 78.80 - 33.40$$

$$\boxed{\Phi_{Vs} = 45.40 \text{ K}}$$

Step # 6:

Check on Section
adequacy

$$\phi \cdot 8 \cdot \sqrt{f_c} \cdot b_w \cdot d = \frac{0.75 \cdot 8 \sqrt{4000} \cdot 16.62}{1000}$$
$$= 133.57 \text{ k}$$

As

$$\phi_{us} < \phi 8 \sqrt{f_c} \cdot b_w \cdot d$$

\Rightarrow It means Section is adequate

Step # ~~7~~: Check on Maximum
Spacing for stirrups

$$\phi \times 4 \times \sqrt{f_c} \times b_w \times d = \frac{0.75 \cdot 4 \sqrt{4000} \cdot 16.22}{1000}$$

$$= 66.79 \text{ kip}$$

As

$$\phi 4 \sqrt{f_c'} \text{ bwd} > \phi V_s = \text{---}$$

So Max Spacing will
be Selected from following
Four Condition.

$$\textcircled{1} S_{\text{max}} = 24'' \quad \textcircled{2} \frac{d}{2} = \frac{22}{2} = 11''$$

$$\textcircled{3} S_{\text{max}} = \frac{0.22 \times 60000}{0.7 \sqrt{4000 \times 16}} = 17.40$$

$$\textcircled{4} S_{\text{max}} = \frac{0.22 \times 60,000}{50 \times 16} = 16.50''$$

From above four condition (15)

least value of spacing
for #3, 2 legged stir up
will be selected

$$\text{So } s_{\text{max}} = 11'' \text{ c}$$

Step #8

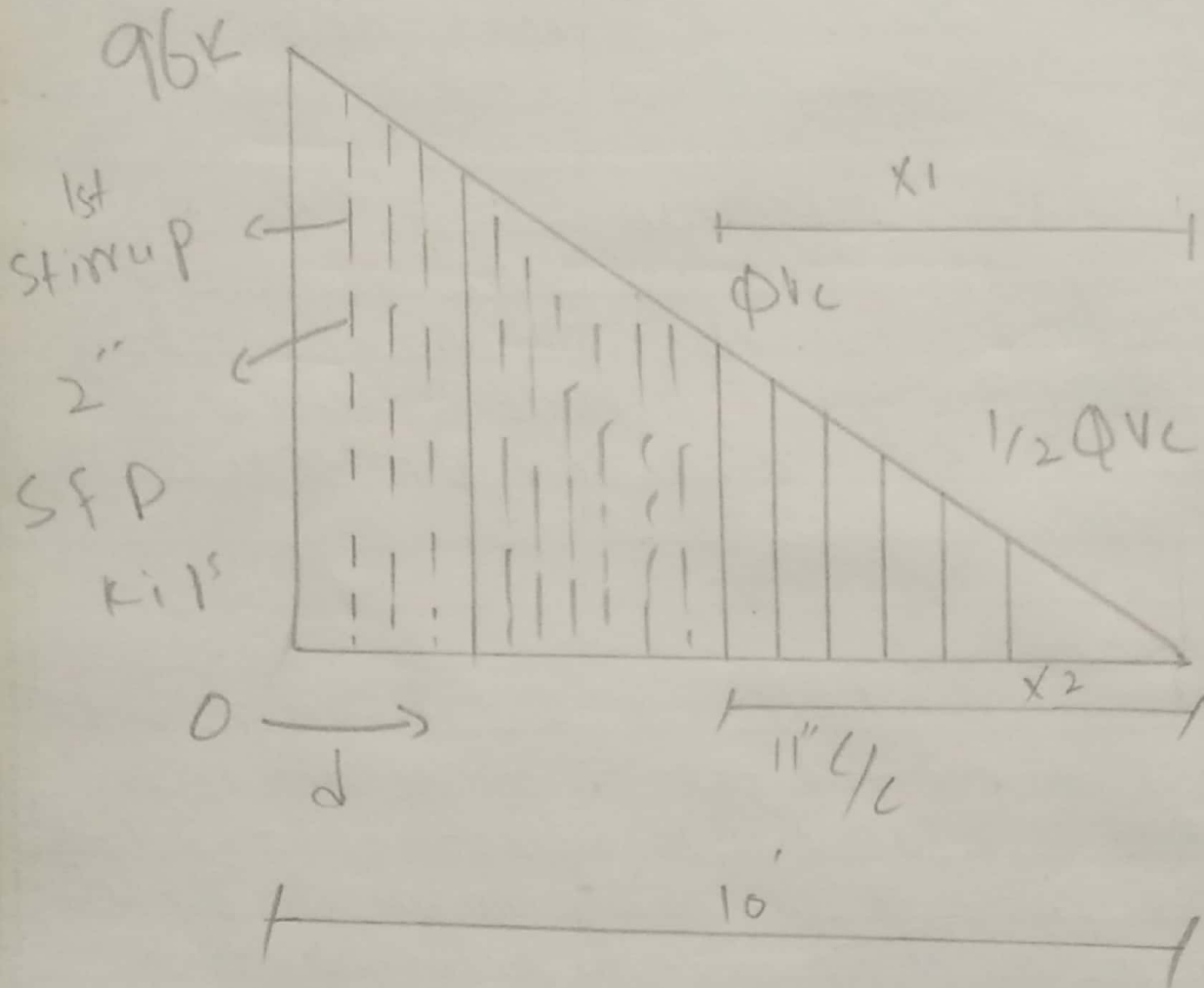
Spacing of stir up
from/at critical section

$$s = \frac{0.75 \times 0.22 \times 60 \times 22}{76.86 - 33.44}$$

$$s = 5'' \text{ c}$$

Step #9:

5' 0"



As we know that

First stirrup from face of support

$$= \frac{8}{2} = \frac{5}{2} \approx 2.5$$

Ans:

Q: 3 :-

(17)

Step #1: Find gross area of concrete.

$$A_g = b \times b \text{ (Since it's Square tied Column)}$$

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

Step #2: Find the area of steel.

$$\text{Since } A_s = 5\% \text{ of } A_g$$

$$= 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

Step #3: Ultimate load carrying capacity

$$P_u = \phi = 0.80 \times [0.85 \times f_c' \times (A_g - A_s) + A_s \times f_y]$$

$$= 0.65 \times 0.80 [0.85 \times 4 [144 - 7.2] + 7.2 \times 60]$$

$$P_u = 466.50 \text{ k}$$

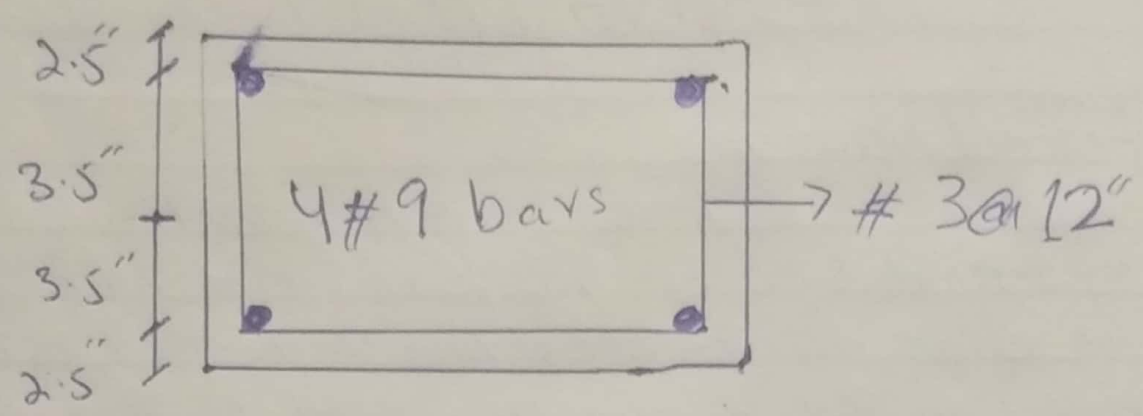
Step 4: Sketch design of tier (4/2 to dist)

From the below value we choose the least value of all the:

1) - $16 \times \text{dia of long bar} = 16 \times 9/8 = 18''$

2) $48 \times \text{dia of tie} = 48 \times 3/8 = 18''$

3) least column dimension = 12"
 So c/c distance b/w ties = 12"



★ Since it's a tied square column so there is ~~no~~ spiral stirrup used. the stirrup used is of rectangular shape due to the specification of the structure thus we will use tie stirrups instead.

Q:-4:-

Sol:-

Step # 1:

$$\text{let } h = 24''$$

Step # 2:

Total weight = wt of Soil + wt of R_c

$$= 3 \times 120 + 2 \times 150$$

$$= 660 \text{ psf} = 0.660 \text{ Ksf}$$

Step # 3:

effective bearing capacity

$$q_e = q_a - W = 2.50 - 0.660$$

$$q_e = 1.84 \text{ Ksf}$$

Step #4: Required area for foundation

$$A_{req} = \frac{\text{Service load}}{q_c} = \frac{100 + 120}{1.84}$$

$$A_{req} = 119.56 \text{ ft}^2$$

Step #5: Since foundation is square:

$$A_{req} = B \times B = 119.56$$

$$B \Rightarrow \cancel{119.56} \quad 119.5 \Rightarrow B \approx 11'$$

Step #6:

$$q_{up} = \frac{\text{factored load}}{(B)^2}$$

$$V_{up} = 1.2 \times 100 + 1.6 \times 120$$

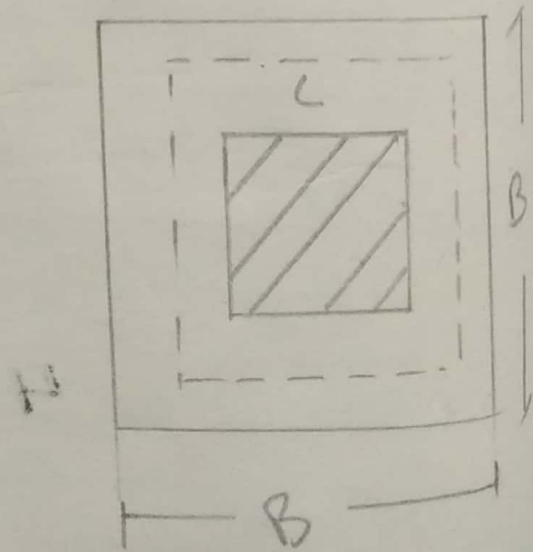
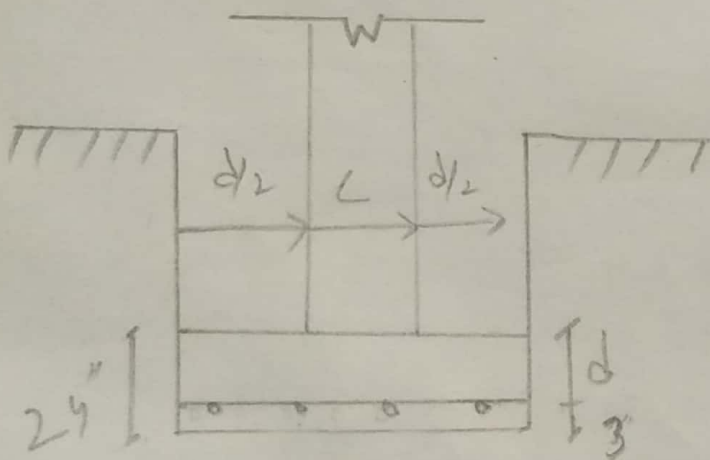
$$\frac{(11)^2}{2.58}$$

$$V_{up} = 2.58 \text{ K/ft}$$

Step #7:

Punching Shear:

$$b_o = 4 + (c + d)$$



$$d = h - \text{clear (over-dia of bar)} - \frac{1}{2} \times d_b$$

$$d = 24 - 3 - 1 - \frac{1}{2} + 1 = 19.5''$$

$$b_o = 4(16 + 19.5'') = 142''$$

Step # 8:

$$V_{u2} = V_{up} \times [B^2 - (c+d)^2]$$

$$= \frac{2.58}{12} \left[(11)^2 - \left(\frac{16 + 19.5}{12} \right)^2 \right]$$

$$\cancel{V_{u2} = 300}$$

$$V_{u2} = 289.60 \text{ k}$$

Step # 9:

$$\cancel{\phi V_{up}} = \cancel{\phi \times 4 \times \sqrt{f_c}}$$

$$\phi V_{up} = \phi \times 4 \times \sqrt{f_c} \times b \times d$$

$$= \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5}{1000}$$

$$\phi V_{up} = 525.38$$

Step # 10:

$$\phi V_{u1} = \phi V_{up} \times B \times \left[\frac{B}{2} - \frac{C}{2} - d \right]$$

$$V_{u1} = 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{2} - \frac{19.5}{12} \right]$$

$$V_{u1} = 90.95 \text{ K}$$

Step # 11:

Self shear capacity:

$$\begin{aligned} \phi_{vc} &= \phi \times 2 \times \sqrt{f_c'} \times b \times d \\ &= \frac{0.75 \times 2 \times \sqrt{4000} (11 \times 12 - 16)}{1000} \end{aligned}$$

$$= 110.04 \text{ K} > V_{u1} \Rightarrow \text{O.K.}$$

Step # 12: Ultimate moment:

$$M_u = \frac{V_{up} \times B \times (B - c)^2}{8} = \frac{2.58 \times 11}{8} \times \left(\frac{11 - 16}{12} \right)^2$$

$$M_u = 331.49 \text{ K} \approx 3977.93 \text{ K}^{\text{cm}}$$

Step #13:

Trial: 01,

$$\text{let } a = 0.2 \times h = 0.2 \times 24 \\ = 4.8''$$

$$= \frac{3977.93}{0.90 \times 60 \times \left(11 - \frac{4.8}{2}\right)} = 8.56 \text{ in}^2$$

Trial: 2:

$$a = \frac{8.5 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.53''$$

$$As = \frac{3977.93}{}$$

$$0.90 \times 60 \times \left(11 - \frac{1.53}{2}\right)$$

$$= 7.197 \text{ in}^2$$

Trial: 3:

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$AS = \frac{3977.93}{\cancel{0.85} \times 0.90 \times 60 \left(11 - \frac{1.28}{2} \right)}$$

$$= 7.1 \text{ m}^2$$

So that area 7.1 m^2

STEP # 14: Check the min
reinforcement by the
following three Methods

a)

$$A_{smin} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24$$
$$= 5.70 \text{ in}^2$$

b)

$$A_{smin} = \frac{200}{f_y} \times B \times d = \frac{200}{60000} \times (11 \times 12) \times 19$$
$$= 8.58 \text{ in}^2$$

(c)

$$A_{smin} = \frac{3 \times \sqrt{f_c'} \times B \times d}{f_y} = \frac{3 \times \sqrt{3000} \times 1000 \times 100}{60000}$$

$$= 7.05 \text{ in}^2$$

from above value
greater value will
be selected then

$$A_{smin} = 8.58 \text{ in}^2$$

Step #15: use #8 bar

$$A_b = 0.785 \text{ in}^2$$

$$N \text{ of bars} = \frac{A_s}{A_b} = \frac{8.58}{0.785} = 10.92$$

≈ 11 bars in

each direction