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Section : A

Subject : PRCD1

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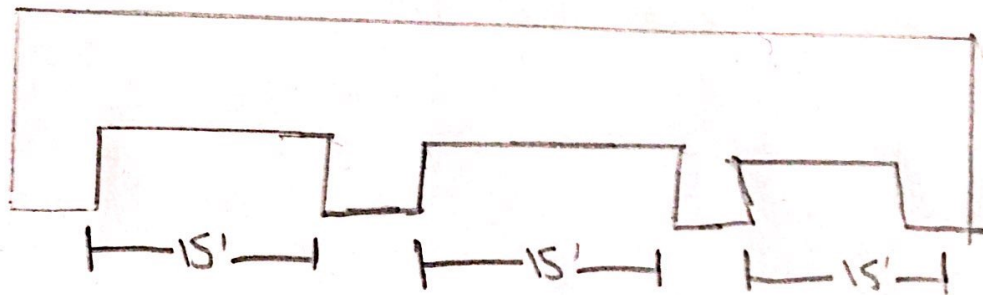
Qno 1,

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Given Data:-

- > 3 equal spans concrete slab
- > Clear span b/w supports = 15ft
- > Factored line load = 100 lb/ft<sup>2</sup>
- > Service Floor Finish load = 20 lb/ft<sup>2</sup>
- >  $F'_c = 4000 \text{ psi}$
- >  $F_y = 40 \text{ ksi}$

Solution:-



Step 1:-

Using Formula

$$t_{\min} = \frac{l}{28} = \frac{15}{28} = 6.4 \approx 6.5''$$

As  $F_y = 40 \text{ ksi}$

We multiply a Factor with this thickness

$$\text{Factor} = \left( 0.4 + \frac{F_y}{100} \right)$$

$$\text{Factor} = \left( 0.4 + \frac{40}{100} \right) = 0.8$$

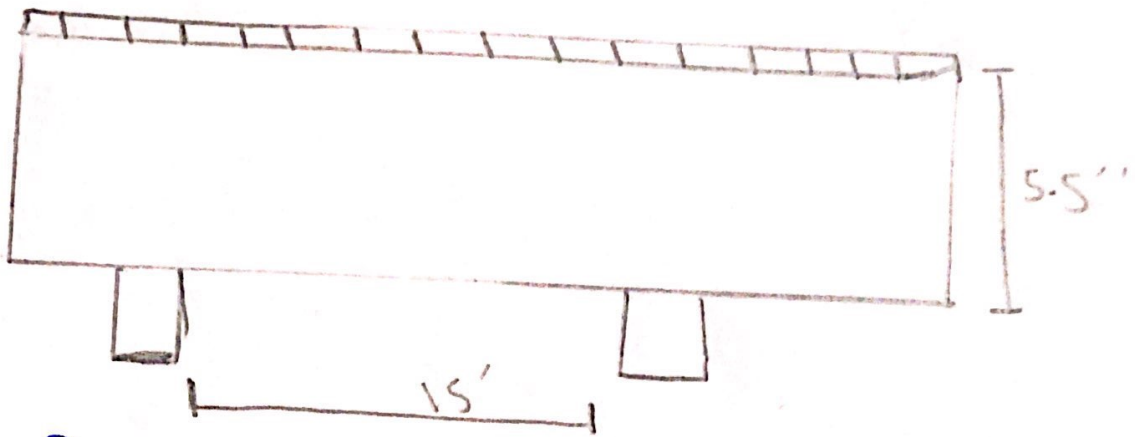
Hence the minimum thickness will be

$$6.5 \times 0.8$$

$$t_{\min} = 5.2 \approx 5.5''$$

Step 2:- (Effective depth)

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By Formula we have

$$\begin{aligned}d &= t - \text{clear cover} - \frac{1}{2} (\text{dia of m.b}) \\ &= 5.5 - 0.75 - \frac{1}{2} (5/8) \\ d &= 4.5''\end{aligned}$$

Step # 3 self weight of slab

$$\frac{t}{12} + \gamma_{\text{concrete}}$$

$$\frac{5.5}{12} + 150 = 68.75 \text{ lb/ft}^2$$

Step # 4 Total Factored load.

$$\text{Factored line load} = 160 \text{ lb/ft}^2$$

The Factor dead load will be

$$D.L = 1.2 (20 + 68.75) = 106.5 \text{ lb/ft}^2$$

$$T.F.L = D.L + LL$$

$$= 106.5 + 160$$

$$= 266.5 \text{ lb/ft}^2$$

$$= 0.2665 \text{ k/ft}^2$$

Step #5 (ultimate moment)

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$$M_u = \frac{W_u \times L^2}{8} = \frac{0.2665 \times (15)^2 \times 12}{8}$$
$$= 89.94 \text{ kip-inch}$$

Step #6

Area of steel For main Bars By Trial and Repeat Method.

Trial #01

Let depth of compression block

$$a = 0.2 \times t$$
$$= 0.2 \times 5.5 = 1.1''$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{1.1}{2})}$$

Trial #2

$$a = \frac{A_{st} \times f_y}{0.85 \times f'_c \times b} = \frac{0.40}{0.85 \times 4}$$

Trial #3

$$a = \frac{0.59 \times 40}{0.35 \times 4 \times 12} = 0.57''$$

$$A_{st} = \frac{89.94}{0.90 \times 4 \times (4.5 - \frac{0.57}{2})} = 0.59 \text{ in}^2$$

so we will use  $A_{st} = 0.59 \text{ in}^2$

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Step #7 Area of steel for distribution reinforcement

$$A_{min} = 0.002 \cdot b \cdot t \quad (\text{For grade 4 steel})$$

$$A_{min} = 0.002 \cdot 12 \cdot 5.5 \Rightarrow 0.132 \text{ in}^2$$

Step #8 spacing for M.B

$$\text{Spacing} = \frac{A_b}{A_{st}} \cdot 12$$

We use #6 bar dia =  $(\frac{6}{8})''$

$$\text{Area} = \frac{\pi}{4} \cdot (\frac{6}{8})^2 = 0.442 \text{ in}^2$$

Step #9 Spacing for distribution bars

$$\text{Spacing} = \frac{A_b}{A_{st}} \quad \text{we use \#5 bar}$$

$$\text{dia} = (\frac{5}{8})'', \quad \text{Area} = \frac{\pi}{4} \cdot (\frac{5}{8})^2 = 0.31 \text{ in}^2$$

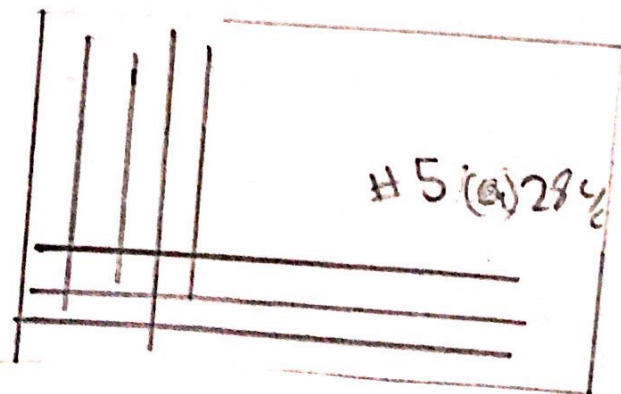
$$\text{Spacing} = \frac{0.31 \cdot 12}{0.132} = 28.1 \approx 28.1 \times 28'' \text{ c/c}$$

Step #10 Final sketch

$$F_c' = 4 \text{ ksi} \quad F_y = 40 \text{ ksi}$$

Main steel #6 at 9" c/c

Distribution steel #5 at 28" c/c



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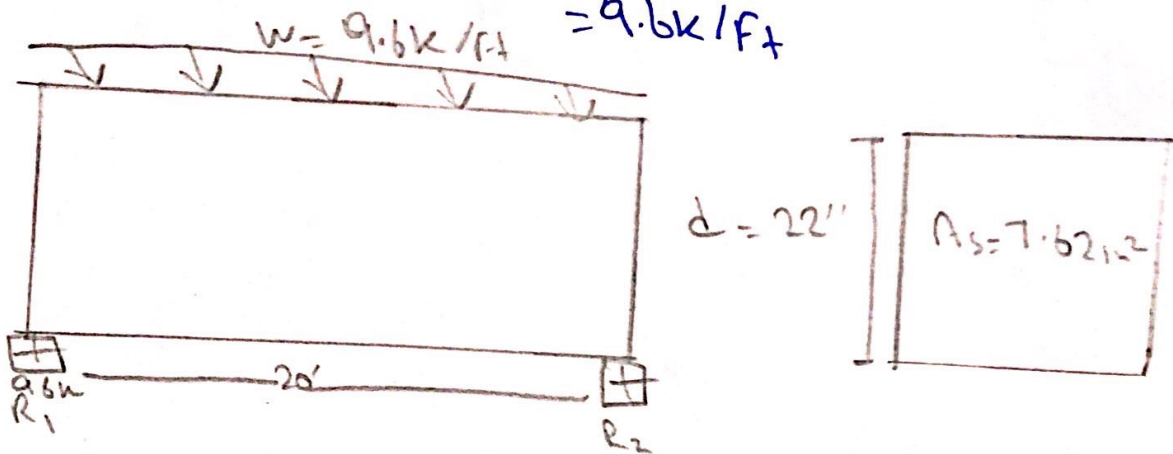
Solution:

At First Find the unit load of beam so b x r c

$$\frac{16}{12} \times 150 = 200 \text{ lb/ft} = 0.2 \text{ k/ft}$$

$$\text{total Factored load} = 9.4 + 0.2$$

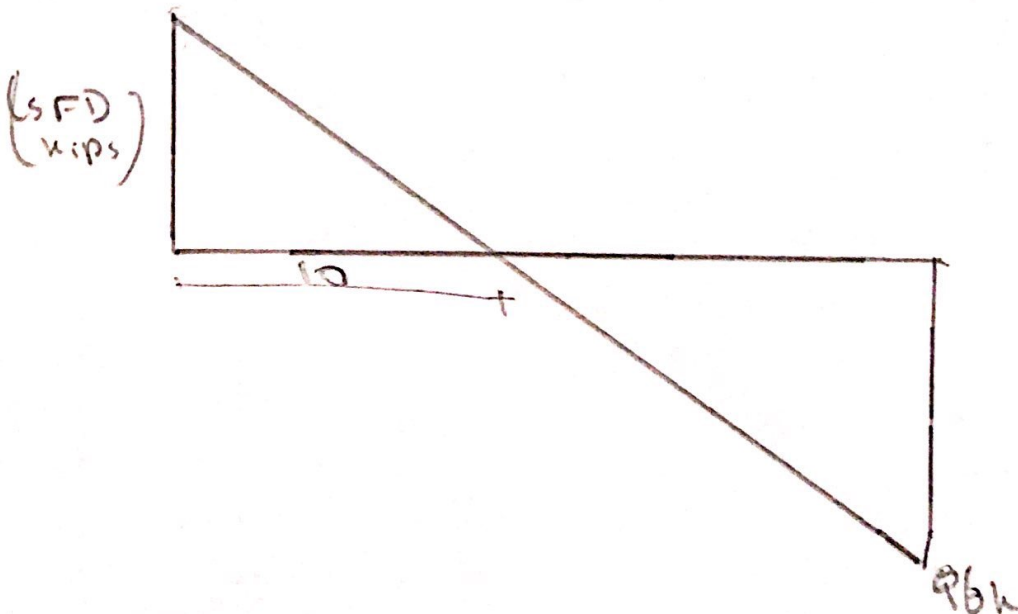
$$= 9.6 \text{ k/ft}$$



Step #1 Finding value of  $R_1$  and  $R_2$

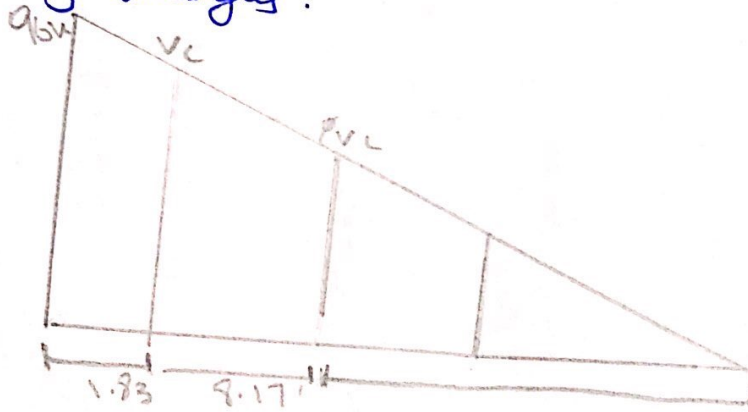
$$\text{total load} = 9.6 \times \frac{20}{2} = 96 \text{ k}$$

Step #2



Step 3 Finding value of critical stress " $V_u$ " & its location.

As we know that critical location is located distance " $d$ " from Face of support  $d = 22' = 1.83'$  value of critical shear at distance " $d$ " by similarity triangles.



From similar =  $\Delta$ 's  $\frac{q_b}{10} = \frac{V_u}{8.17}$   
 $V_u = 78.43k$

Step # 4 Finding value of " $\phi V_c$ " & " $\frac{1}{2} \phi V_c$ " & its distance from zero shear to right side

$$\phi V_c = \phi \times 2 \times \sqrt{F_c} \times b \times d = \frac{0.75 \times 2 \times \sqrt{4000} \times 16 \times 22}{1000}$$

$$\phi V_c = 33.40k$$

location of  $\phi V_c$  by similarity of  $\Delta$ 's

$$\frac{q_b}{100} = \frac{33.40}{k_1} = k_2 = 3.48'$$

Now  $\frac{1}{2} \phi V_c = \frac{33.40}{2} = 16.70k$

Location of  $\frac{1}{2} \phi V_c \Rightarrow \frac{q_b}{20} = \frac{16.70}{k_2}$

$$k_2 = 1.74'$$

Step # 05 Find value of  $\phi V_s (V_u = \phi V_s + \phi V_c)$

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So we have

$$\phi V_s = V_u - \phi V_c$$

$$\phi V_s = 78.43 - 33.40$$

$$\phi V_s = 45.03k$$

Step # 6 Check section Adequacy.

$$\phi (0.8 + \sqrt{F_c}) \times b_w \times d = \frac{0.75 + 0.8 + \sqrt{4000} \times 16 \times 22}{1000}$$
$$= 133.57k$$

$133.57k > \phi V_s$  (mean section is adequate.)

Step # 7 Check mini spacing for stirrups

$$\phi \times 4 \times \sqrt{F_c} \times b_w \times d \Rightarrow \frac{0.7 \times 4 \times \sqrt{4000} \times 16 \times 22}{1000}$$
$$= 66.79k > \phi V_s = 44.03k$$

thus max spacing will be selected from the following 4 conditions

$$\textcircled{1} S_{max} = 24''$$

$$\textcircled{2} \frac{d}{2} = \frac{22}{2} = 11''$$

$$\textcircled{3} S_{max} = \frac{A_u \times F_y}{0.75 + \sqrt{F_c} \times b}$$

$$\textcircled{4} I_{max} = \frac{0.22 \times 60000}{50 \times 16} = 16.50$$

From the above 4 conditions least value of spacing for #3 U shaped will be selected so  $S_{max} = 11''$

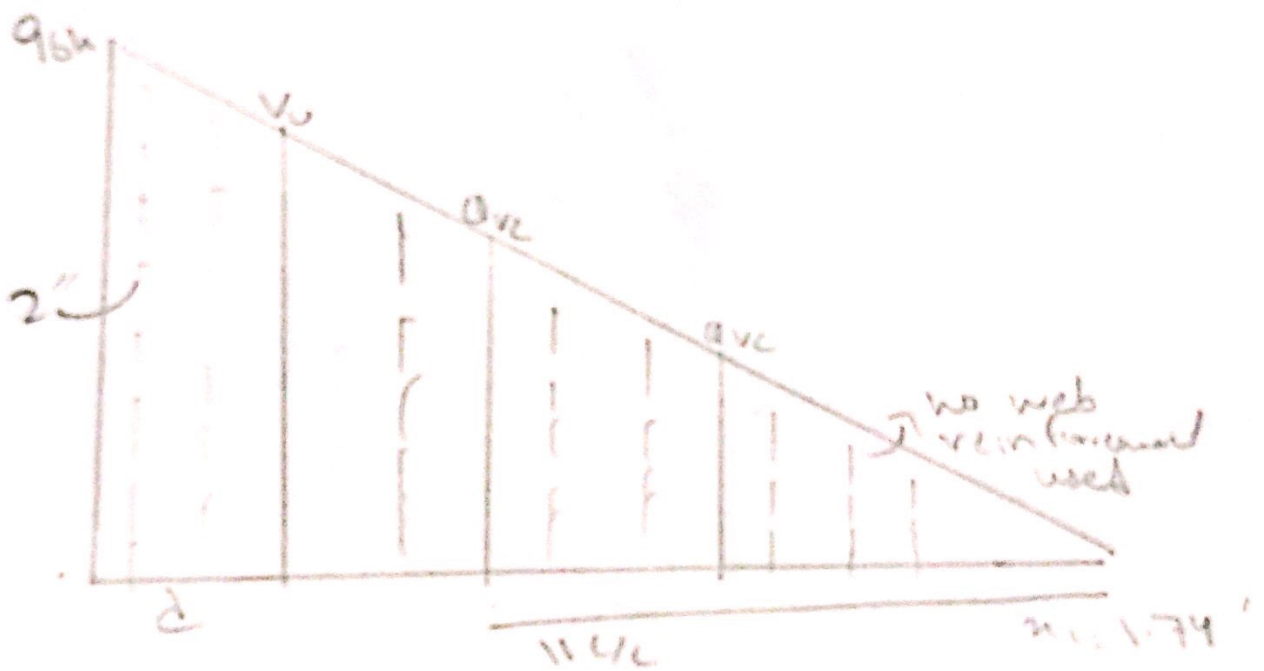


Step #8 Spacing of stirrup from at critical section 7817

$$s = \frac{0 + A_v + f_y + d}{V_u - \phi V_c} = \frac{0.75 + 0.22 + 60 + 22}{79.43 - 33.40}$$

$$s = 4.94 \approx 5" c/c$$

Step #9 Final section



we know that first stirrup from face of support =  $\frac{5}{2} = 2.5 \approx 2"$

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Solution:-

Step #01:-

Find gross area of concrete

$$A_g = b \times b \text{ (since it is a square column)}$$

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

Step #02

Find the area of steel

$$\text{Since } A_s = 5\% \text{ of } A_g$$

$$= 0.05 \times 144$$

$$A_s = 7.2 \text{ in}^2$$

Step #03

ultimate load carrying capacity

$$P_u = 0 \times 0.80 + [0.85 \times F'_c \times (A_g - A_s) + A_s \times f_y]$$
$$= 0.85 \times 0.80 [0.85 \times 4 [144 - 7.2] + 7.2 \times 60]$$

$$P_u = 466.50 \text{ k}$$

Step #04

Sketch and design of Ties (c/c to distance)

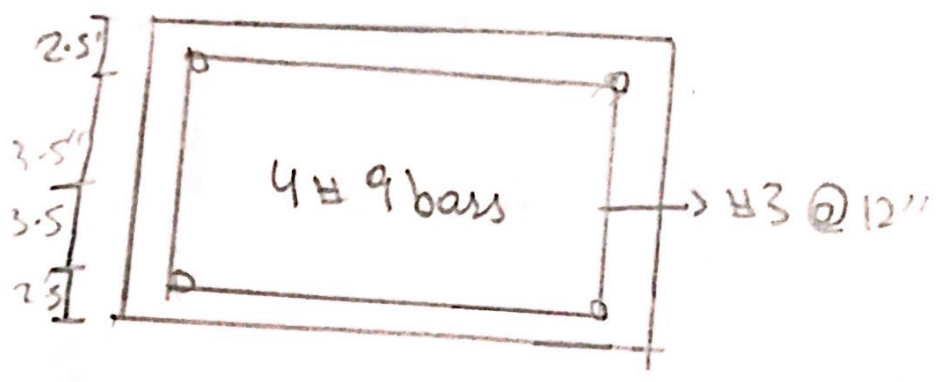
From the below value choose the least value of all this

$$1) \text{ lbr dia of long bar} = 16 \times \frac{2}{3}$$
$$= 10.67$$
$$= 11$$

2)  $4\phi + \text{dia of Tie bar} = 4\phi + 3/8$   
 $= 18''$

3) least column dimension = 12''

So c/c distance b/w ties = 12''



Since its a tied square column so there is no spiral stirrup used, the stirrup used is of rectangular shape due to the specification of the structure thus use will be stirrups instead.

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Solution:-

Step #1

$$\text{let } h = 24''$$

Step #2

Total weight = wt of soil + wt of Re

$$= 3 \times 120 + 2 \times 150$$

$$= 660 \text{ psf} = 0.660 \text{ ksf}$$

Step #3

Effective bearing capacity

$$q_e = q_a - w$$

$$= 2.50 - 0.660$$

$$q_e = 1.84 \text{ ksf}$$

Step #4

Required Area for Foundation.

$$\text{Area}_r = \frac{\text{service load}}{q_e} = \frac{100 + 120}{1.84}$$
$$= 119.57 \text{ ft}^2$$

Step #5

Since Foundation is square.

$$\text{Area}_r = b \times b = 119.57 \Rightarrow B \approx 11$$

Step # 06:- upward bearing capacity of soil

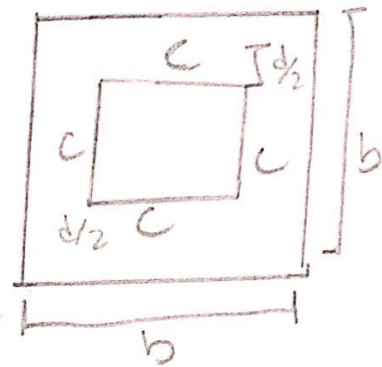
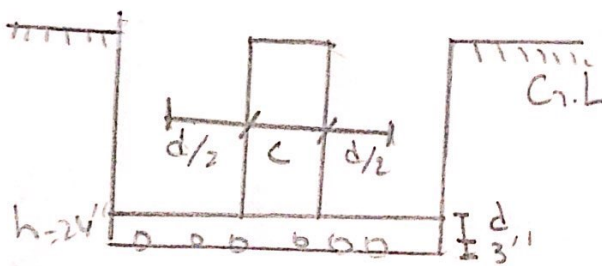
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$$q_{up} = \frac{\text{Factored load}}{(B)^2} = \frac{1.2 \times 100 + 1.6 \times 120}{11^2}$$

$$q_{up} = 2.58 \text{ k / ft}^2$$

Step # 07 Punching shear

$$b_o = 4 \times (c + d)$$



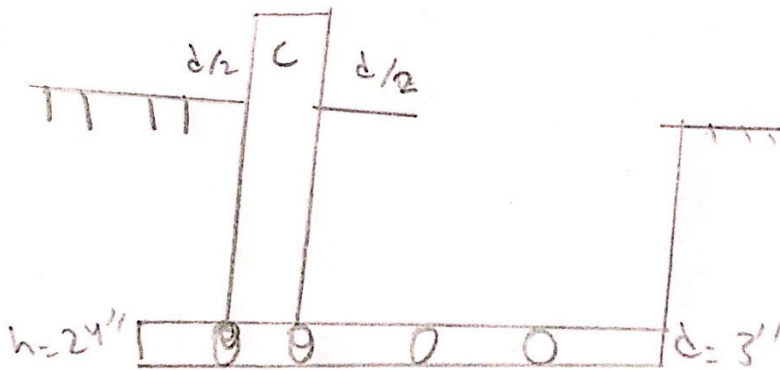
$$d = h - c - \text{dia of bar} - \frac{1}{2} d_b$$

$$= 24 - 3 - 1 - \frac{1}{2}(1) = 19.5''$$

∴ Tak #8 bar

$$\text{dia} = \frac{8}{8} = 1''$$

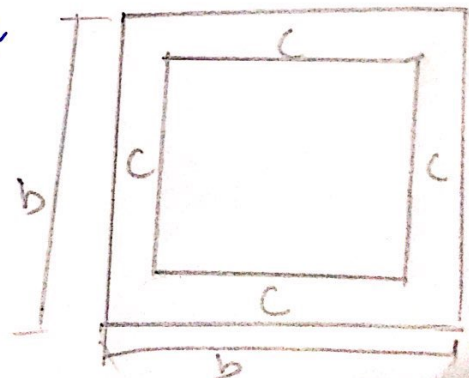
$$b_o = 4 \times (16 + 19.5) = 142''$$



$$d = h - c - \text{dia of bar} - \frac{1}{2} d_b$$

$$= 24 - 3 - 1 - \frac{1}{2}(1) = 19.5''$$

$$b_o = 4 \times (16 + 19.5) = 142''$$



Step # 8:-

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$$V_{u2} = q_{up} + [B^2 - (c+d)^2]$$
$$= 2.58 + [11^2 - \frac{(16+19.5)^2}{12}]$$

$$V_{u2} = 289.60k$$

Step # 9

$$\phi V_{up} = \frac{\phi \times 4 + \sqrt{F_c} \times b \times d}{1000}$$

$$= \frac{0.75 \times 4 + \sqrt{4000} \times 142 \times 19.5}{1000}$$

$$= 525.38k$$

Step 10 - Beam shear / one way shear check -

$$V_{u1} = q_{up} \times B \times \left[ \frac{B}{2} - \frac{c}{2} - d \right]$$

$$V_{u1} = 2.58 \times 11 \left[ \frac{11}{2} - \frac{16}{2} - \frac{19.5}{12} \right]$$

$$V_{u1} = 90.95k$$

Step 11 - Self shear capacity

$$\phi V_c = \phi \times 2 + \sqrt{F_c} \times b \times d$$

$$= \frac{0.75 \times 2 + \sqrt{4000} \times (11 \times 12 - 16)}{1000}$$

$$= 110.04k > V_{u1} \Rightarrow O.K$$

Step 12:- Ultimate Moment

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$$M_o = \frac{q_w p + B}{8} \times (B - C)^2 = \frac{2.58 \times 11}{8} \times \left(11 - \frac{16}{12}\right)^2$$

$$M_w = 331.49 \text{ k}' = 3977.93 \text{ k}''$$

Step 13:- Area of steel for mainbars by trial  
& repeat Method

Trial 1:-

$$\text{Let } a = 0.2 \times h = 0.2 \times 24 = 4.8$$

$$A_s = \frac{M_u}{\phi \times F_y \times \left(d - \frac{a}{2}\right)} = \frac{3977.93}{0.9 \times 60 \times \left(11 - \frac{4.8}{2}\right)} = 8.56 \text{ in}^2$$

Trial 2:-

$$a = \frac{A_s \times F_y}{0.85 \times f_c \times b} = \frac{8.56 \times 60}{0.85 \times 3 \times 11 \times 12}$$

$$A_s = \frac{3977.93}{0.9 \times 60 \times \left(11 - \frac{1.53}{2}\right)} = 7.97 \text{ in}^2$$

Trial 3:-

$$a = \frac{7.197 \times 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$A_s = \frac{3977.93}{0.9 \times 60 \times \left(11 - \frac{1.28}{2}\right)} = 7.1 \text{ in}^2$$

So thus Area = 7.1 in<sup>2</sup>

Step 14L

Check the min reinforcement by the following as method

$$A_{smin} = 0.0018 \times B \times h = 0.0018 \times (11 \times 12) \times 24$$

$$A_{smin} = 5.70 \text{ in}^2$$

$$A_{smin} = \frac{200}{F_y} \times B \times d = \frac{200}{60000} \times (11 \times 12) \times 19.5$$

$$= 8.58 \text{ in}^2$$

$$A_{smin} = \frac{3 \times \sqrt{F'_c}}{F_y} \times B \times d = \frac{3 + \sqrt{3000}}{60000} \times (11 \times 12) \times 19.5$$

$$= 7.05 \text{ in}^2$$

From above values greater value will be selected thus  $A_{smin} = 8.58 \text{ in}^2$

Step 15#

using #8 bars

$$A_b = 0.785$$

$$\text{No. of Bars} = \frac{A_s}{A_b} = \frac{8.58}{0.785} = 10.92$$

$\approx 11$  bars in each direction