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Paper : PRCO-1

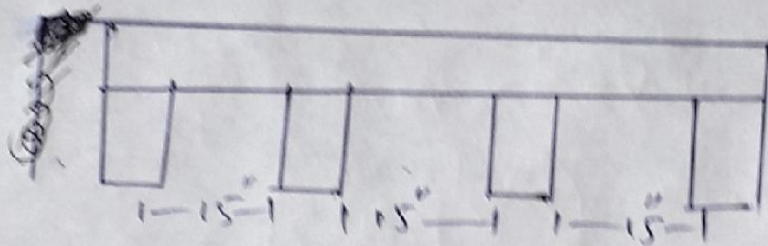
Date : 26 June, 2020.

Q#01

Given data:

- 3 equal spans concrete slab
- Clear span b/w supports = 15 ft
- factored live load = 160 lb/ft²
- Service floor finish load = 20 lb/ft²
- $f_c' = 4000 \text{ psi}$
- $f_y = 40 \text{ ksi}$

Solution:



Step #01

Minimum Thickness

$$\Rightarrow T_{\min} = L/28 = 15/28 = 6.4 \approx 6.5''$$

As $f_y \rightarrow 40 \text{ ksi}$

So multiply this factor with thickness

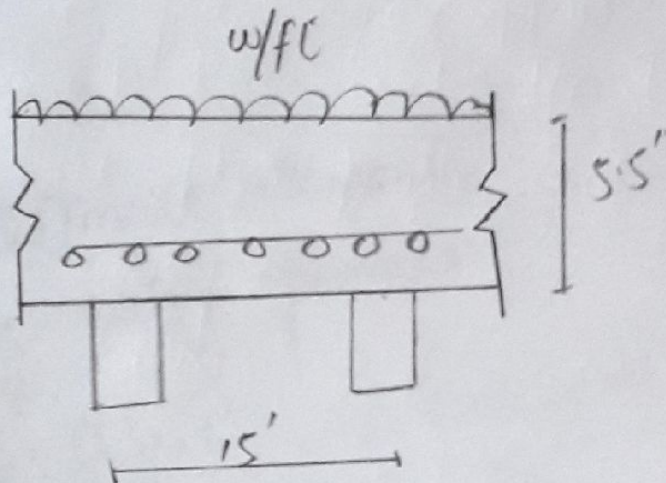
$$\begin{aligned} \Rightarrow \text{factor} &= \left(0.4 + \frac{f_y}{100} \right) \\ &= \left(0.4 + \frac{40}{100} \right) = 0.8 \end{aligned}$$

Hence the minimum thickness will be

$$6.5 \times 0.8$$

$$T_{\min} = 5.2 = 5.5''$$

Step#02



By formula.

$$d = T - \text{clear cover} - \frac{1}{2} \phi (\text{dia of main bars})$$
$$= 5.5 - 0.75 - \frac{1}{2} \left(\frac{5}{8} \right) \cong 4.5''$$

Step#03 ~~the~~ Self weight of slab.

By formula.

$$= \frac{T}{12} \times \gamma_{\text{concrete}}$$

$$= \frac{5.5}{12} \times 150 = 68.75 \text{ lb/ft}^2$$

Step#04 Total factored load.

$$\text{factored live load} = 180 \text{ lb/ft}^2$$

So The factored dead load will be

$$D.L = 1.2(20 + 68.75) = 106.5 \text{ k/ft}^2$$

$$\begin{aligned} \text{Total factored load} &= D.L + L.L \\ &= 106.5 + 160 = 266.5 \text{ k/ft}^2 \\ &\text{or } 0.2265 \text{ k/ft}^2 \end{aligned}$$

Step #5

Ultimate Moment

By using formula.

$$M_u = \frac{W_u \times L^2}{8} = \frac{0.2265 \times 15^2}{8} \times 12 = 89.94 \text{ kip-inch}$$

Step #6

Area of Steel for main Bars By Trial & Repeat method.

* Trial #01

Let depth of compression block

$$a = 0.2 \times T = 0.2 \times 5.5 = 1.1''$$

$$A_{st} = \frac{M_u}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{1.1}{2})} = 0.63 \text{ in}^2$$

* Trial #02

$$a = \frac{A_{st} \times f_y}{0.85 \times f_c' \times b} = \frac{40}{0.85 \times 4 \times 19} = 0.62 \text{ in}^2$$

$$A_{st} = \frac{mV}{\phi \times f_y \times (d - a/2)} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{0.6}{2})}$$

$$A_{st} = 0.59 \text{ in}^2$$

* Trail # 03:

$$a = \frac{0.59 \times 40}{0.83 \times 4 \times 10} = 0.57"$$

$$A_{st} = \frac{89.94}{0.90 \times 40 \times (4.5 - \frac{0.57}{2})} = 0.59 \text{ in}^2$$

So we will use $A_{st} = 0.59 \text{ in}^2$

Step # 07 Area of steel for distribution Reinforcement

$$A_{min} = 0.002 \times b \times L \quad (\text{for grade 40 steel})$$

$$= 0.002 \times 12 \times 5.5 = 1.32 \text{ in}^2$$

Step # 08:

spacing of main bars

$$\text{Spacing} = \frac{A_b}{A_{st}} \times 100$$

(6)

We use #6 bar dia = $(6/8)''$

$$\text{Area} = \pi/4 (6/8)^2 = 0.442 \text{ in}^2$$

Step #9

Spacing for distribution bars.

$$\text{Spacing} = A_b / A_s$$

We use #5 bar S_u

$$\text{dia} = (5/8)'' \Rightarrow \text{Area} = \pi/4 (5/8)^2 = 0.31 \text{ in}^2$$

$$\text{Spacing} = \frac{0.31}{0.132} \times 12 = 27.98'' \approx 28'' \text{ c/c}$$

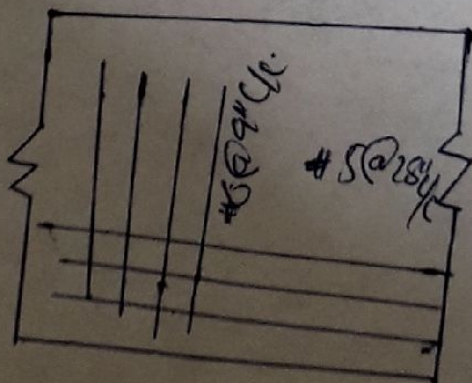
Step #10

find sketch.

$$f_c = 4 \text{ ksi}, f_y = 40 \text{ ksi}$$

main steel #6 at 9" c/c

distribution steel #5 at 28" c/c



Q#02: A Simply Supported ⁽⁷⁾
 diagram.

SOLUTION:

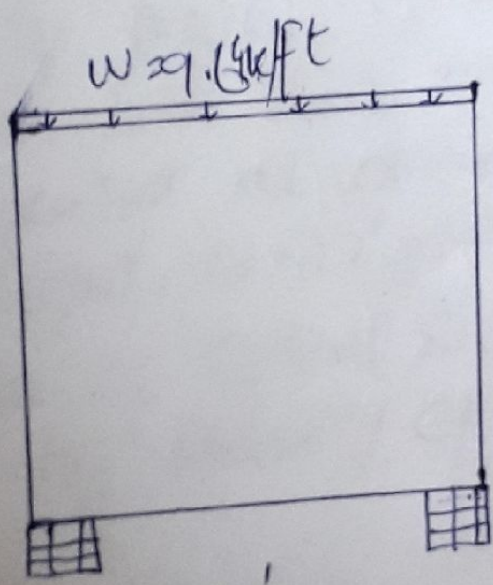
first of all find the unit load of beam.

So $b \times \gamma_c$

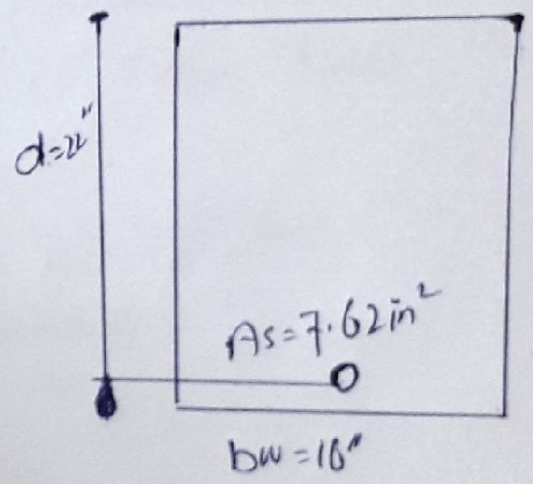
$= \frac{16}{12} \times 150 = 200 \text{ lb/ft} = 0.2 \text{ k/ft}$

→ Now, $1.2 \times 0.2 = 0.24$

→ Total factored load = $9.4 + 0.24 = 9.64 \text{ k/ft}$



Length = 20'



Step 01

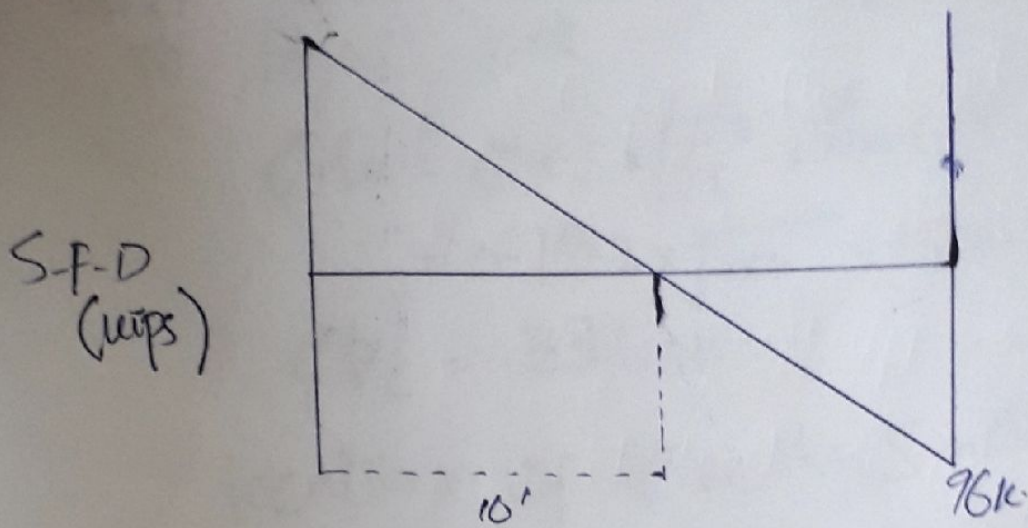
find value of R_1 and R_2

Total load = $9.64 \times \frac{20}{2} = 96.4 \text{ k}$

(8)

Step #02

Draw the Shear force diagram.

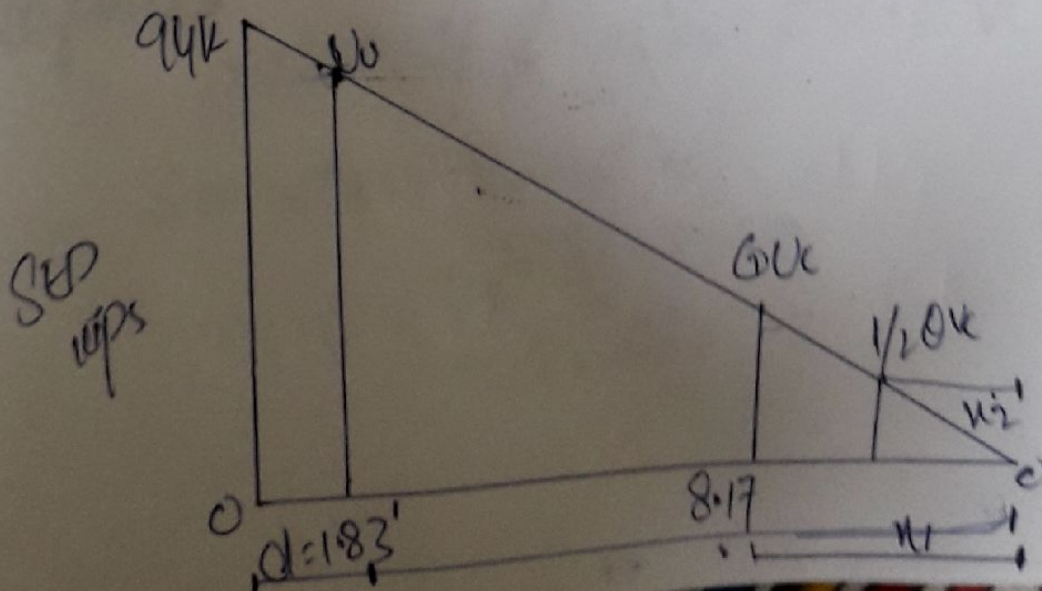


Step #03

find the value of Critical Stress " V_v " and its location.

→ we know that, the critical section is located at distance " d " from face of support. $d = 22'' = 1.83'$

value of Critical Shear at distance ' d ' by Similarity of Triangles.



Step # 4

(9)

find value of ' ϕV_c ' and ' $\frac{1}{2}\phi V_c$ '
and also it distances from zero shear
to Right side.

$$\phi V_c = \phi \times 2 \times \sqrt{f_c'} \times b_w \times d$$
$$= 0.75 \times 2 \times \sqrt{4000} \times 16 \times 22$$

$$\phi V_c = 33.40 \text{ k}$$

location of ϕV_c by similarity of $\Delta S'$

$$\frac{96}{10} = \frac{33.40}{x_1} = 3.48'$$

Now

$$\frac{1}{2}\phi V_c = \frac{33.40}{2} = 16.70 \text{ k}$$

$$\text{location of } \frac{1}{2}\phi V_c \Rightarrow \frac{96}{10} = \frac{16.70}{x_2}$$

$$\Rightarrow x_2 = 1.74'$$

Step # 05

value of ϕV_s ($V_u = \phi V_s + \phi V_c$)

$$\text{So } \phi V_s = V_u - \phi V_c$$
$$= 78.43 - 33.40$$
$$= 45.03 \text{ k}$$

(10)

Step 06

Check on section adequacy

$$\Rightarrow \phi \times 8 \times \sqrt{f_c'} \times b \times d = \frac{0.75 \times 8 \times \sqrt{4000} \times 16 \times 22}{1000}$$
$$= 133.57 \text{ k}$$

As $\phi U_s < \phi 8 \sqrt{f_c'} b \times d$

OTS means section is adequate.

Step # 7

(11)

Check on Section adequacy

$$\Rightarrow \phi 4 \sqrt{f_c'} \times b_w \times d = \frac{0.75 \times 4 \times \sqrt{4000} \times 16 \times 22}{1000} = 66.79 \text{ kslp}$$

$$\text{As, } \phi 4 \sqrt{f_c'} b_w d > \phi V_s = 43.40 \text{ k}$$

So, max-spacing will be selected from following four conditions

1) $S_{\max} = 24''$

2) $d/2 = 22/2 = 11''$

3) $S_{\max} = \frac{A_v \times f_y}{0.75 \times \sqrt{f_c'} \times b_w} = \frac{0.22 \times 60000}{0.75 \times \sqrt{4000} \times 16} = 17.40''$

4) $S_{\max} = \frac{A_u \times f_y}{\phi \times 50 \times b_w} = \frac{0.22 \times 60000}{50 \times 16} = 16.50''$

from above four conditions, least value of spacing from #3, & legged stirrups will be selected.

So $S_{\max} = 11'' \text{ c/c}$

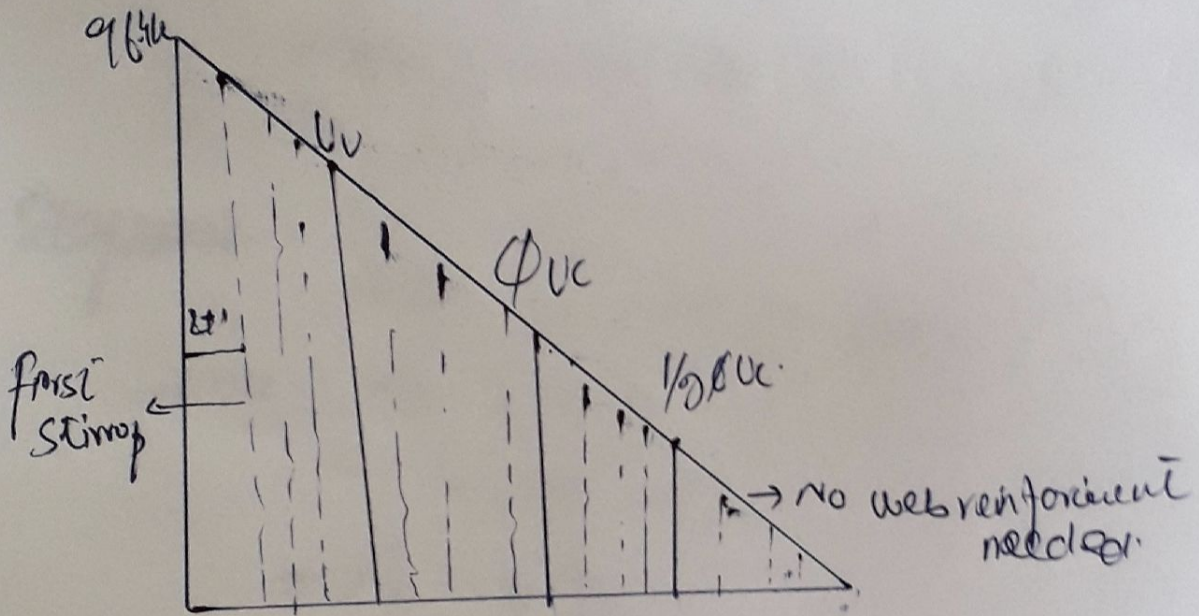
(12)

Step # 08

Spacing of Stirrup from a critical section

$$S = \frac{\phi \times A_v \times f_y \times d}{V_u - \phi V_c} = \frac{0.75 \times 0.22 \times 60 \times 22}{78.43 - 33.40} = 48.4'' \approx 50''$$

Step # 09



Q3: Calculate ⁽¹³⁾ the Axial - - -

- - - Spirals:

Step #01

Find gross Area Concrete.

$A_g = b \times b$ (since it is square cross section column)

$$A_g = 12 \times 12 = 144 \text{ in}^2 \text{ (Actual)}$$

Step #02

Find the Area of steel

Since $A_s = 5\%$ of A_g

$$= 0.05 \times 144$$

$$\Rightarrow A_s = 7.2 \text{ in}^2$$

Step #03

Ultimate the load Carrying Capacity.

$$P_u = \phi \times 0.80 \times \{ 0.85 \times f_c' \times (A_g - A_s) + A_s \times f_y \}$$

$$= 0.65 \times 0.80 \{ 0.85 \times 4 \{ 144 - 7.2 \} + 7.2 \times 60 \}$$

$$P_u = 466.50 \text{ k}$$

Step # 04:

(14)

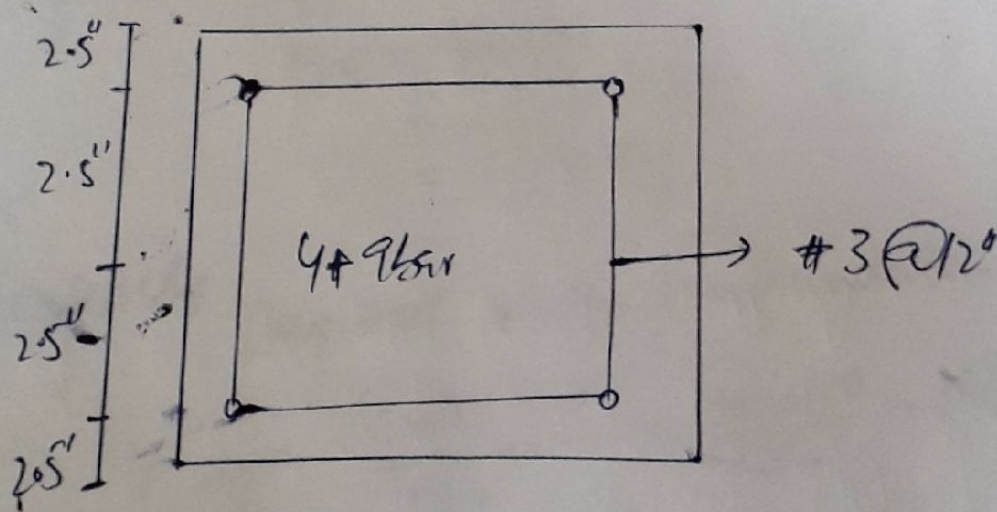
Sketch & design of ties (c/c to distance)
from the below value we choose
the least value of all thus.

$$\rightarrow 16 \times \text{dia of long bar} = 16 \times 9/8 = 18''$$

$$\rightarrow 48 \times \text{dia of Tie bar} = 48 \times 3/8 = 18''$$

$$\rightarrow \text{least column dimension} = 18''$$

$$\text{So, c/c distance b/w ties} = 18''$$



\rightarrow Since it is a tied square column so there is no spiral stirrup used. The stirrup used is of rectangular shape due to specification of the structure thus used will be tie stirrups instead.

2#04 Design ----- final design

(15)

Solution:

Step#01 $w \bar{h} = 24''$

Step#02 total weight $\bar{w} = w_T \text{ of soil} + w_U \text{ of } R_c$
 $= (2 \times 120) + (2 \times 150)$
 $= 600 \text{ lbs} = 0.660 \text{ ksf}$

Step#03 effective Bearing Capacity
 $q_e = q_a - w$
 $= 2.50 - 0.660$
 $= 1.84 \text{ ksf}$

Step#04 Required Area for foundation
 $A_{req} = \frac{\text{Service load}}{q_e} = \frac{100 + 120}{1.84} = 119.57 \text{ ft}^2$

Step#05 Since foundation is square
 $\text{Area} = b \times b = 119.57 \approx 11'$

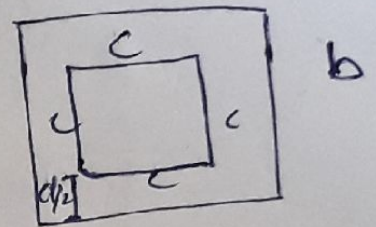
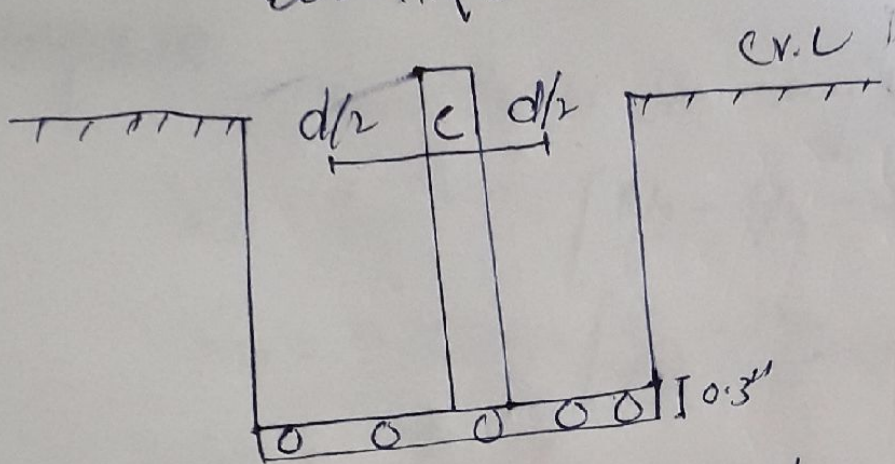
Step#06: Upward bearing Capacity of Soil.

$$q_{up} = \frac{\text{factored load}}{B^2} = \frac{1.2 \times 100 + 1.6 \times 20}{4^2}$$

$$q_{up} = 2.58 \text{ k/ft}^2$$

Step#07: punching shear

$$b_o = 4 \times (c + d)$$



$$d = h - c - \text{dia of bar} - \frac{1}{2} d_b$$

$$= 24 - 3 - 1 - \frac{1}{2}(1) = 19.5''$$

$$\therefore \#8 \text{ bar, } \text{dia} = \frac{8}{8} = 1''$$

$$b_o = 4 \times (16 + 19.5) = 142$$

Step#08:

$$V_{u2} = q_{up} (B^2 - (c + d)^2)$$

$$= 2.58 \left[4^2 - \left(\frac{16 + 19.5}{12} \right)^2 \right]$$

$$= 289.60 \text{ k}$$

Step # 09

(17)

$$\begin{aligned}\phi V_{cp} &= \phi \times 4 \times \sqrt{f_c'} \times b \times d \\ &= \frac{0.75 \times 4 \times \sqrt{4000} \times 142 \times 19.5}{1000} \\ &= 525.38\end{aligned}$$

Step # 10

Beam shear on way shear check

$$\begin{aligned}V_{u1} &= q_{up} \times B \times \left[\frac{B}{2} - \frac{C}{2} - d \right] \\ V_{u1} &= 2.58 \times 11 \times \left[\frac{11}{2} - \frac{16}{2} - 19.5 \right] \\ V_{u1} &= 90.95 \text{ k}\end{aligned}$$

Step # 11

Self shear capacity.

$$\begin{aligned}Q_{vc} &= \phi \times 2 \times \sqrt{f_c'} \times b \times d \\ &= \frac{0.75 \times 2 \times \sqrt{4000} \times (11 \times 12.16)}{1000} \\ &= 110.04 \text{ k} > V_{u1} \Rightarrow \text{Okay}\end{aligned}$$

Step # 12

Ultimate moment.

$$\begin{aligned}M_u &= \frac{q_{up} \times B}{8} \times (B - C)^2 \\ &= \frac{2.58 \times 11}{8} \times \left(11 - \frac{16}{2} \right)^2 = 331.49 \text{ kNm}\end{aligned}$$

Step #13

(18)

Area of Steel for main beam by
Trail & Repeat method.

Trail #01

$$\text{let } a = 0.2 \times h = 0.2 \times 24 = 4.8''$$

$$A_s = \frac{m_u}{\phi \times P_y \times (d - a/2)} = \frac{3977.93}{0.90 \times 60 \times (11 - 4.8/2)} = 8.56 \text{ in}^2$$

Trail #02

$$\Rightarrow a = \frac{A_s \times f_y}{0.85 \times f_c' \times b} = 1.53''$$

$$A_s = \frac{3977.93}{0.90 \times 60 \left(11 - \frac{1.53}{2}\right)} = 7.197 \text{ in}^2$$

Trail #03

$$a = \frac{7.197 + 60}{0.85 \times 3 \times 11 \times 12} = 1.28''$$

$$A_s = \frac{3977.93}{0.90 \times 60 \left(11 - \frac{1.28}{2}\right)} = 7.1 \text{ in}^2$$

So their Area = 7.1 in²

(19)

Step #14: Check the min Reinforcement

$$a) A_{smin} = 0.0018 \times B \times h = 0.0018 (11 \times 12) \times 24 \\ = 5.70 \text{ in}^2$$

$$b) A_{smin} = \frac{200}{f_y} \times B \times H \\ = \frac{200}{60000} (11 \times 12) \times 19.5 \\ = 8.58 \text{ in}^2$$

$$c) A_{smin} = \frac{3 \times \sqrt{f_c'}}{f_y} \times B \times d = \frac{3 \sqrt{3000} \times (11 \times 12) \times 19.5}{60000}$$

→ From above value greater value will be selected $A_{smin} = 8.58 \text{ in}^2$.

Step #15:

Using #8 bar
we get

$$A_b = 0.785 \text{ in}^2$$

$$\text{No of bars} = \frac{A_s}{A_b} = \frac{8.58}{0.785} = 10.92 \approx 11 \text{ bars} \\ \text{in each direction}$$