

# **IQRA NATIONAL UNIVERSITY**



## **Power Electronics** **Final Assignment Spring 2020**

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# Question-1

⇒ Difference between single phase half wave and full wave bridge rectifier:

⇒ Half wave rectifier which convert only one half of the AC cycle into pulsating DC. while full wave rectifier is an electronic circuit which convert entire cycle AC into pulsating DC.

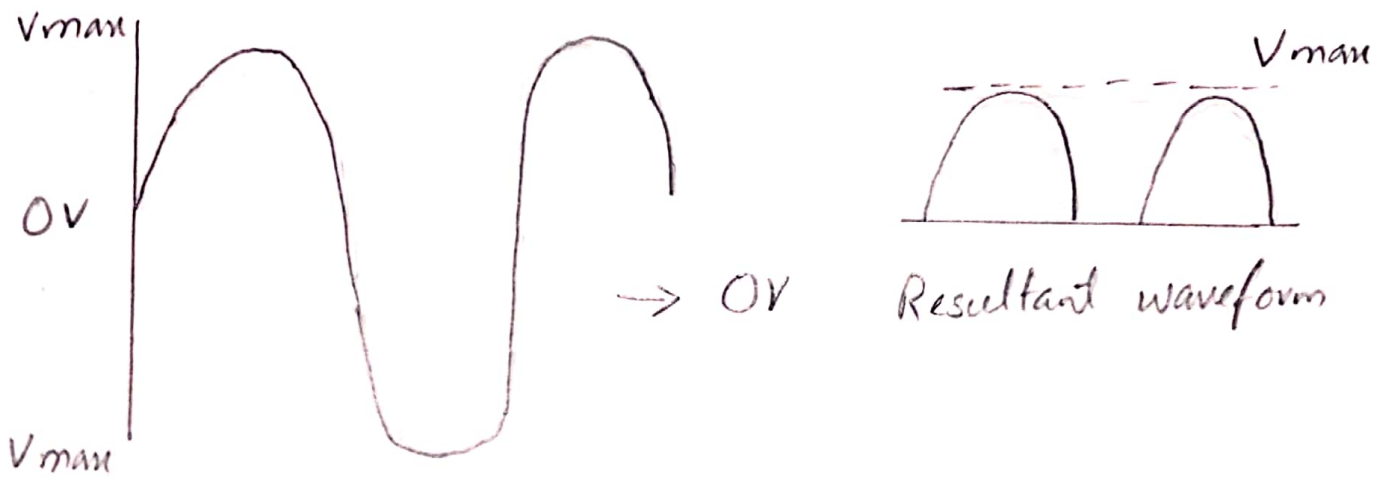
⇒ Half wave utilize only half of AC cycle for the conversion while full wave utilize full wave of AC cycle.

⇒ Half wave is unidirectional, the conduction is one direction only either convert positive or negative, that why called Half wave rectifier is bidirectional, it convert for positive

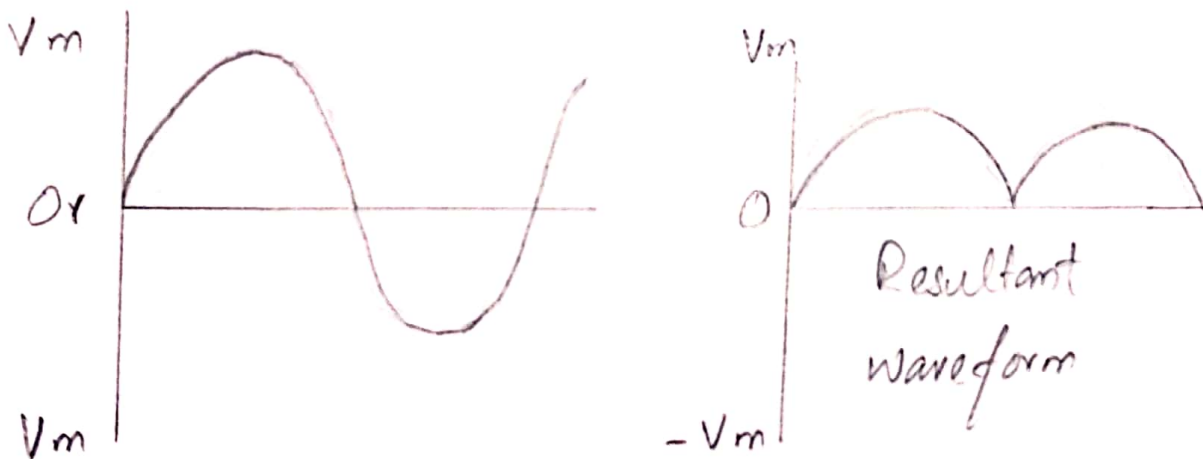
as well as negative half of the cycle.

⇒ Output waveform of single phase half

wave rectifier



And single phase wave bridge rectifier.



⇒ The number of diode in half wave rectifier is 1 while in bridge rectifier is 4.

⇒ Similarities between single phase half wave & full wave bridge rectifier:

⇒ Peak inverse voltage of single half wave and full wave rectifier are same which is  $V_{in}$  & same in both rectifier.

⇒ Both utilize the single phase for the operation.

⇒ Single phase uncontrol and control rectifier difference and similarities:

⇒ Uncontrol they are naturally turn on whenever a positive voltage is applied between its terminal & when they stop by applying it negative voltage.

⇒ while in control rectifier, the conduction start at any angle in positive half cycle normally 0 to 180 degree once the conduction turn on & off.

## Question - 2

Given:-  $V_m = 22\text{ V}$

$$R = 13\ \Omega$$

Solution:- For half wave.

1  $\Rightarrow$   $V_{dc}$  :

$$\frac{V_m}{\pi} \rightarrow \textcircled{1}$$

where  $V_m = 22\text{ V}$  &  $\pi = 3.14$

putting these values in eq  $\textcircled{1}$

$$V_{dc} = \frac{22}{3.14}$$

$$V_{dc} = 7.006$$

For full wave bridge

$$\Rightarrow \frac{2 V_m}{\pi}$$

putting values

$$V_{dc} = \frac{2(22)}{3.14}$$

$$V_{dc} = \frac{44}{3.14}$$

$$V_{dc} = 14.012$$

2  $\Rightarrow$   $I_{dc}$  :

For half wave

$$I_{dc} = \frac{V_m}{\pi R}$$

$$I_{dc} = \frac{22}{(3.14)(13)}$$

$$I_{dc} = \frac{22}{40.82}$$

$$I_{dc} = 0.538 \text{ Amp}$$

for full wave ;

$$I_{dc} = \frac{I_m}{\pi} \rightarrow \textcircled{2}$$

where ,  $I_m = \frac{V_m}{R}$

$$I_m = \frac{22}{13}$$

$$I_m = 1.69 \text{ A}$$

putting in eq (2)

$$I_{dc} = \frac{1.69}{3.14}$$

$$I_{dc} = 0.538 \text{ A}$$

3  $\Rightarrow$   $V_{rms}$  :

For half wave :

$$V_{rms} = \frac{V_m}{2}$$

$$V_{rms} = \frac{22}{2}$$

$$V_{rms} = 11 \text{ V}$$

For full wave :

$$V_{rms} = \frac{1}{\sqrt{2}} V_s \longrightarrow (3)$$

As,

$$V_s = \frac{V_m}{\sqrt{2}}$$

$$V_s = \frac{22}{\sqrt{2}}$$

$$V_s = \frac{22}{1.414}$$

$$V_s = 15.5$$

putting values of  $V_s$  in eq (3).

$$V_{rms} = (\sqrt{2}) (15.5)$$

$$V_{rms} = (1.414) (15.5)$$

$$V_{rms} = 21.917 \text{ V}$$

$\Rightarrow 4 \Rightarrow I_{rms}$  : For half wave & full wave.

For half wave:

$$I_{rms} = \frac{V_m}{2R}$$



putting values;

$$I_{rms} = \frac{22}{2(13)}$$

$$I_{rms} = \frac{22}{26}$$

$$I_{rms} = 0.846 \text{ Amp}$$

For full wave:

$$I_{rms} = \frac{I_m}{2} \rightarrow (4)$$

$$\text{where } I_m = \frac{V_m}{R}$$

$$I_m = \frac{22}{13}$$

$$I_m = 1.69 \text{ A}$$

put value of  $I_m$  in eq (4)

$$I_{rms} = \frac{1.69}{2}$$

$$I_{rms} = 0.840$$

5 ⇒ which rectifier do you think is better and why.

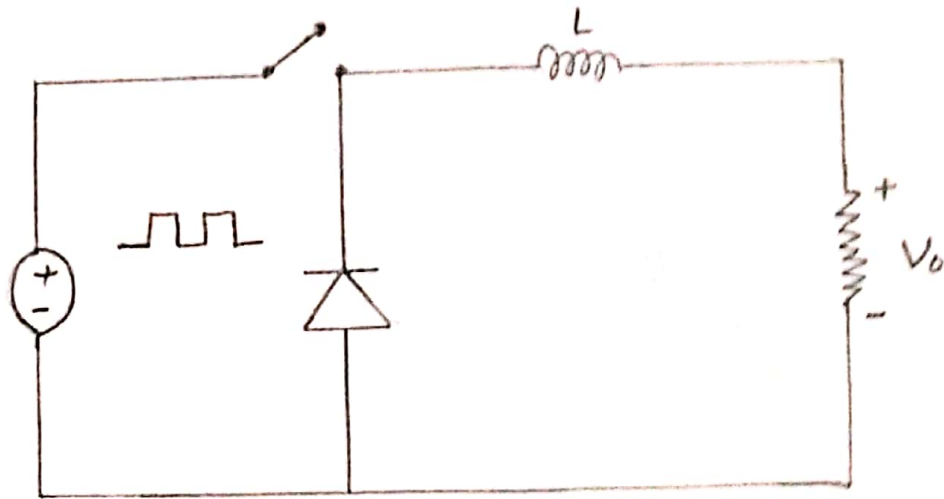
⇒ I would like to refer the uncontrol full wave bridge rectifier because the efficiency of the full wave bridge rectifier is better than in half wave rectifier and output frequency also greater than half wave rectifier.

## Question - 3 :

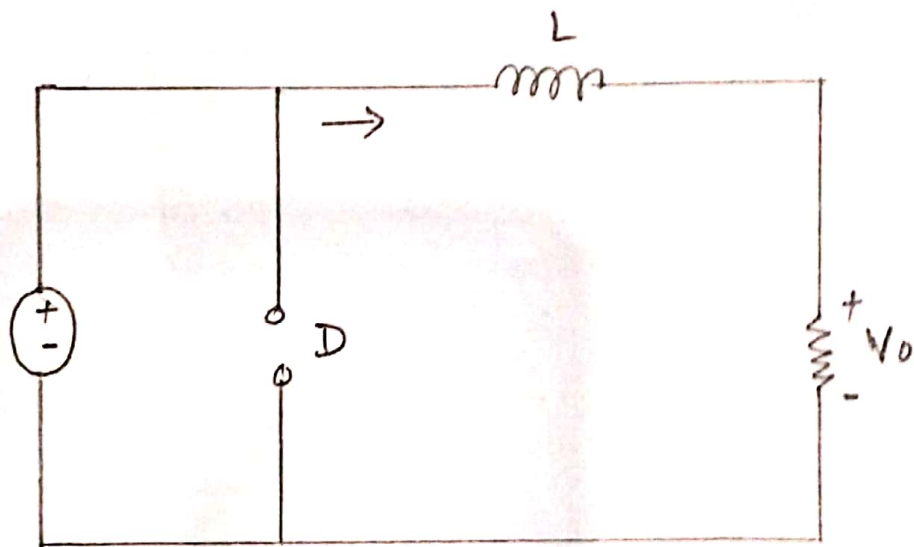
### Buck Chopper :

- ⇒ Output voltage is less than input voltage.
- ⇒ The thyristor in the circuit acts a switch.
- ⇒ when thyristor is ON. supply voltage appear across the load.
- ⇒ when thyristor is OFF, the voltage across the load will be zero.
- ⇒ practical arrangement includes an inductor  $L$  and diode which are used to eliminate current pulsation providing a smooth DC current.
- ⇒ with  $S$  closed,  $D$  is off and it remain off and it remain off as long as  $S$  is ON.

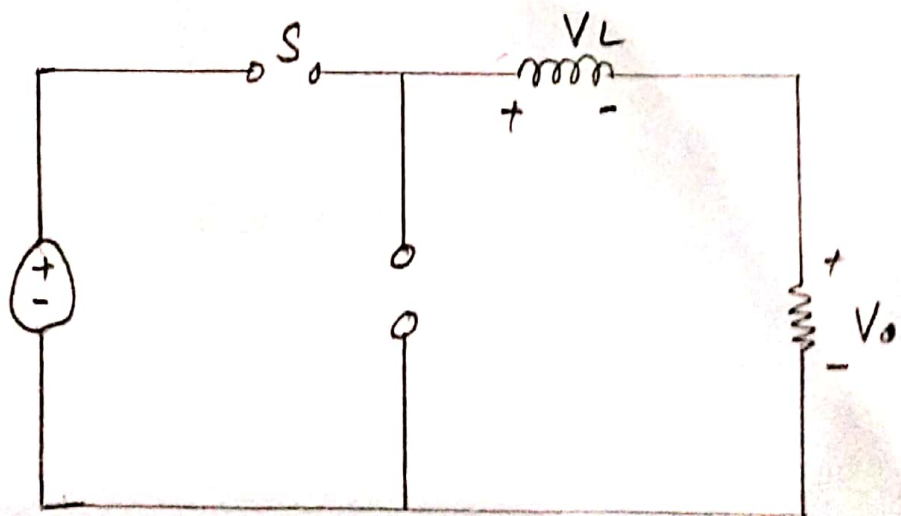
- ⇒ The input current build up exponentially and flow through  $L$  & Load.
- ⇒  $V_o$  equal to  $V_1$
- ⇒ With  $S$  off or open, the current through  $I$  decay to zero.
- ⇒ This cause inductive voltage with opposite polarity across  $L$ .
- ⇒  $V_2$  forward bias diode  $D$ .
- ⇒ Current flows through  $L$  & Load diode  $D$ .
- ⇒ This arrangement permit the use of simple filter inductance  $L$  to provide a satisfactory smooth DC Load current.
- ⇒ With high switch frequency, smaller inductance is sufficient to get desired output.



Circuit of Buck Converter



Circuit when closed



Circuit when switch is open

## Given Data:

$$V_{in} = 50V$$

$$D = 0.22 \%$$

$$R = 13 \Omega$$

$$\text{Frequency } (f) = 20 \text{ KHz}$$

1)  $\Rightarrow$   $V_{out}$

we know that

$$V_{out} = \alpha \times V_s \quad \text{OR} \quad D \times V_s \rightarrow \textcircled{1}$$

Here  $\alpha =$  Duty cycle.

which  $22 \% = 0.22$

putting all value in eq  $\textcircled{1}$

$$V_{out} = (0.22)(50)$$

$$V_{out} = 11V$$

2  $\Rightarrow$   $I_{out}$  :

$$I_{out} = \frac{V_o}{R}$$
$$= \frac{11}{13}$$

$$I_{out} = 0.846 \text{ A}$$

3  $\Rightarrow$   $I_{in}$  :

we know that

$$I_o = \frac{I_i}{\alpha \cdot RD}$$

$$I_i = I_o \times D$$

$$I_i = 0.846 \times 0.22$$

$$I_i = 0.186$$

4  $\Rightarrow$  Inductor :

we know that

$$L = \frac{T \cdot OFF \times R}{2}$$

Let Suppose  $T_{OFF} = 0.009$

$$L = \frac{0.006}{2} \times 13$$

$$L = 0.039 \text{ H}$$

## Question - 4

### Boost Chopper:

- $\Rightarrow$  The output voltage is more than the input voltage by several times.
- $\Rightarrow$  L is used to provide smooth input current.
- $\Rightarrow$  The SCR (s) acts as the switch which work in PWM mode.
- $\Rightarrow$  With S ON, the L is connected to the supply.
- $\Rightarrow$  Load voltage  $V_L$  jumps instantaneously to  $V_s$  but current through L increase linearly & stored energy.



- ⇒ When  $S$  is open, the current collapses and energy stored in  $L$  is transferred to  $C$  through  $D$ .
- ⇒ The induced voltage across the inductor reverse and adds to source voltage, increasing output voltage.
- ⇒ The current that was flowing through  $S$  now flow through  $L$ ,  $D$  &  $C$  to Load.
- ⇒ Energy stored in inductor is released to Load.
- ⇒ When  $S$  closed again,  $D$  becomes reverse bias, the capacitor energy supplied the load voltage and cycle again

$$V_o = V_i + V_L$$

- ⇒  $V_o$  is always higher than  $V_i$  as polarity of inductor voltage  $V_L$  is same as  $V_i$ .

⇒ If inductor  $L$  is very large, source current  $I_1$  is ripple free & considered constant  $W_{ON} = V_1 I_1 T_{ON}$

⇒ Assuming  $C$  to be large enough to neglect the voltage ripple,  $V_o$  is considered constant.

$$W_{OFF} = (V_o - V_i) * I_i * T_{OFF}$$

⇒ Since losses are neglected, the energy stored transferred during  $T_{OFF}$  by  $L$  must be equal to energy gained during  $T_{ON}$

$$W_{ON} = W_{OFF} = V_i I_i T_{ON}$$

$$= (V_o - V_i) * I_i * T_{OFF}$$

$$V_o = V_i \left( 1 + \frac{T_{ON}}{T_{OFF}} \right) = V_i \left( \frac{T}{T - T_{ON}} \right)$$

$$V_i = \left( \frac{1}{1 - \frac{T_{ON}}{T}} \right) = V_o \left( \frac{1}{1 - d} \right)$$

Thus  $V_o$  is always greater than  $V_1$

$$\Rightarrow P_1 = P_o \rightarrow V_1 I_1 = \frac{V_o^2}{R} \Rightarrow I_1 = \frac{V_o^2}{V_L} * \frac{1}{R}$$

$$\Rightarrow I_o = I_1 \times \frac{T_{OFF}}{T} \Rightarrow I_o = I_1 (1-d)$$

$$\Rightarrow P_o = P_1 \Rightarrow V_1 I_1 \Rightarrow \frac{V_o^2}{R} = \frac{V_1^2}{(1-d)^2} * \frac{1}{R}$$

$$\Rightarrow I_1 = \frac{V_1}{(1-d)^2} * \frac{1}{R}$$

$$\Rightarrow I_L = \frac{V_1}{(1-d)^2} * \frac{1}{R}$$

$$\Rightarrow I_L = \frac{I_{max} + I_{min}}{2} = I_1$$

$$\Rightarrow I_{max} + I_{min} = 2 * I_1$$

$\Rightarrow$  Voltage across  $L$  is ;

$$V_L = V_1 = L * \frac{di}{dt}$$

$$\Delta I_1 = \frac{V_1}{L} * T_{ON}$$

Given Data :-

$$V_{in} = 50V$$

$$\text{duty cycle } D = 0.22$$

$$\text{Resistor } R = 13\Omega$$

$$\text{frequency } F = 20 \text{ kHz}$$

1  $\Rightarrow$   $V_{out}$

As we know

$$V_o = V_i \left( \frac{1}{1-d} \right)$$

$$V_o = 50 \left( \frac{1}{1-0.22} \right)$$

$$V_o = 50 \left( \frac{1}{0.78} \right)$$

$$V_o = 64.10$$

2  $\Rightarrow$   $I_{out}$

$$I_o = I_i (1-d) \rightarrow \textcircled{1}$$

First finding  $I_{in}$

⇒  $I_{in}$

$$I_{in} = \frac{V_i}{(1-d)^2} * \frac{1}{R}$$

$$I_{in} = \frac{50}{(1-0.22)^2} * \frac{1}{13}$$

$$I_{in} = \frac{50}{(0.78)^2} * \frac{1}{13}$$

$$I_{in} = \frac{50}{0.6084} * \frac{1}{13}$$

$$I_{in} = 148.63 * \frac{1}{13}$$

$$I_{in} = 6.32 \text{ A}$$

Putting this value in eq ①.

$$I_{out} = I_1 (1-d)$$

$$I_{out} = 6.32 (1-0.22)$$

$$I_{out} = 4.9296 \text{ A}$$

## Question - 5

- ⇒ Buck - Boost Chopper:
- ⇒ It combines the concept of both step-up & step-down chopper.
- ⇒ The output voltage is either higher or lower than input voltage.
- ⇒ The output voltage polarity also be reserved.
- ⇒ The switch is either an SCR or GTO or IGBT.
- ⇒ When S is ON, D is reverse biased and  $I_D$  is zero.
- ⇒ While S is OFF, the source is disconnected
- ⇒ The current through inductor does not change instantaneously and it forward biases the diode, providing path for the load.
- ⇒ With S = ON ( $T_{ON}$ );  $W_{ON} = V_1 * I_1 * T_{ON}$

⇒ With  $S = \text{OFF}$  ( $T_{\text{OFF}}$ );

$$W_{\text{OFF}} = V_1 * I_1 * T_{\text{OFF}}$$

⇒ Ignoring losses;

$$W_{\text{ON}} = W_{\text{OFF}} = V_1 * I_1 * T_{\text{ON}}$$

$$\Rightarrow V_1 * I_1 * T_{\text{OFF}}$$

$$\Rightarrow V_0 = V_1 \frac{dt}{(1-d)T} = V_1 \frac{d}{(1-d)}$$

$$I_L = \frac{I_{\text{max}} + I_{\text{min}}}{2}$$

$$I_1 = I_L d = \frac{(I_{\text{max}} + I_{\text{min}})}{2} * d$$

The average and put  $P_1 = V_1 I_1$

$$= \left( \frac{I_{\text{max}} + I_{\text{min}}}{2} \right)$$

$$* dv \Rightarrow P_0 = \frac{V_0^2}{R}$$

$$I_{\max} - I_{\min} \Rightarrow \frac{V_1}{L} T_{\text{ON}}$$

Again  $I_{\max} + I_{\min} = 2 \times I_1$

Now,

$$I_{\max} = V_1 \left[ \frac{1}{R(1-d)^2} + \frac{T_{\text{ON}}}{2L} \right]$$

$$I_{\min} = V_1 \left[ \frac{1}{R(1-d)^2} - \frac{T_{\text{ON}}}{2L} \right]$$

$$I_{\text{P-D}} = I_{\max} - I_{\min} = \frac{V_1 T_{\text{ON}}}{L}$$

For continuous current mode.

$$I_{\min} = V_1 \left[ \frac{1}{R(1-d)^2} - \frac{T_{\text{ON}}}{2L} \right]$$

$$\Rightarrow \frac{1}{R(1-d)^2} = \frac{T_{\text{ON}}}{2L} \Rightarrow$$

$$\Rightarrow L = \frac{R T_{\text{ON}}}{2} (1-d)^2$$



Given Data:-

$$V_{in} = 50V$$

$$V_{out} = 22\% = 0.22$$

$$\text{Resistor (R)} = 13\Omega$$

$$\text{Frequency } f = 20 \text{ kHz}$$

1  $\Rightarrow$  'Duty cycle (D)

we know that

$$\frac{V_o}{V_i} = \frac{-D}{1-D}$$

$$V_o = \frac{V_i D}{1-d}$$

$$\Rightarrow 0.22 = 50 \frac{d}{1-d}$$

$$\Rightarrow 0.22(1-d) = d50$$

$$\Rightarrow 0.22 - 0.22d = d50$$

$$\Rightarrow 0.22 = d50 + 0.22$$

$$0.22 = 50 \cdot 22 d$$

$$\Rightarrow d = 0.0022$$

$$2 \Rightarrow I_{out}$$

we know that

$$I_{max} + I_{min} = \frac{2 d V_i^2}{R (1-d)^2}$$

$$= \frac{2 (0.0022) 50}{13 (1 - 0.0022)^2}$$

$$= \frac{0.22}{12.94}$$

$$I_{max} + I_{min} = 0.0017 \rightarrow \textcircled{1}$$

we know that

$$I_{out} = \frac{I_{max} + I_{min}}{2}$$

putting eq  $\textcircled{1}$  in place of  $I_{max} + I_{min}$

$$I_{out} = \frac{0.0017}{2} \Rightarrow 0.00085A$$

$$3 \Rightarrow I_i = ?$$

$$I_i = I_c d$$

$$I_i = 0.00085 \times 0.0022$$

$$I_i = 0.00000187 \text{ A}$$

4  $\Rightarrow$  Inductor:

$$L = \frac{RTd}{2} (1-d)^2$$

putting value where  $T = 1/F$

$$L = \frac{13(5 \times 10^{-5}) \times 0.0022}{2} (1 - 0.0022)^2$$

$$L = \frac{0.0000014}{2} (0.9978)^2$$

$$\Rightarrow L = 6.93 \times 10^{-7} \text{ H}$$