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Section :- A

Subject :- Mechanics of Solid 2

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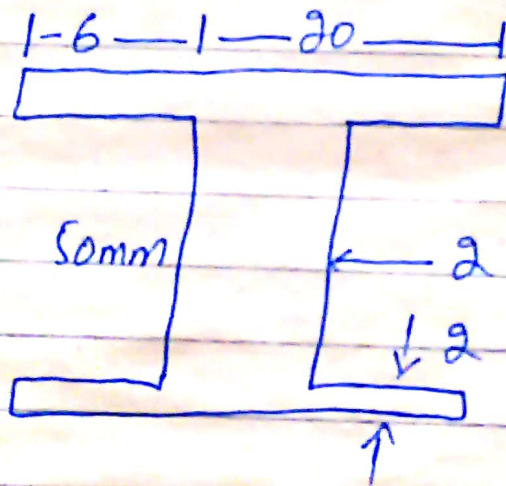
(4)

Question No:- 1

Part (a)

Answer:

Solution:



Required: Location of Shear Centre.

Sol: As we know

$$e = \frac{t f h^2 b^2}{4I}$$

and:

$$I = 2 \left(\frac{bh^3}{12} + Ay^2 \right) + \left(\frac{bh^3}{12} + Ay^2 \right)$$

(2)

$$I = 2 \left(\frac{26(2)^3}{12} + (20 \times 2)(25)^2 \right) + \left[\frac{2(50)^3}{12} + 0 \right]$$

$$I = 50034.66 + 20.833$$

$$I = 70867.99 \text{ mm}^4$$

$$e = \frac{2(50)^2(25)^2}{4(70867.99)} = 11.02 \text{ mm}$$

So Shear Centre $e = 11.02 \text{ mm}$



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Question: 1

Part (b) ::

Answer::

Data::

$$\Rightarrow H = 26 \text{ ft}$$

\Rightarrow assume diameter

$$D = 22 \text{ ft}$$

$$\Rightarrow \text{tangential stress} = 600 \text{ lb/ft}^3$$

$$\Rightarrow \text{Specific weight of water tank} = 62.4 \text{ lb/ft}^3$$

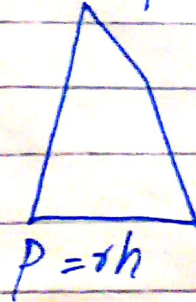
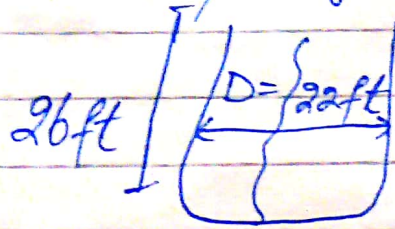
we have to find the thickness = ?

(4)

Solution:

The pressure developed by water = $p = \gamma h$

$$\delta t = \frac{PD}{2t}$$



$$\delta t = \frac{PD}{2t} \Rightarrow \frac{\gamma h D}{2t}$$

$$2t \times \delta t = \gamma h D$$

$$2t = \frac{\gamma h D}{\delta t}$$

$$t = \frac{\gamma h D}{\delta t \times 2}$$

$$t = \frac{(62.4) \times (26 \times 12) \times (22 \times 12)}{600 \times 2}$$

$$\underline{t = 0.24''}$$



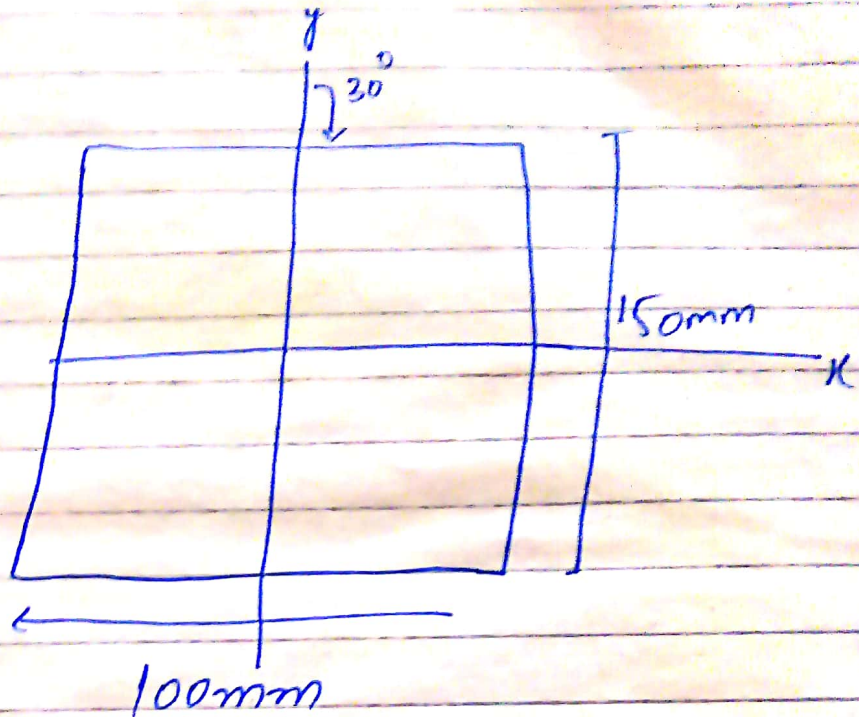
(5)

Question:-02:

Part (a)

Answer:

Solution:



moment of inertia

$$I_z = \frac{bh^3}{12} = \frac{0.1(0.15)^3}{12} = I_z = 2.8125 \times 10^{-5}$$

Now,

$$I_y = \frac{hb^3}{12} = \frac{0.15(0.1)^3}{12}$$

$$I_y = 1.25 \times 10^{-5}$$

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$$\theta = \frac{M_{zy}}{I_z} + \frac{M_{yz}}{I_y}$$

$$\theta = \frac{m \cos \theta}{I_z} + \frac{m \sin \theta}{I_y}$$

where,

$$m = P \cos \theta = 12 \cos 30^\circ = m_z$$

$$m_z = 10.8510$$

$$m \sin \theta = P \sin \theta = m_y$$

$$m_y = 12 \sin 30$$

$$m_y = -11.8563$$

$$\theta = \left(\frac{m_z}{I_z} \right) + \left(\frac{m_y}{I_y} \right)$$

$$\theta = \frac{1.851}{2.812 \times 10^{-5}} + \left(\frac{-11.8563}{1.25 \times 10^{-5}} \right)$$

$$= 882628 \text{ Nm}^2$$

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Sgn Convention

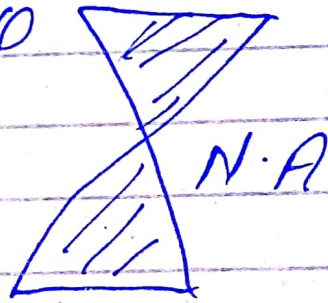
| | |
|---|---|
| 2 | 1 |
| 3 | 4 |

if we take compression as negative and tension as positive and the beam.

Simply Supported

| | |
|---|---|
| 2 | 1 |
| 3 | 4 |

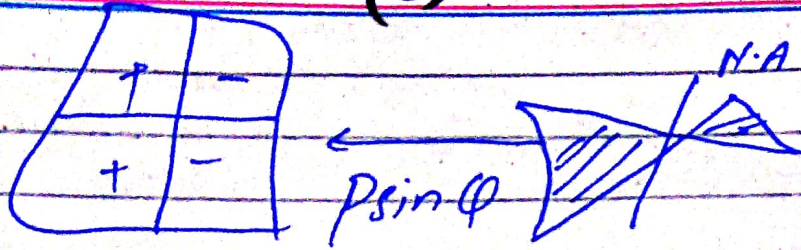
Point



Quadrant 1, 2 -ve

Quadrant 3, 4 +ve

(8)



Quadrant 1, 4 -ive
Quadrant 2, 3 +ive

In case of unsymmetrical loading the neutral axis of an angle of α . the principal axis (i)

& the algebraic sum of stress at N.A. is zero.

$$\sigma = \frac{M \cos \phi}{I_z} y + \frac{M \sin \phi}{I_y} z \quad \text{--- (1)}$$

In this case, N.A. passes through 2, 4 So,

$$\sigma = \frac{M \cos \phi}{I} y + \frac{M \sin \phi}{I_y} z$$

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Let Consider a point A on N.A lies in Quadrant 2, where

- Bending Stress due to $p \cos \phi$ is compressive ϵ_p
- Bending Stress due to $p \sin \phi$ is tensile.

$$\text{eg (i)} \Rightarrow 0 = \frac{-M \cos \phi y_A}{I_z} + \frac{M \sin \phi z_A}{I_y}$$

$$\Rightarrow 0 = -\frac{M \cos \phi}{I_z} y_A + \frac{M \sin \phi}{I_y} z_A$$

$$\Rightarrow \frac{M \cos \phi}{I_z} y_A + \frac{M \sin \phi}{I_y} z_A$$

$$\frac{y_A}{z_A} = \frac{I_z}{I_y} \frac{\sin \phi}{\cos \phi} \Rightarrow \tan \phi_x = \frac{I_z}{I_y} \tan \phi \rightarrow \text{(ii)}$$

(10)

Now put values of \bar{I}_z, \bar{I}_y & ϕ
in eq (ii)

$$\tan \alpha = \frac{\bar{I}_z \tan 30^\circ}{\bar{I}_y}$$

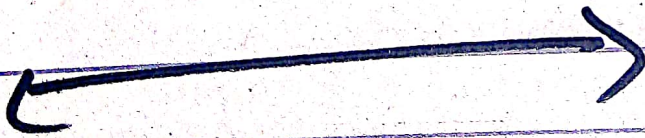
$$\Rightarrow \tan \alpha = \frac{2.8125 \times 10^{-5} (\tan 30^\circ)}{1.25 \times 10^{-5}}$$

$$\tan \alpha = -14.4129$$

$$\alpha = \tan^{-1}(-14.4129)$$

$$\alpha = 1.5^\circ$$

$$\alpha = 1^\circ 30' 5''$$



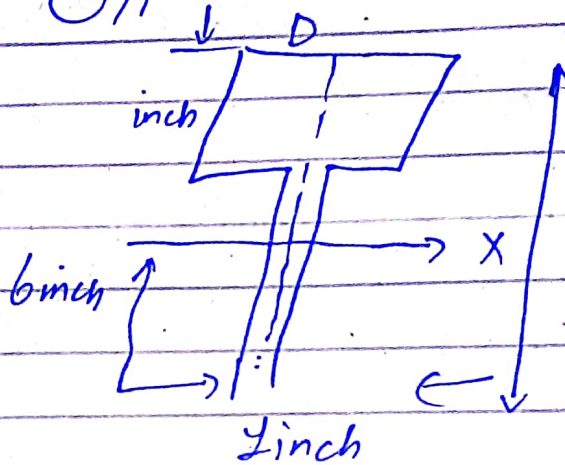
(11)

Question (2)

Part (b)

Answers:-

Solution:- Given,



$$L = 16 \text{ ft}$$

$$I_x = 112 \cdot 6 \text{ inch}^4$$

$$I_y = 18 \cdot 7 \text{ inch}^4$$

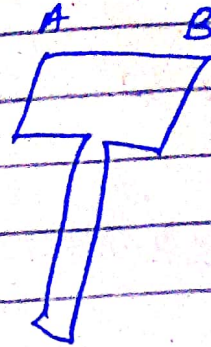
$$\sigma_c = 12000 \text{ psi}$$

$$\sigma_t = 500 \text{ psi}$$

(12)

Solution

By looking figer we can judge that maximum compression would



ocure on a & maximum tension C at B. these will tension as well a compression which will reduce that effect of each other, so we will calculatate stresses at A & C.

So,

$$\sigma_A = \frac{M \times y}{I_x} + \frac{m \times y}{I_y} \times \text{comp.}$$

$$\sigma_C = \frac{m \times y}{I_x} + \frac{m \times y}{I_y} \quad (\text{Tension})$$

Now M_x & m_y

(13)

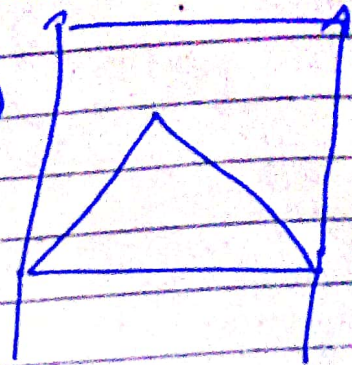
So,

$$M_x = \frac{p \cos 60^\circ (16 \times 12)}{4}$$

$$M_x = 48 p \cos 60^\circ$$

$$M_y = \frac{p \sin 60^\circ (16 \times 12)}{4}$$

$$M_y = 48 p \sin 60^\circ$$



Now,

$$I_A = \frac{M_x^2}{I_x} + \frac{M_y^2}{I_y}$$

$$\Rightarrow 1200 = \frac{48 p \cos 60^\circ \times 3.7^2}{112.8}$$

$$\frac{48 \sin 60^\circ \times 3.7^2}{18.7}$$

Solving the equation

$$\Rightarrow p = 1638.6 \text{ lb}$$

(14)

Now

$$J_c = \frac{mxy}{I_x} + \frac{myx}{I_y}$$

$$5000 = 48p \cos 60^\circ \times (5.93) + \frac{48p \sin 60^\circ \times 0.5}{}$$

Solving the equation 8.7

$$p = 2104.9 \text{ lb}$$

So the maximum load p applied should 1638.6 lb

~~Be ended~~

Question No.: 3Answer..Solution..

Given data

$$\text{Length} = 10 \text{ ft}$$

$$E = 10.3 \times 10^6$$

$$b = 0.75$$

$$h = 2$$

$$\text{Factor of Safety} = 2$$

Required Data:-

(a) Safe load of haved = ?

(b) Safe load of at fixed = ?

As we know that

Strut is a compression member act as a column.

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Case I:

Strut or Column act as a hinged column about an axis perpendicular to the direction

dimension then,

$$I = I_x \frac{(0.75)(2)^3}{12} = 0.5 \text{ inch}^4$$

$L_e = L =$ (For hinged ended column)

$$P_{CB} = \frac{\pi^2 EI}{L_e^2} = \frac{(1)^2 (10.8 \times 10^6) (0.5) (\pi^2)}{(10 \times 12)^2}$$

$$P_{CV} = 35.26.176 \text{ lb}$$

(17)

$$P_{safe} = \frac{P_{cr}}{\text{Factor of Safety}} = \frac{3526.176}{2}$$

$$P_{safe} = 1763.088 \text{ lb}$$

Case 2:

Strut or Column act as a fixed ended column about an axis perpendicular to ~~0.75~~ is

Side i.e y-axis

$$I = I_y = \frac{2 \left(\frac{0.75}{12} \right)^3}{12} = 0.070 \text{ inch}^4$$

$L_e = 4/2$ (For fixed ended column)

then,

$$P_{cr} = \frac{(\pi)^2 EI \pi^2}{L_e^2}$$

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$$= \frac{(1)^2 (10.3 \times 10^6) (0.07) (\bar{1}^2)}{\left(\frac{10}{2} \times 12\right)^2}$$

$$P_{cr} = 1974.658 \text{ lb}$$

$$P_{safe} = \frac{P_{cr}}{\text{factor of safety}}$$

$$P_{safe} = \frac{1974.658}{2}$$

$$P_{safe} = 987.329 \text{ lb}$$

In both cases take the smaller value of P_{safe} .

$$P_{safe} = \cancel{918.17} \quad 987.329 \quad 1763$$

By ended thinks you Sir:

